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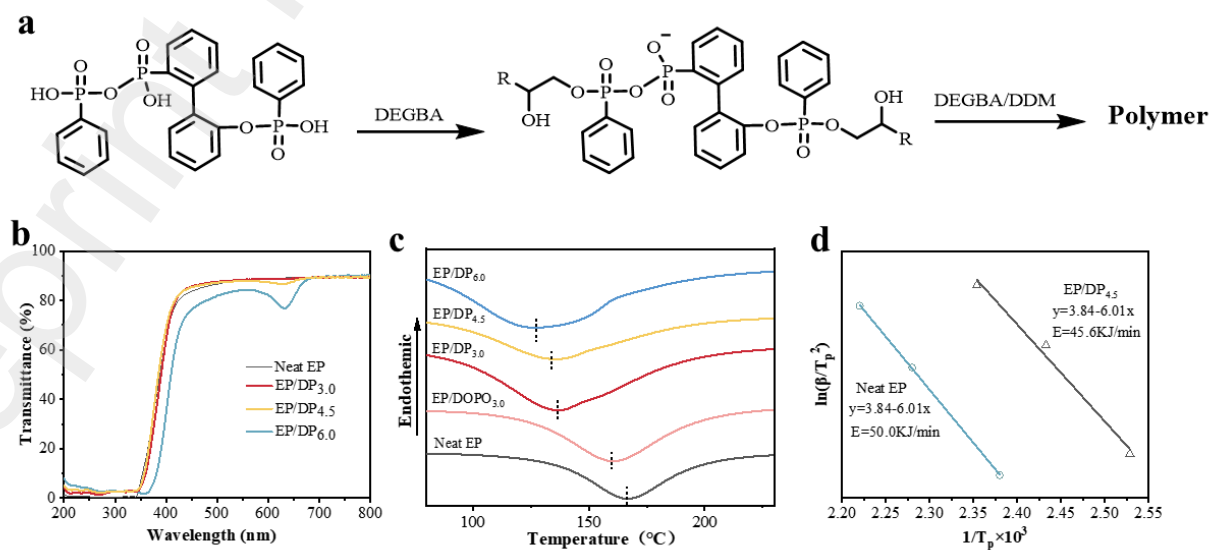


Figure 2. (a) Curing promotion mechanism of DP. (b) Optical performance of EP samples. (c) DSC curves of EP samples at a temperature increase rate of 10 K/min. (d) Kissinger method of fitting curves for EP and EP/DP_{4.5}.

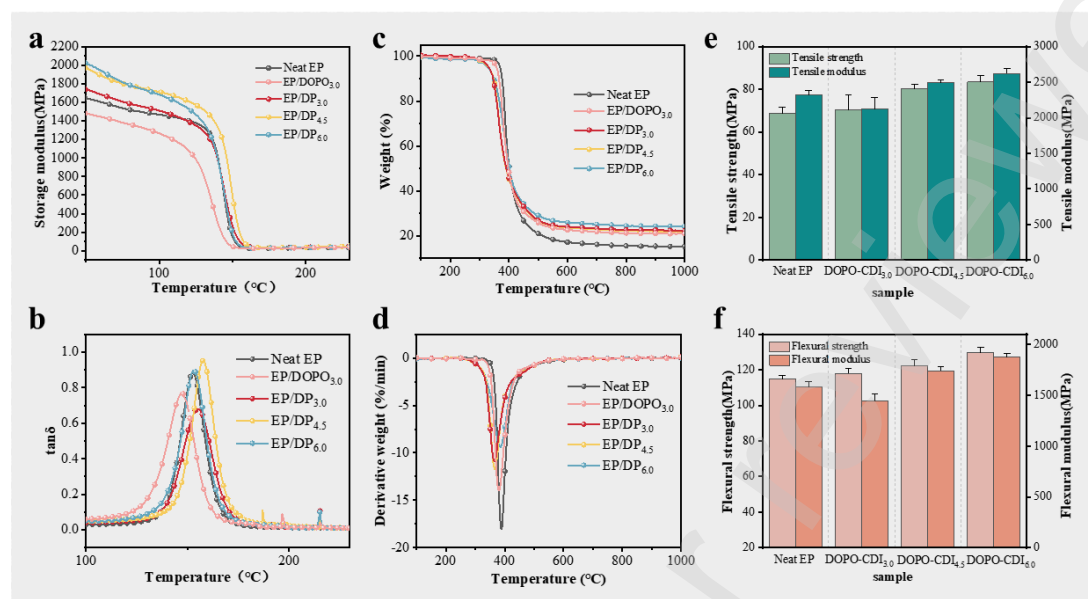


Figure 3. (a) Curves of storage modulus and (b) loss modulus versus temperature. (c) Curves of weight and (d) derivative weight as a function of temperature. (e) Tensile and (f) Flexural Properties of EP Samples.

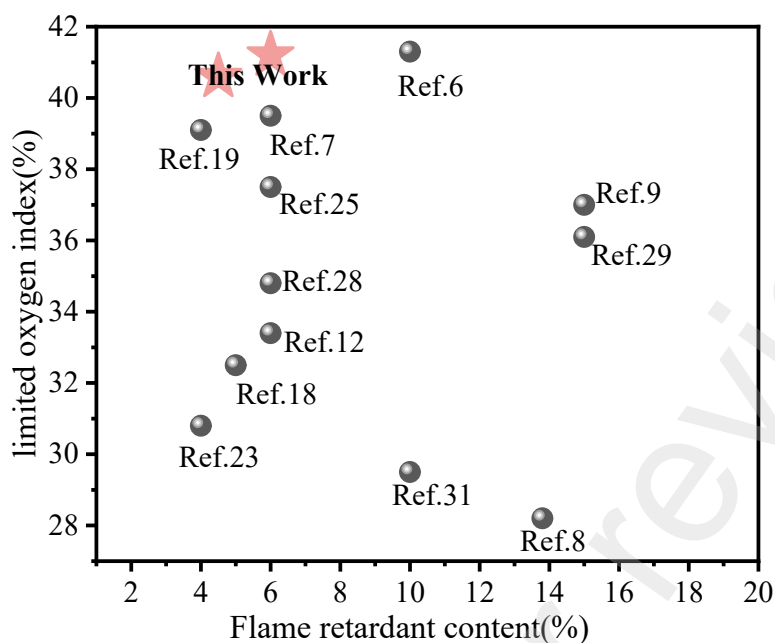


Figure 4. Scatter Plot of Flame Retardant Efficiency Comparison of Flame Retardants.

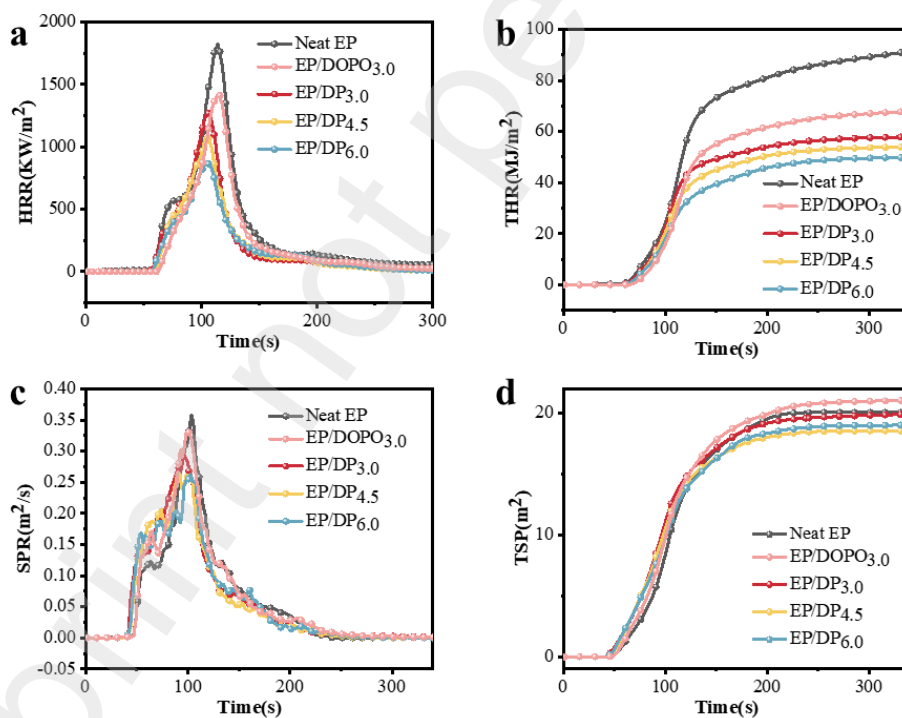


Figure 5. (a)HRR. (b)THR. (c)SPR. (d)TSP curves of EP thermosets obtained from cone calorimetry.

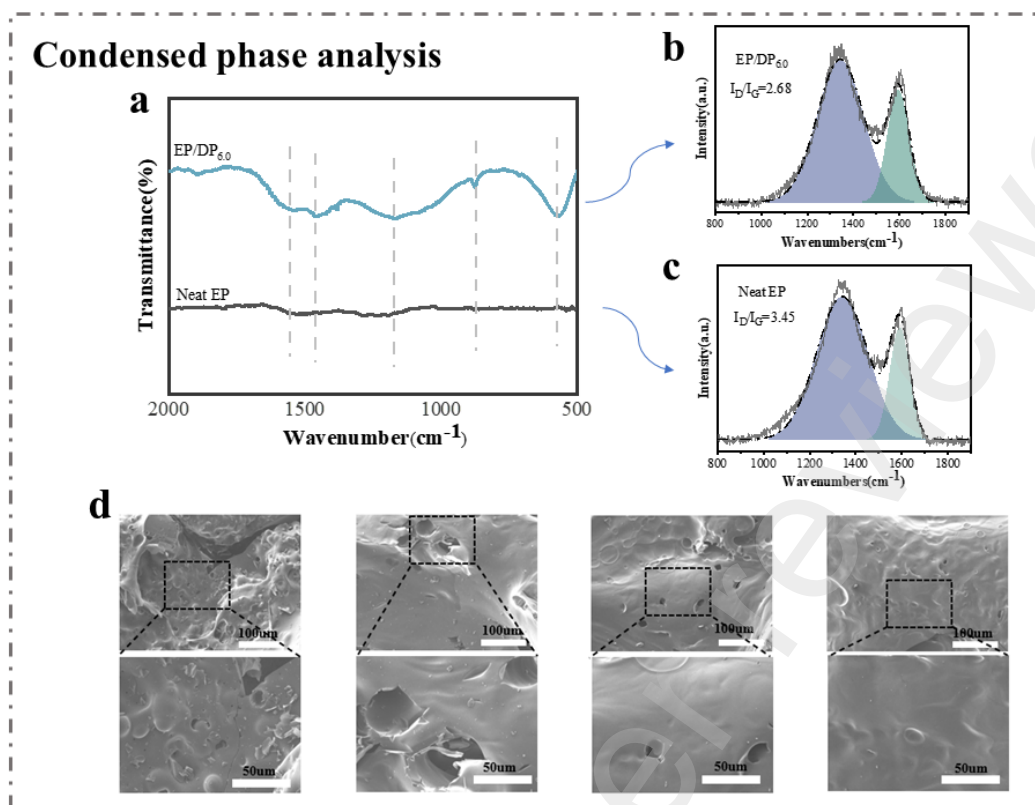


Figure 6. (a) FTIR of EP/DP_{6.0} and Neat EP combustion residues. (b) Raman spectral fitting curve of EP/DP_{6.0} and (c) Neat EP. (d) Microscopic morphology of combustion residues of EP samples (100x and 270x).

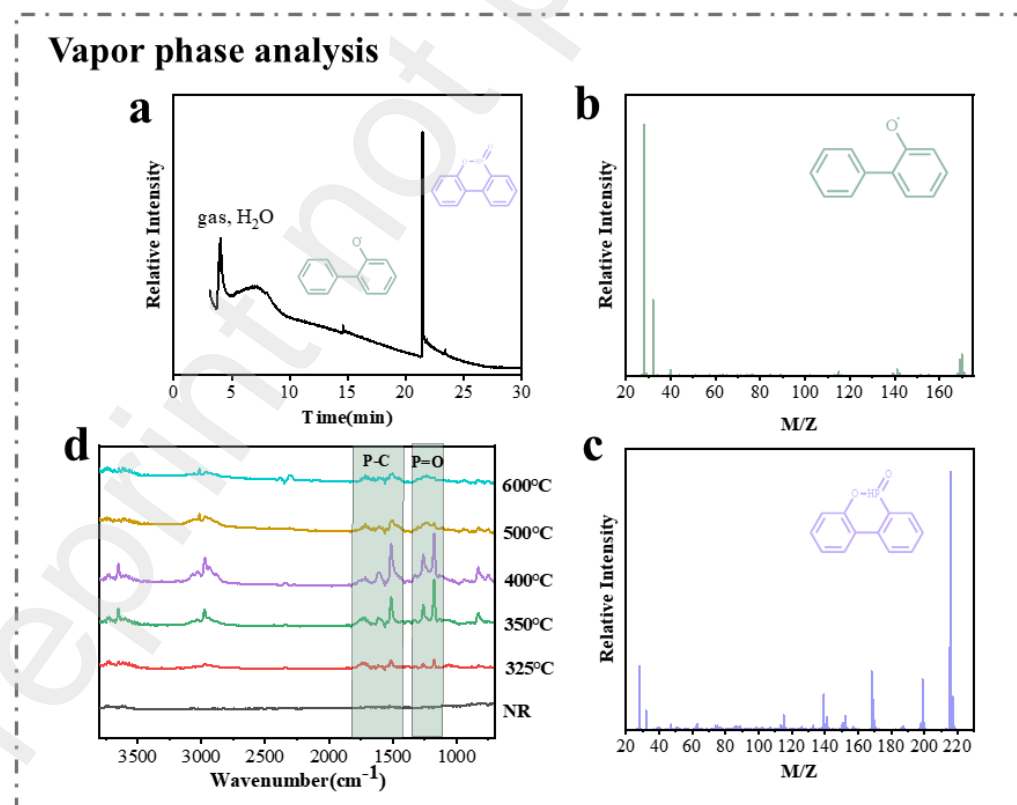
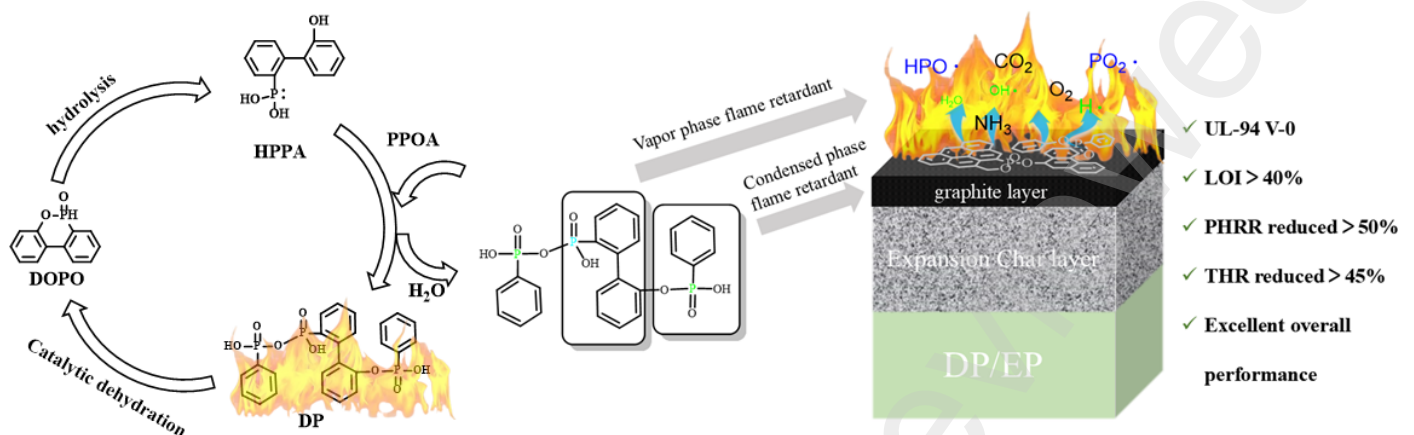


Figure 7. (a) Thermal cleavage Py-GC/MS spectra of DP. (b) Partial radical fragments and (c) DOPO fragments from thermal cleavage. (d) TG-IR spectrum of EP/DP_{6,0}.



Due to the excellent catalytic charring ability of PPOA, DP is able to re-form DOPO when heated, thus avoiding the adverse effect of DOPO on the material performances while providing the gas-phase flame retardant effect of DOPO.

Figure 8. DP design concept and mechanism of action.

1 **A high-performance flame retardant liquid synthesized on the basis of DOPO**
2 **hydrolysis products avoids the defects of DOPO**

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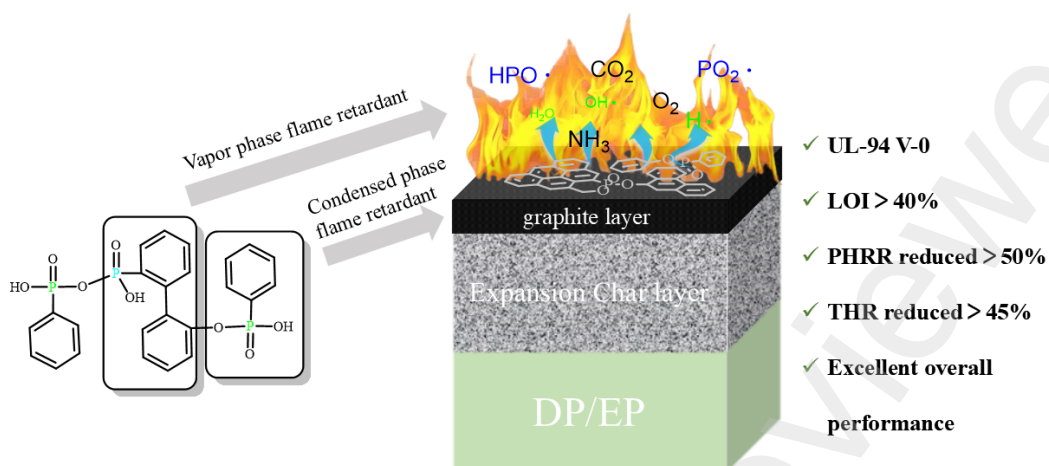
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11 **ABSTRACT:**

12 It was first proposed to use 2-(2-hydroxyphenyl) phenyl phosphonic acid
13 (HPPA), which is hydrolysis product of DOPO, has a structure more similar to EP, to
14 replace DOPO in the preparation of flame retardant, and finally synthesized a highly
15 efficient liquid flame retardant DP based on HPPA, the theoretical phosphorus content
16 of DP is up to 17.5wt%, so EP can achieve excellent flame retardant/inhibit
17 combustion effect with a small amount addition of DP. For example, the LOI of
18 EP/DP_{6.0} is increased to 41.2% and reaches the V-0 rate of UL-94, the PHRR and
19 THR are reduced by 52.4% and 45.2% respectively, in addition, the addition of DP in
20 small quantities does not destroy the overall performance of EP, maintains and
21 improves the excellent mechanical and thermal properties of epoxy resin as a whole,
22 and DP has excellent curing promoting effects, meeting the processing and use
23 requirement of high performance EP. It is better than DOPO overall and has good
24 application prospects.



25

26 **KEYWORDS:** Epoxy resin, Flame retardant, Overall properties, DOPO, HPPA

1. INTRODUCTION

Epoxy(EP) are thermosetting material widely used in many fields and have attracted much attention in recent years due to their high specific strength, excellent thermal stability and outstanding chemical resistance [1][2][3]. However, similar to most organic carbon skeleton materials, epoxy resins are extremely flammable, which greatly restricts the application of epoxy resins, especially in aerospace, railway transportation, electrical and electronic fields that require high safety [4][5]. Therefore, the flame retardant modification of epoxy resins is an important and valuable topic.

The current research on the flame retardant modification of EP mainly focuses on phosphorus flame retardants, which have the advantages of being environmentally friendly, highly effective and strongly active compared to traditional halogen and metal-based flame retardants [6][7], and can be tailored to the functionality of different application requirements [8]. For example, IDPP, a latent curing agent based on 9,10-Dihydro-9-oxa-10-phosphaphenanthrene-10-oxide(DOPO) and imidazole developed by Xu et al. utilizes a coordination effect to reduce imidazole activity, enabling EP to remain processable for a long time at room temperature [9].

DOPO is one of the most commonly used organophosphorus flame retardants, however, unmodified DOPO mainly plays the role of vapor phase flame retardant, so the flame retardant efficiency is poor and often needs to be added in large quantities to the material to achieve a better flame retardant effect [10][11]. According to the experiment, we found that the heterophenanthrene group of DOPO does not bring good thermal stability to the matrix material due to the plasticizing effect, and DOPO is a solid that is difficult to dissolve in the EP monomer, so the processing of DOPO-modified EP is often time consuming and energy wasting [10][12]. In contrast, we believe that 2-(2-hydroxyphenyl) phenyl phosphonic acid(HPPA), a by-product of DOPO synthesis, has a chemical structure similar to that of DEGBA, and therefore may be more suitable as a matrix material for the preparation of EP flame retardants.

55 Normally, HPPA is difficult to be separated from the mixture with DOPO,
56 therefore, no research on the modification of HPPA has been conducted in the field of
57 epoxy flame retardant until now, some studies have shown that acidic conditions can
58 promote the conversion of DOPO to HPPA [13].

59 It is well known that the addition of large amounts of flame retardants can lead to
60 the deterioration of the overall performance of the substrate[14][15], so we are devoted
61 to the design of a high-phosphorus content flame retardant based on HPPA, to achieve
62 excellent flame retardancy and good overall performance with a low level of additive.

63 In this work, we utilized the difference of nucleophilicity between the functional
64 group in HPPA and PPOA, and manufactured a liquid flame retardant DP with high
65 phosphorus content by vacuum heating assistance, which can make the epoxy resin
66 system reach 1 wt% phosphorus content by adding only 6 wt%, has both gas-phase and
67 condensed-phase flame retardant effects, which meets our expectation of excellent
68 flame retardancy without destroying the overall properties of EP.

70 2. MATERIALS AND METHODS

71 2.1. Materials

72 In supplementary document.

73 2.2. Synthesis of DP

74 Firstly, 25.92 g of DOPO (0.12 mol) and 15.8 g of PPOA (0.1 mol) were weighed
75 into a 250 ml three-necked flask equipped with magnetic stirring and condensation
76 reflux device. Measure 100 ml of DMF and 25 ml of dilute hydrochloric acid (1mol/L)
77 with a measuring cylinder and slowly drop the dilute hydrochloric acid into DMF, and
78 then add it to the three-necked flask after mixing well and stirring at 100°C for 8h to
79 activation. After that, the system was transferred to a vacuum reaction device and
80 reacted at -80 Kpa and 90 °C for 2 h. Finally, all the water and most of the DMF were
81 removed by rotary evaporation then washed 3 times with toluene to remove the residual
82 DMF and excess DOPO to obtain a colorless and transparent liquid flame retardant DP.

83 2.3. Fabrication of EP thermosets

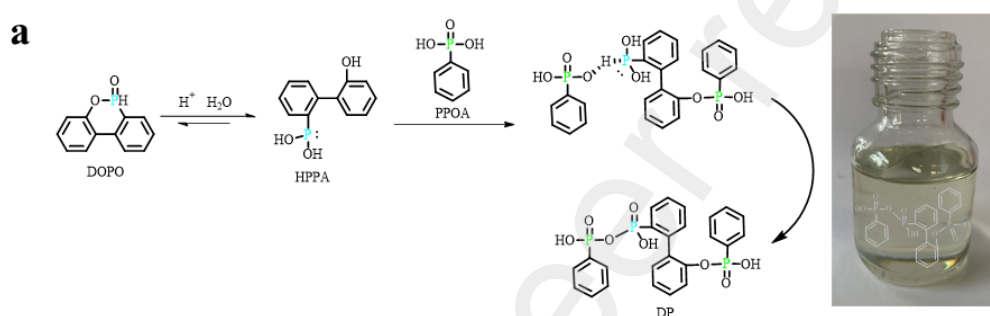
84 In the preparation of EP/DP, a specific amount of EP monomer and DP were
85 weighed and mechanically stirred at 90°C for at least 10 min to obtain a homogeneous
86 solution, and then DDM was added after the system cooled down to 80°C. After
87 completely dissolved, put into the vacuum defoamer to remove the foam and pour into
88 the mold that has been preheated then put into the oven. Curing program is set to 80°C
89 1h, 130°C 2h, 180°C 2h.

90 Neat EP and EP/DOPO3.0 were prepared in a similar procedure by adding DDM
91 after obtaining a homogeneous system at 100°C, dissolving, defoaming and placing in
92 an oven, and the curing procedure followed the typical Neat EP curing steps of 100°C
93 for 2h, 150°C for 2h, and post-curing at 180°C for 2h. Detailed formulations of each
94 group of thermosetting resins are shown in Table 1.

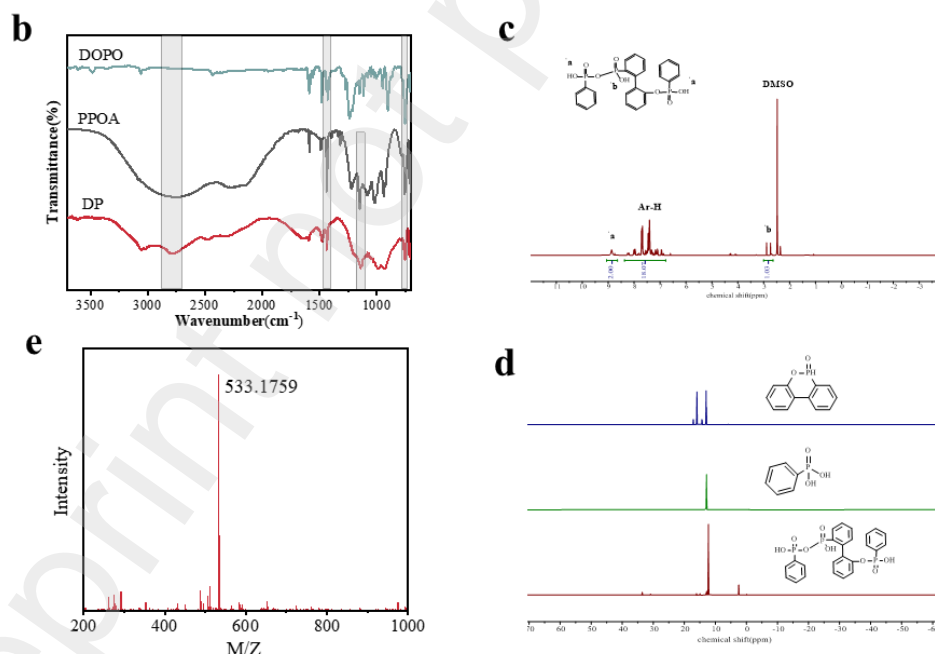
95 Table 1. The formulations of epoxy thermosets

| Sample | DGEBA(wt%) | DDM(wt%) | DP(wt%) | P(wt%) |
|------------------------|------------|----------|---------|--------|
| Neat EP | 80 | 20 | 0 | 0 |
| EP/DOPO _{3.0} | 77.6 | 19.4 | 3.0 | 0.43 |
| EP/DP _{3.0} | 77.6 | 19.4 | 3.0 | 0.53 |
| EP/DP _{4.5} | 76.4 | 19.1 | 4.5 | 0.79 |
| EP/DP _{6.0} | 75.2 | 18.8 | 6.0 | 1.05 |

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Figure 1: (a) The form and synthesis steps of DP. (b) FT-IR spectra of DOPO, PPOA and DP, (c) ^1H NMR of DP. (d) ^{31}P NMR of raw materials and DP. (e) high resolution mass spectrometry of DP.

102

2.4. Characterizations

103

In supplementary document.

104 3. RESULTS AND DISCUSSION

105 3.1. Characterization of DP

106 We have accurately characterized DP by FTIR, ^1H NMR, ^{31}P NMR and high-
107 resolution mass spectrometry as shown in Fig. 1, firstly, the wavelength 2820 cm^{-1}
108 reflects the P-OH bond absorption peaks of HPPA and PPOA **Error! Reference**
109 **source not found.**[16][18]. The absorption peak at 1440 cm^{-1} reflects the P-Ph
110 absorption peak of DP liquid, while the P=O absorption peak of DP is similar to that
111 of PPOA located at 1140 cm^{-1} [20][21].

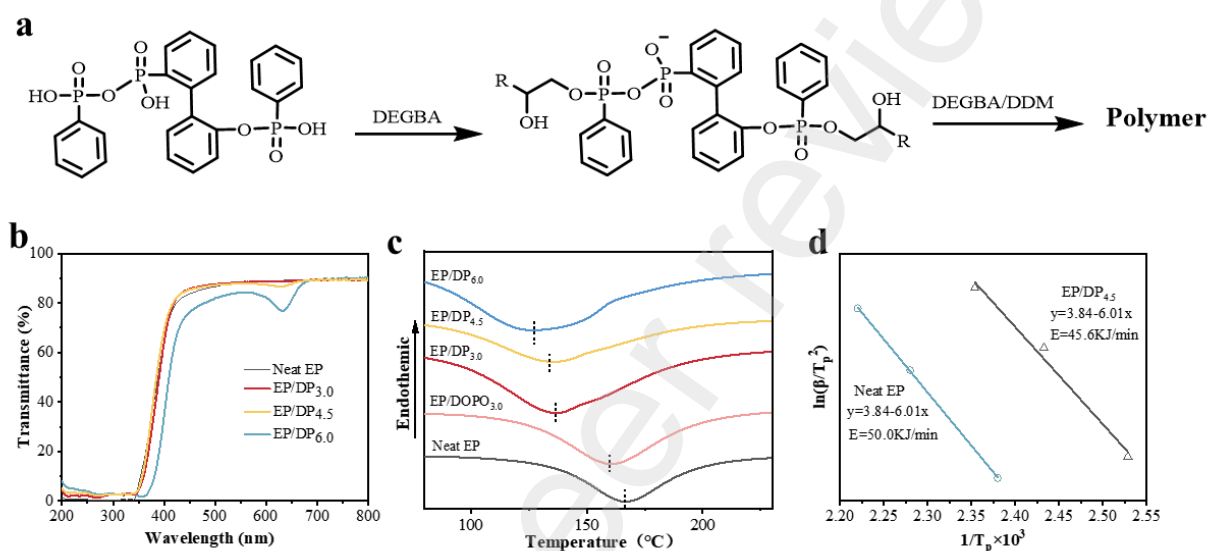
112 ^1H NMR and ^{31}P NMR were used to characterize the chemical environments of
113 the atoms within the DP molecule and the areas of the peaks corresponded to the
114 structural formulae of DP. In the ^{31}P NMR spectrum, only one absorption peak
115 appears due to the similarity of the chemical environment in which each phosphorus
116 atom in the DP molecule. Multiple peak analyses were reported as follows: ^1H NMR
117 (500 MHz, $\text{DMSO-}d_6$) δ 8.81 (d, $J = 58.9\text{ Hz}$, 2H), 8.37 – 6.78 (m, 18H), 3.00 – 2.64
118 (m, 1H). ^{31}P NMR (202 MHz, $\text{DMSO-}d_6$) δ 12.24. It is worth noting that trace PPOA
119 may form coordination products with H_2O , but this does not affect the excellent
120 overall performance of DP.

121 In order to further demonstrate the correctness of our analysis of the FTIR and
122 NMR spectra, we took the DMF solution of DP and carried out high resolution mass
123 spectrometry, which showed that the molecular weight results of DP corresponded to
124 its structural formula, thus proving the successful synthesis of DP.

125 3.2. Optical performance

126 Since DP liquid has good compatibility with the matrix materials, its introduction
127 does not significantly reduce the transparency of the EP, and the maximum visible
128 light transmission is higher than 90%, as observed in Fig 2b. at low DP addition
129 levels. However, when the addition amount reaches 6 wt%, the overall transmittance
130 decreases and is accompanied by the greenish phenomenon, which may be due to the

131 participation of DP in the curing reaction that affects the crosslinking network
 132 structure of EP to a relatively large extent. In addition, the material exhibits excellent
 133 overall UV shielding due to the fact that the aromatic structure promotes the
 134 absorption of UV light by EP[22][23], an advantage that makes EP/DP a potential
 135 candidate for use in electronic packaging applications[24].



136
 137 **Figure 2.** (a) Curing promotion mechanism of DP. (b) Optical performance of
 138 EP samples. (c) DSC curves of EP samples at a temperature increase rate of 10
 139 K/min. (d) Kissinger method of fitting curves for EP and EP/DP_{4.5}.

140 3.3. Curing Behavior analysis

141 Through DSC test (Fig 3c, 3d), we found that the exothermic peak temperature
 142 (T_p) of EP/DP was significantly reduced (from 166.7°C to 128°C) compared with that
 143 of Neat EP. Therefore, it is believed that the phosphate group affected by conjugation
 144 and induction, due to its improved nucleophilicity, can participate in and significantly
 145 promote the curing reaction (Fig 3a), shorten the curing time and reduce the energy
 146 consumption, which is favorable for the industrial production of FREP[25]. The
 147 Kissinger method provides empirical formulae commonly used to calculate the
 148 apparent activation energy (E), and the positive effect of the phosphate groups in DP

149 on the curing reaction is argued by calculating a certain degree of reduction in the E
150 value for EP/DP_{4,5}[26].

151 **3.3. Thermal Properties**

152 We mainly examine the heat resistance and thermal stability of EP by dynamic
153 thermo-mechanical analysis (DMA) and thermogravimetric analysis (TGA), seen in
154 Fig 4a-d. and Table 2 respectively, the heat resistance of EP was mainly characterized
155 based on T_g . It is obvious that the introduction of DOPO causes a deterioration in the
156 heat resistance of EP due to the plasticizing effect[27]. Compared to DOPO, the
157 addition of DP liquid does not adversely affect the heat resistance of EP. This is due
158 to the fact that DP unlock the large heterophenanthrene ring of DOPO, allowing it to
159 participate in the curing reaction to form a network structure and hindering the
160 relative movement between the molecular chains.

161 The cross-link density (V_e) of EP was calculated using the theoretical rubber
162 elasticity formula [25][28], and it was found that the introduction of DP could
163 significantly increase the V_e of EP, supporting our viewpoints above. In addition, the
164 rigidity of EP thermosets is generally characterized by the energy storage(E') modulus
165 at 50 °C. The high polarity of DP can shorten the spacing of the EP molecule chains,
166 thus increasing the slip resistance and improving the stiffness of the system[29].

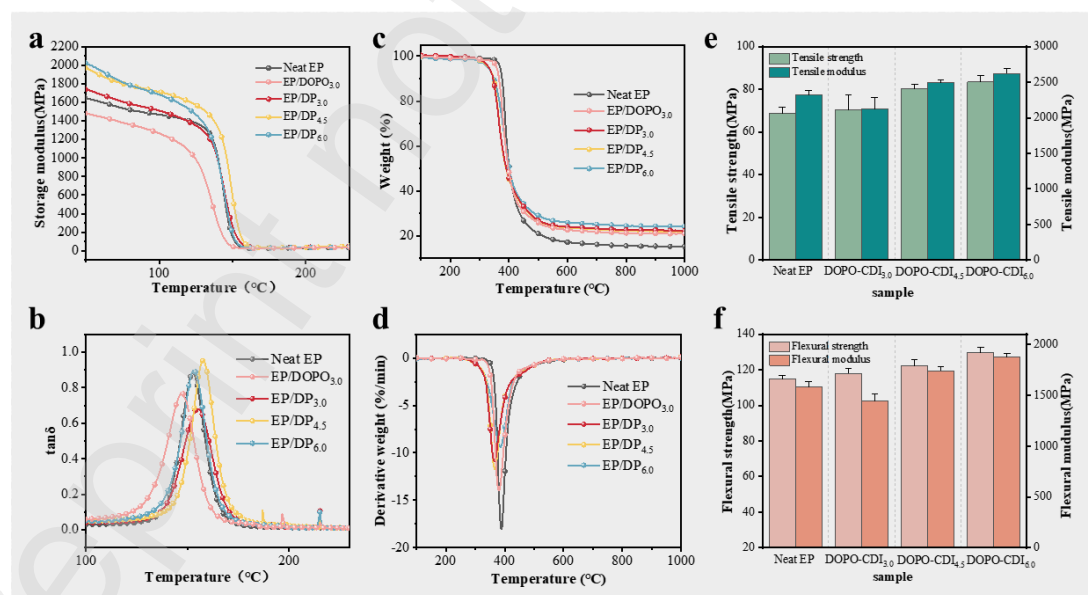
167 In the DTG test, it was observed from the test results that both DOPO and DP
168 advance the initial decomposition temperature ($T_{5\%}$) and the maximum mass loss
169 temperature (T_{Max}) of EP as a whole, it is a normal phenomenon of early
170 decomposition due to the introduction of weak bonds such as P-C and P-O
171 bonds[30][31]. We mainly used the maximum decomposition rate (R_{Max}) to
172 characterize the thermal stability of EP and found that the addition of DP liquid
173 resulted in a large reduction in R_{Max} . This is due to the fact that DP promotes charring
174 of EP and the phosphorus-containing graphitic layer formed on the air-exposed
175 surface can protect the substrate[6][32]. The large increase in thermal residual char

176 after the introduction of DP supports this viewpoint and it is worth noting that the
 177 slightly lower residual carbon in EP/DP_{4.5} compared to EP/DP_{3.0} may be due to the
 178 phosphorus effect (from 0.54 wt% to 0.81 wt%) insufficient to compensate for the
 179 effect of the reduction in cross-linking density and modulus on the thermal
 180 properties[25].

181 **Table 2. DMA and TGA Results of EP Thermosets**

| Sample | T _g (°C) | E' at 50°C(MPa) | V _e (mol/m ³) | R _{Max} (%/°C) | Char residue 1000°C(wt%) |
|------------------------|---------------------|-----------------|--------------------------------------|-------------------------|--------------------------|
| Neat EP | 153 | 1645 | 2572 | 18.1 | 15.2 |
| EP/DOPO _{3.0} | 147 | 1482 | 2579 | 14.0 | 20.4 |
| EP/DP _{3.0} | 155 | 1739 | 3203 | 10.9 | 22.3 |
| EP/DP _{4.5} | 158 | 1968 | 3157 | 11.7 | 21.8 |
| EP/DP _{6.0} | 157 | 1891 | 3087 | 9.4 | 24.2 |

182



183

184 **Figure 3.** (a) Curves of storage modulus and (b) loss modulus versus temperature. (c)

185 Curves of weight and (d) derivative weight as a function of temperature. (e) Tensile
186 and (f) Flexural Properties of EP Samples.

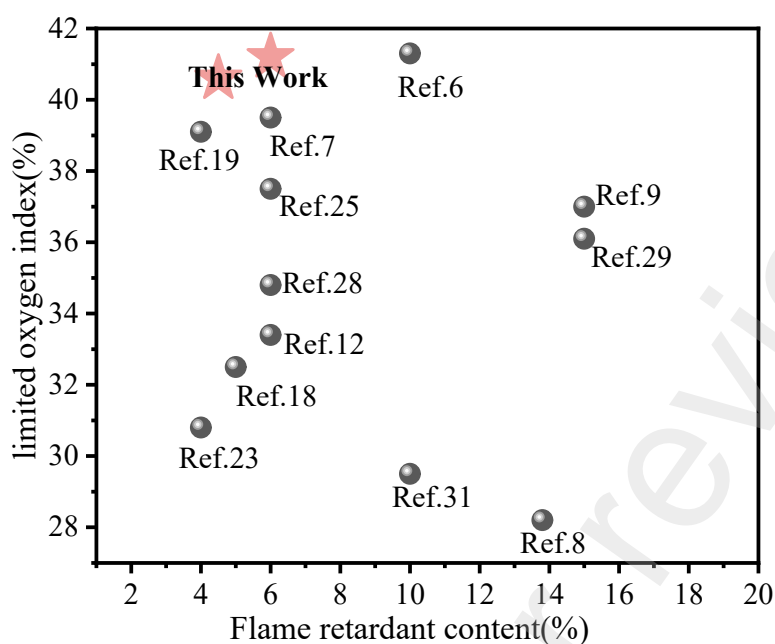
188 **3.4. Mechanical Properties**

189 Due to the good compatibility of DP with the matrix material, the introduction of
190 DP did not cause any deterioration in the mechanical properties, and the already
191 excellent mechanical properties of EP were further enhanced due to rigid matrix effect
192 and conjugation effect [33] [34]. The Fig 3e,3f. shows the results of our tests, where
193 the EP samples exhibit different levels of increase in each strength and modulus.

194 **3.5. Flame retardancy and combustion behavior of EP Thermosets**

195 Flame retardancy is one of the most valuable part of flame retarded epoxy (FREP),
196 however large amount of research based on FREPs is achieved by preparing flame
197 retardants with high flame retardancy efficiency or by adding a large amount of flame
198 retardant, which may result in a deterioration of the overall performance of the EP or
199 insufficient flame retardancy[1][35][36][37]. The high phosphorus content of DP liquid
200 (17.5wt%) addresses these potential issues and is an example of how flame retardants
201 can be added at low levels to achieve excellent flame retardancy and overall
202 performance.

203 As shown in Table 3, Neat EP has the worst flame retardancy and fails the vertical
204 flame test (UL-94), while after the introduction of DOPO, the flame retardancy
205 improves slightly but still fails to meet the UL-94 V-0 rating, with the deteriorating of
206 the overall properties. With the introduction of DP liquid, EP's limiting oxygen index
207 (LOI) increased dramatically, and can pass the UL-94 V-0 rating, only 6wt% can be
208 added to reach 41.2%LOI, the very high flame retardant efficiency of DP is attributed
209 to the high phosphorus content of DP liquid and the combined vapor phase[38] and
210 condensed phase[16] flame retardancy based on DOPO and PPOA. In addition, we
211 compare the flame retardant efficiencies of some of the excellent work cited in this
212 article with DP by means of scatter plots to intuitive arguments (Fig 4.).



213

214 **Figure 4.** Scatter Plot of Flame Retardant Efficiency Comparison of Flame
 215 Retardants.

216 **Table 3. Flame retardancy of EP Thermosets**

| Sample | P(wt%) | LOI(%) | UL-94 | Dripping |
|------------------------|--------|--------|-------|----------|
| Neat EP | 0 | 26.4 | NR | Yes |
| EP/DOPO _{3.0} | 0.43 | 32.6 | V-1 | No |
| EP/DP _{3.0} | 0.54 | 36.8 | V-0 | No |
| EP/DP _{4.5} | 0.81 | 40.6 | V-0 | No |
| EP/DP _{6.0} | 1.09 | 41.2 | V-0 | No |

217 Cone calorimetry test is used to simulate the combustion behavior of the samples
 218 under real fire conditions, and we have summarized the test results in **Table 4 and Fig**
 219 **5.** First, the time to ignition (TTI) shows an overall decrease with the addition of
 220 phosphorus-containing compounds, which is similar to the decrease in decomposition

221 temperatures in subsection 3.3, and is interpreted as the introduction of weak bonds to
222 promote early decomposition of the samples.

223 Peak heat release rate (PHRR) and total heat release rate (THR) are key
224 parameters used to measure the burning intensity of samples, the addition of DOPO
225 only slightly reduces the burning intensity[39], this is mainly due to the lack of
226 condensed phase flame retardant capability of DOPO[40], while DP strongly inhibits
227 the burning exotherm, the addition of only 6 wt% can reduce PHRR and THR by
228 52.4% and 45.2% respectively, which greatly improves the fire safety of EP.

229 The increase in the average carbon monoxide yield (Av-COY) and decrease in
230 the average carbon dioxide yield (Av-CO₂Y) with the introduction of DP indicates
231 incomplete combustion of FREP is intensified[41][42], which is attributed to the
232 excellent gas-phase flame retardancy of DP, allowing phosphorus-containing free
233 radicals generated by thermal decomposition effectively quench hydroxyl radicals
234 generated by combustion, thereby blocking the chain reaction of combustion.

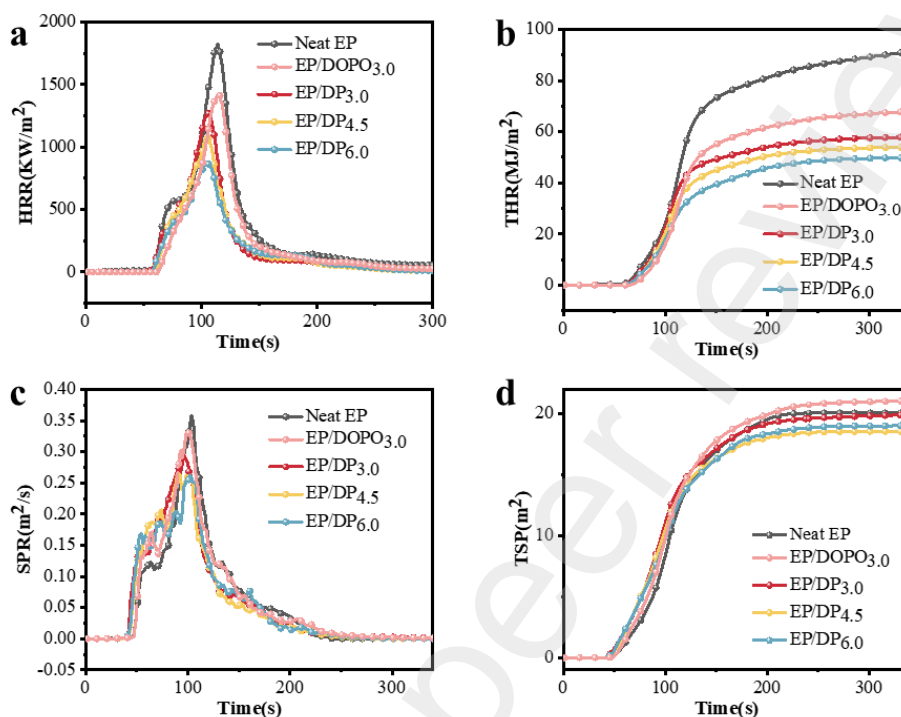
235 Surprisingly, the smoke inhibition effect of DP is not obvious, similar to that of
236 DOPO, and we suspect the main reason is that the flame retardant element of DP
237 liquid is single and the amount added is small. Therefore, the introduction of more
238 and suitable secondary flame retardants elements will be the main objective of the
239 next phase of our work.

240 **Table 4. combustion behavior of EP Thermosets**

| Sample | Neat EP | EP/DOPO _{3.0} | EP/DP _{3.0} | EP/DP _{4.5} | EP/DP _{6.0} |
|-----------------------------|---------|------------------------|----------------------|----------------------|----------------------|
| TTI(s) | 50 | 46 | 43 | 42 | 47 |
| PHRR(KW/m ²) | 1822.8 | 1416.2 | 1269.1 | 1079.2 | 867.6 |
| THR(MJ/m ²) | 91.3 | 69.4 | 58.2 | 54.3 | 50.0 |
| Av-COY(kg/kg) | 0.089 | 0.084 | 0.097 | 0.101 | 0.097 |
| Av-CO ₂ Y(kg/kg) | 2.16 | 1.44 | 1.37 | 1.31 | 1.56 |

| | | | | | |
|-------------------------|------|------|------|------|------|
| PSPR(m ² /s) | 0.36 | 0.29 | 0.26 | 0.20 | 0.33 |
| TSP(m ²) | 20.0 | 21.1 | 19.9 | 18.5 | 19.0 |

241



242

243 **Figure 5.** (a)HRR. (b)THR. (c)SPR. (d)TSP curves of EP thermosets obtained
244 from cone calorimetry.

245 3.6. Condensed phase analysis

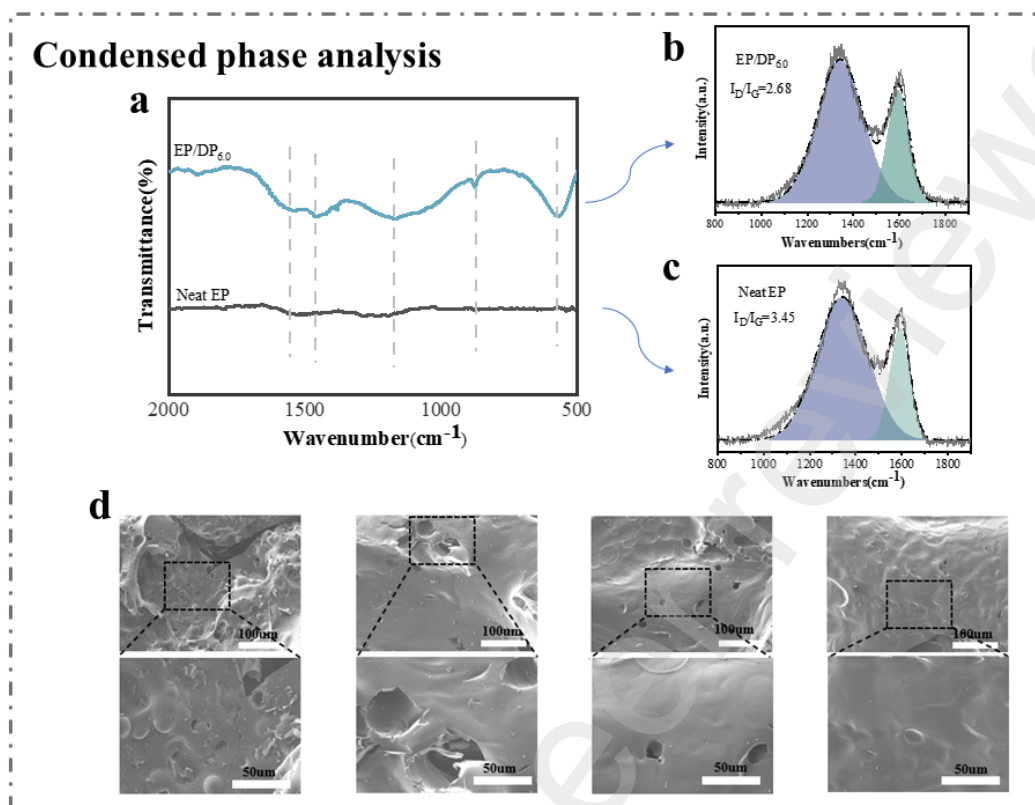
246 In order to investigate the flame-retardant mechanism of DP based on the
247 condensed phase, we selected the most completely burnt part of sample after the cone
248 calorimetry test to perform a series of tests. First, we performed FTIR test on the
249 residual char(Fig 6a.), and it can be clearly observed that the residual char produced by
250 Neat EP has weak absorption peaks only in the region of the benzene ring. In contrast,
251 EP/DP_{6.0} has prominent characteristic peaks of the benzene ring (1560 cm⁻¹, 1470 cm⁻¹) [41], while 1180 cm⁻¹ and 880 cm⁻¹ are attributed to P=O and P-O, respectively [42]
252 [43], in addition to the broad peak at 575 cm⁻¹, which is the absorption peak for the
253 formation of chemical bonds between elemental H and C or P. It is shown that the
254

255 introduction of DP can assist EP to construct a phosphorus-containing graphite layer
256 during the combustion process.

257 In order to further characterise the degree of graphitisation of our prepared FREP,
258 we performed Raman spectroscopy tests(Fig 6b, 6c.), and the double peaks in the
259 spectrum are the D-band (1339 cm⁻¹) and the G-band (1584 cm⁻¹), and their intensities
260 (ID, IG) were used to characterise the amount of amorphous and graphitised carbon,
261 respectively, and it can be observed that the ID/IG decreases significantly with the
262 introduction of DP[46], which further suggests that the cohesion of the DP phase flame
263 retardant effect is substantial.

264 We visualised the micromorphology of the EP samples by scanning electron
265 microscopy (Fig 6d.) and observed that the residual char produced by the combustion
266 of Neat EP was loose and full of holes, and therefore could not shield the exothermic
267 heat of combustion and protect the substrate as well. With the introduction of DP, the
268 residual carbon of EP became dense and flat, and the combustion exotherm was
269 suppressed. The above demonstrates the viewpoint about the excellent condensed phase
270 flame retardant effect of DP.

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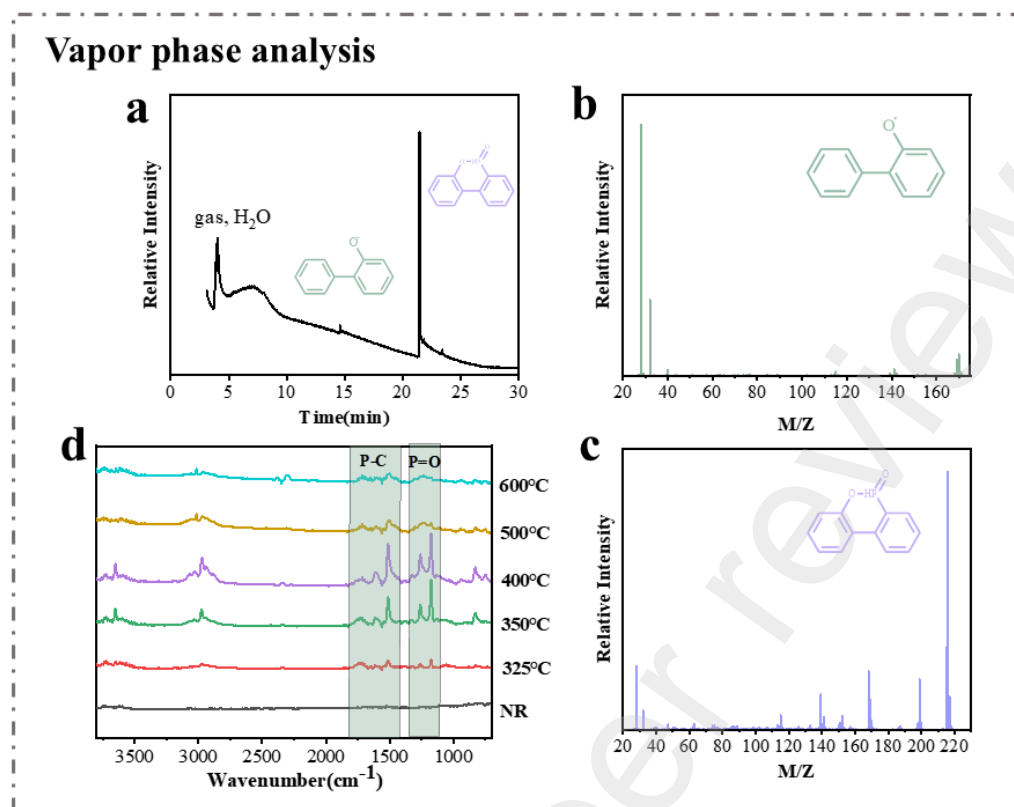
274 **Figure 6.** (a) FTIR of EP/DP_{6.0} and Neat EP combustion residues. (b) Raman
275 spectral fitting curve of EP/DP_{6.0} and (c) Neat EP. (d) Microscopic morphology of
276 combustion residues of EP samples (100x and 270x).

277

278 **3.7 Vapor phase analysis**

279 The vapor phase flame retardant effect of DP was investigated by Py-GC/MS and
280 TG-IR. It can be observed by Fig 7a-c that the vapor phase products of DP thermally
281 cracked under nitrogen atmosphere are relatively homogeneous, mainly consisting of
282 DOPO fragments, radicals, water and gases, which is attributed to the ability of PPOA
283 fragments to promote dehydration and catalytic charring [47][48], and the formation of
284 DOPO by thermal dehydration of HPPA is the main reason for the flame retardant effect
285 of DP in the vapor phase.

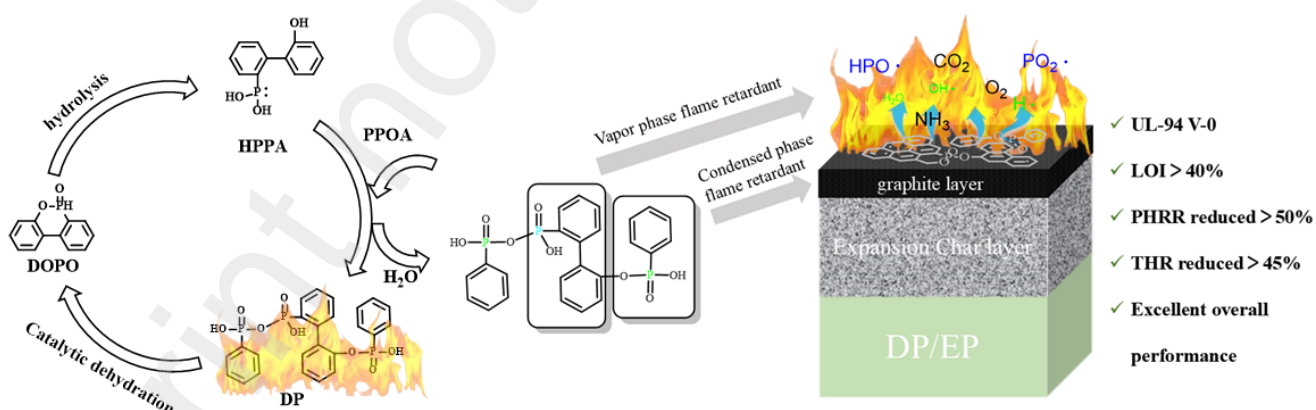
286 We further investigated the vapor phase flame retardant mechanism of DP by TG-
287 IR and observed from Fig 7d. that in addition to water and alkanes, a large amount of
288 phosphorus-containing substances are released from EP/DP_{6.0} at high temperatures,
289 such as fragments containing P-C (1515cm^{-1}) and P=O (1260cm^{-1}) captured by
290 FTIR[6][49], which are eventually converted into phosphorus-containing radicals at
291 elevated temperatures and play the role of quenching combustion radicals and
292 interrupting the chain reaction of combustion, thus reducing the intensity of combustion,
293 which reduce the intensity of combustion. Finally, we summarize the design concept
294 and mechanism of action of DP in Fig 8.



295

296 **Figure 7.** (a)Thermal cleavage Py-GC/MS spectra of DP. (b)Partial radical
 297 fragments and (c)DOPO fragments from thermal cleavage. (d)TG-IR spectrum of
 298 EP/DP_{6.0}.

299



Due to the excellent catalytic charring ability of PPOA, DP is able to re-form DOPO when heated, thus avoiding the adverse effect of DOPO on the material performances while providing the gas-phase flame retardant effect of DOPO.

Figure 8. DP design concept and mechanism of action.

301 **4. CONCLUSIONS**

302 This work proposes a novel flame retardant precursor, HPPA, obtained by
303 hydrolysis of DOPO. Our HPPA-based liquid flame retardant DP is structurally similar
304 to EP, which is easier to dissolve in EP monomers and form chemical bonds with EP,
305 thus obtaining excellent processing, thermal and mechanical properties.

306 The most attractive feature of DP is its excellent flame retardancy, it has both gas
307 phase and condensed phase flame retardancy based on HPPA fragments and PPOA
308 fragments, and has a phosphorus content up to 17.5wt%, which makes it achievable to
309 obtain excellent flame retardancy by adding only 6wt% of DP to EP, with its LOI
310 reaching over 40% and its PHRR and THR being reduced by 52.4% and 45.2%
311 respectively. We believe that DP is expected to replace DOPO and become widely used
312 in the epoxy resin industry.

313 **Data Availability Statement**

314 The data presented in this study are available on request from the corresponding
315 author.

316 **Conflicts of Interest:**

317 The authors declare no conflict of interest.

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- 454

Table 1. The formulations of epoxy thermosets

| Sample | DGEBA(wt %) | DDM(wt%) | DP(wt%) | P(wt%) |
|------------------------|-------------|----------|---------|--------|
| Neat EP | 80 | 20 | 0 | 0 |
| EP/DOPO _{3.0} | 77.6 | 19.4 | 3.0 | 0.43 |
| EP/DP _{3.0} | 77.6 | 19.4 | 3.0 | 0.53 |
| EP/DP _{4.5} | 76.4 | 19.1 | 4.5 | 0.79 |
| EP/DP _{6.0} | 75.2 | 18.8 | 6.0 | 1.05 |

Table 2. DMA and TGA Results of EP Thermosets

| Sample | T _g (°C) | E' at 50°C(MPa) | V _e (mol/m ³) | R _{Max} (%/°C) | Char residue 1000°C(wt%) |
|------------------------|---------------------|-----------------|--------------------------------------|-------------------------|--------------------------|
| Neat EP | 153 | 1645 | 2572 | 18.1 | 15.2 |
| EP/DOPO _{3.0} | 147 | 1482 | 2579 | 14.0 | 20.4 |
| EP/DP _{3.0} | 155 | 1739 | 3203 | 10.9 | 22.3 |
| EP/DP _{4.5} | 158 | 1968 | 3157 | 11.7 | 21.8 |
| EP/DP _{6.0} | 157 | 1891 | 3087 | 9.4 | 24.2 |

Table 3. Flame retardancy of EP Thermosets

| Sample | P(wt%) | LOI(%) | UL-94 | Dripping |
|------------------------|--------|--------|-------|----------|
| Neat EP | 0 | 26.4 | NR | Yes |
| EP/DOPO _{3.0} | 0.43 | 32.6 | V-1 | No |
| EP/DP _{3.0} | 0.54 | 36.8 | V-0 | No |
| EP/DP _{4.5} | 0.81 | 40.6 | V-0 | No |
| EP/DP _{6.0} | 1.09 | 41.2 | V-0 | No |

Table 4. combustion behavior of EP Thermosets

| Sample | Neat EP | EP/DOPO _{3.0} | EP/DP _{3.0} | EP/DP _{4.5} | EP/DP _{6.0} |
|-----------------------------|---------|------------------------|----------------------|----------------------|----------------------|
| TTI(s) | 50 | 46 | 43 | 42 | 47 |
| PHRR(KW/m ²) | 1822.8 | 1416.2 | 1269.1 | 1079.2 | 867.6 |
| THR(MJ/m ²) | 91.3 | 69.4 | 58.2 | 54.3 | 50.0 |
| Av-COY(kg/kg) | 0.089 | 0.084 | 0.097 | 0.101 | 0.097 |
| Av-CO ₂ Y(kg/kg) | 2.16 | 1.44 | 1.37 | 1.31 | 1.56 |
| PSPR(m ² /s) | 0.36 | 0.29 | 0.26 | 0.20 | 0.33 |
| TSP(m ²) | 20.0 | 21.1 | 19.9 | 18.5 | 19.0 |