



# HCCI Engine: Numerical and Experimental Approach

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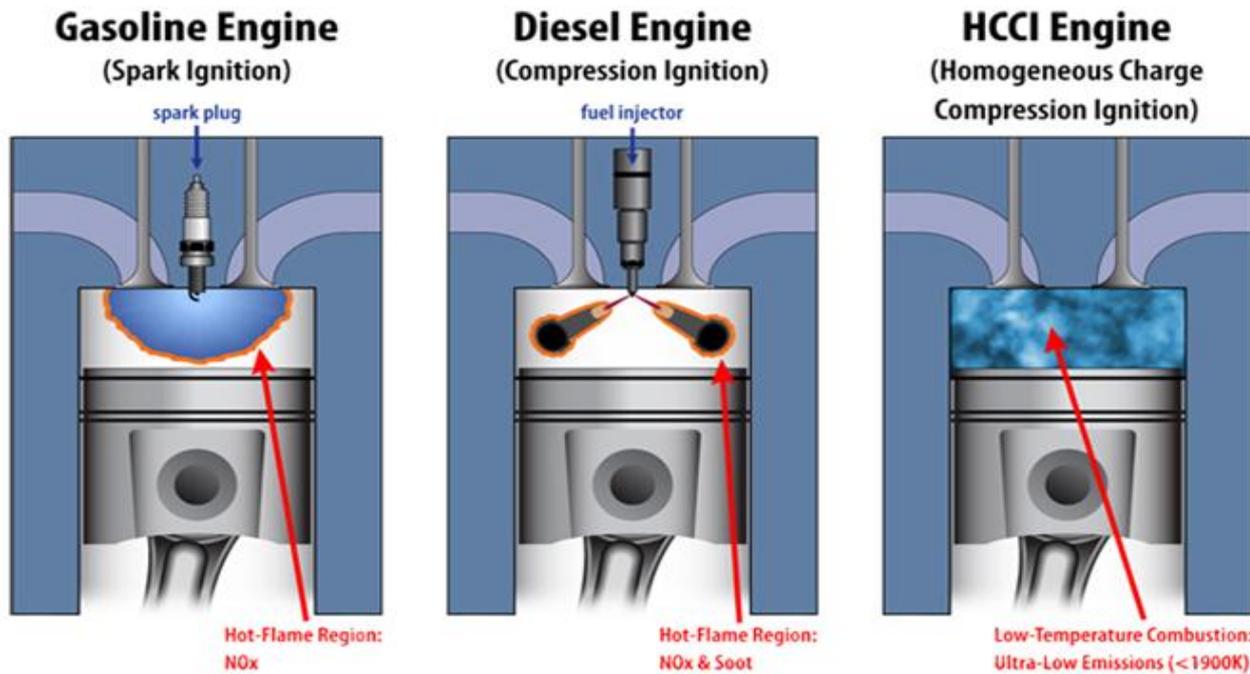
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- Introduction
- Numerical Approach
  - Model formulation
  - Results and analysis
- Experimental Approach
  - Engine Diagram
  - Preliminary test
- Conclusion

- What is HCCI engine?
  - It stands for Homogeneous Charge Compression Ignition engines.
  - First research was started by Onishi et al. in 1979.
  - This engine has been investigated worldwide as this technology has not matured sufficiently.
  - It could be used in either SI or CI configurations with high compression ratio (CR)
  - In principle, there is no spark plug or injector inside the combustion chamber like SI or CI engines to control the combustion: auto-ignition occurs in multiple spots once the mixture has reached its chemical activation energy.

# Introduction

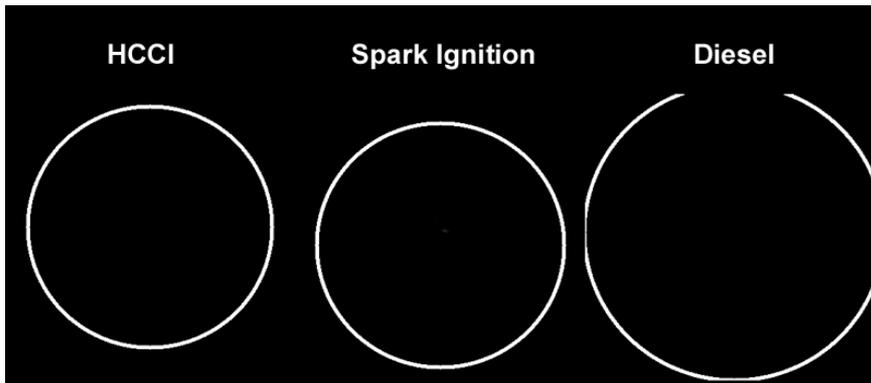
- What is the difference?
  - SI engines: Requires spark plug and low CR
  - CI engines: Requires fuel injector and high CR
  - HCCI engines: Without spark plugs or fuel injectors. Can be configured using CI or SI mode with high CR – leads to high engine efficiency with low emissions level.



Source: Lawrence Livermore National Laboratory, [https://www-pls.llnl.gov/?url=science\\_and\\_technology-chemistry-combustion](https://www-pls.llnl.gov/?url=science_and_technology-chemistry-combustion)

# Introduction

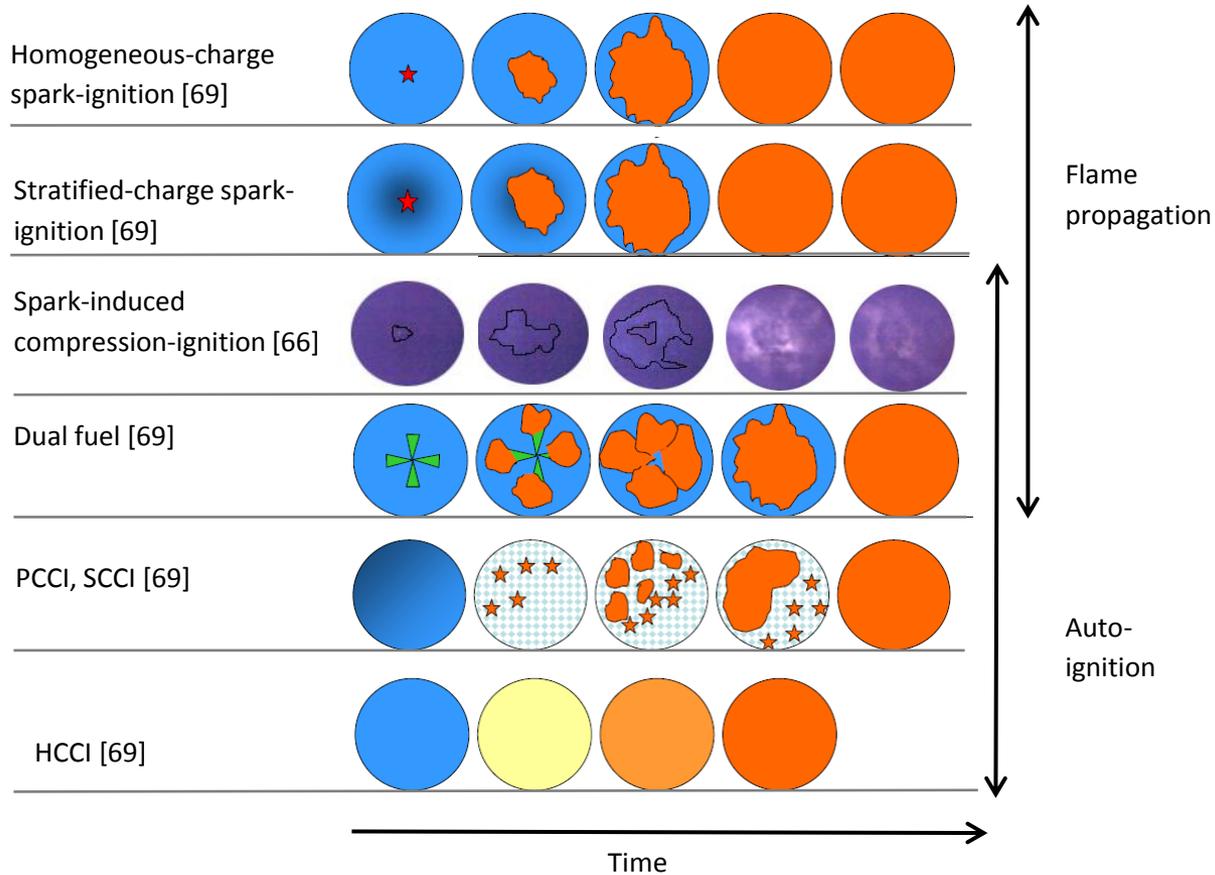
- Combustion behaviour:
  - SI engines: It has flame propagation with longer combustion period
  - CI engines: Auto-ignite when the fuel is injected into hot compressed air
  - HCCI engines: Auto-ignite in multiple spots instantaneously with fast combustion period



Source: Engine Research Centre, University of Wisconsin,  
<http://www.erc.wisc.edu/combustion.php>

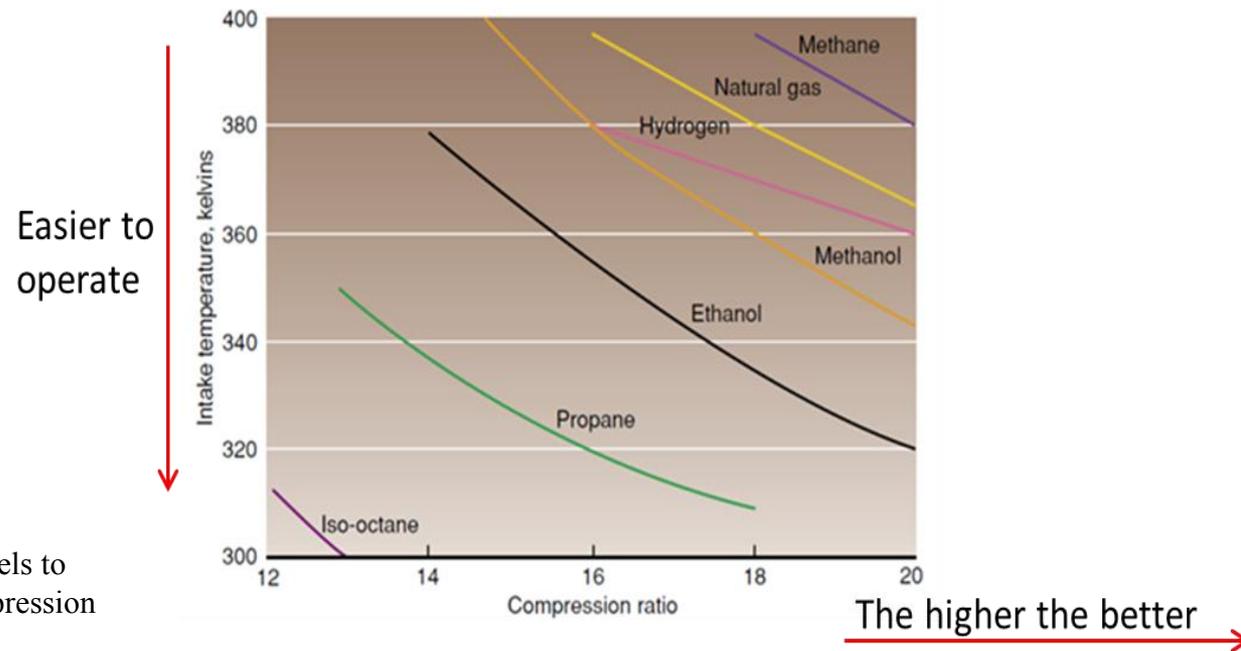


## ■ Homogeneous charge engine types



# Introduction

- HCCI engines can operate using any type of fuels as long as the fuel can be vaporized and mixed with air before the ignition.
- Fuel auto-ignition point is important to look at in order to get smooth engine operation: Different fuels will have different auto-ignition points as shown in below figure.



**Figure** Intake temperatures required for fuels to operate under HCCI mode with various compression ratios (Aceves & Flowers 2004).

## ■ HCCI advantages:

- High engine efficiency relative to SI engines by employing high CR and fast combustion [2,3].
- Ability to operate using a wide range of fuels [4].
- Can be implemented in any engine configuration: automobile engines, stationary engines, high load engines or small size engines [5,6]

## ■ HCCI disadvantages:

- Difficulties in controlling the auto-ignition and heat release rate at high load operation and achieving cold start [7,8].
- Knocking due to sudden onset of the combustion behaviour, which reduces engine reliability due to high vibration effects: produces pinging sound which can be heard outside.

## ■ HCCI challenge:

- To control the auto-ignition timing of the mixture because there is no spark plug or fuel injector to control the start of the combustion.
- To achieve cold start.
- To meet emission standards.
- To control knock.

- **Zero-Dimensional Model without Turbulence and Mixing Models**

# Model Formulation



## ■ Conservation of mass:

- $\frac{dm}{dt} = \sum_j \dot{m}_j$

## ■ Conservation of species:

- An n-heptane reduced chemical reaction mechanism was used [13].
- The properties are similar to conventional diesel (e.g. cetane number)
- Consists of 160 species and 770 elementary reactions

- $\frac{dY_i}{dt} = \frac{\dot{\omega}_i W_i}{\rho}, i = 1, \dots, n$

## ■ Gas exchange process:

- A gas exchange process takes place when inlet or exhaust valve is open.
- One-dimensional, steady state, isentropic flow is used to model the process [16].

## ■ Conservation of energy:

- The equation was derived from the first law of thermodynamics for an open system to get the change in temperature.

- $$\frac{dT}{dt} = \frac{1}{c_p - \frac{Pv}{T}} \left[ - \left( \sum H_i - \frac{Pv \sum_i R_{u/W}}{R_{u/W}} \right) \frac{dY_i}{dt} - \frac{\dot{m}}{m} (h_j - Pv) + \frac{1}{m} \left( \sum \dot{m}_j h_j - P \frac{dV}{dt} + \frac{dQ}{dt} \right) \right]$$

- Where the pressure was calculated using the ideal gas law equation:

- $$P = \rho T \frac{R_u}{W}$$

## ■ Heat transfer:

- Heat is transferred to the wall through convection and radiation.
- Radiation heat transfer on HCCI engines is neglected because the effect is very small, due to low soot and low temperature combustion [14,15]
- The modified Woschni equation by Chang et al. [14] was used.

# Results and Analysis

## ■ Validation

- The model was validated against numerical and experimental data from Guo et al. [17]: the fuel was injected at inlet manifold.
- To account for mixing effects: the effective intake temperature was set 20°C higher than the intake temperature [17].

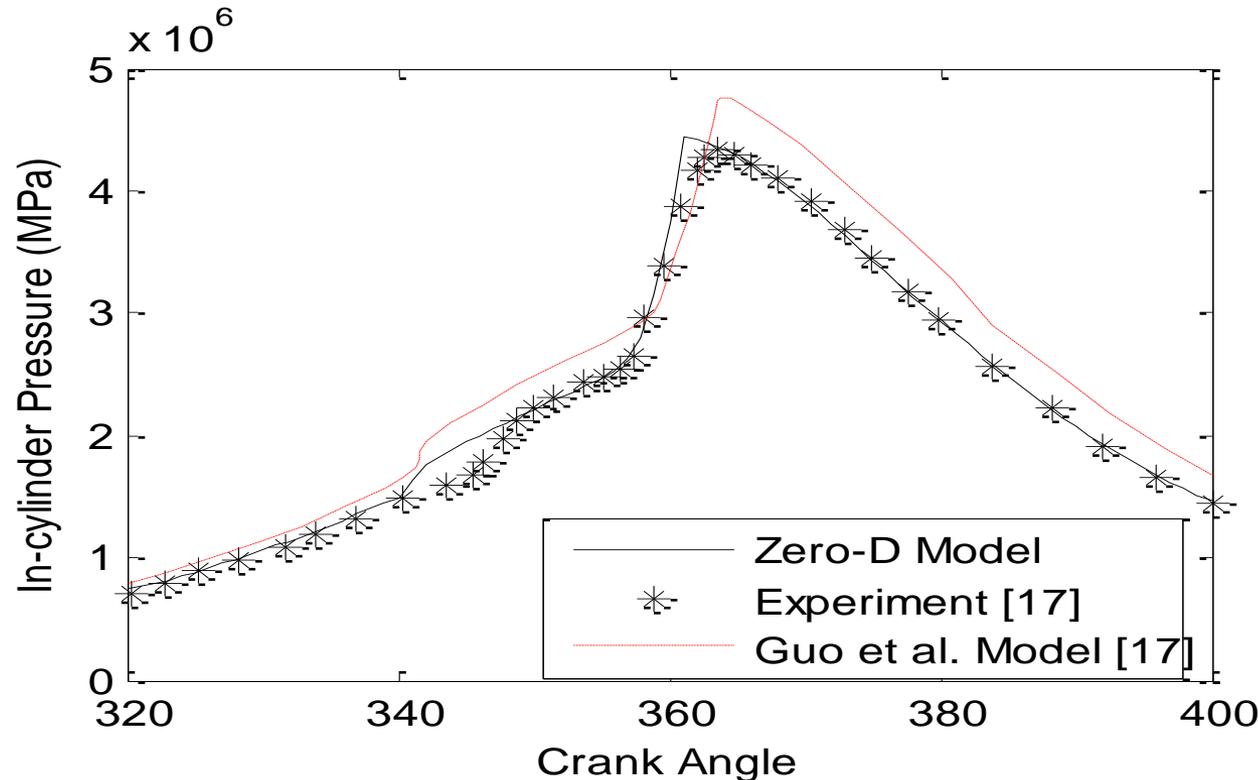
Table 1 Engine parameter used in the simulation [17]

<b>Cylinder bore</b>	82.55 mm
<b>Stroke</b>	114.3 mm
<b>Connecting rod length</b>	254 mm
<b>Compression ratio</b>	10
<b>Engine speed</b>	900 rpm
<b>Inlet valve open (IVO)</b>	10° CA ATDC
<b>Inlet valve closed (IVC)</b>	36° CA ABDC
<b>Exhaust valve open (EVO)</b>	40° CA BBDC
<b>Exhaust valve closed (EVC)</b>	5° CA ATDC

# Results and Analysis

## Validation

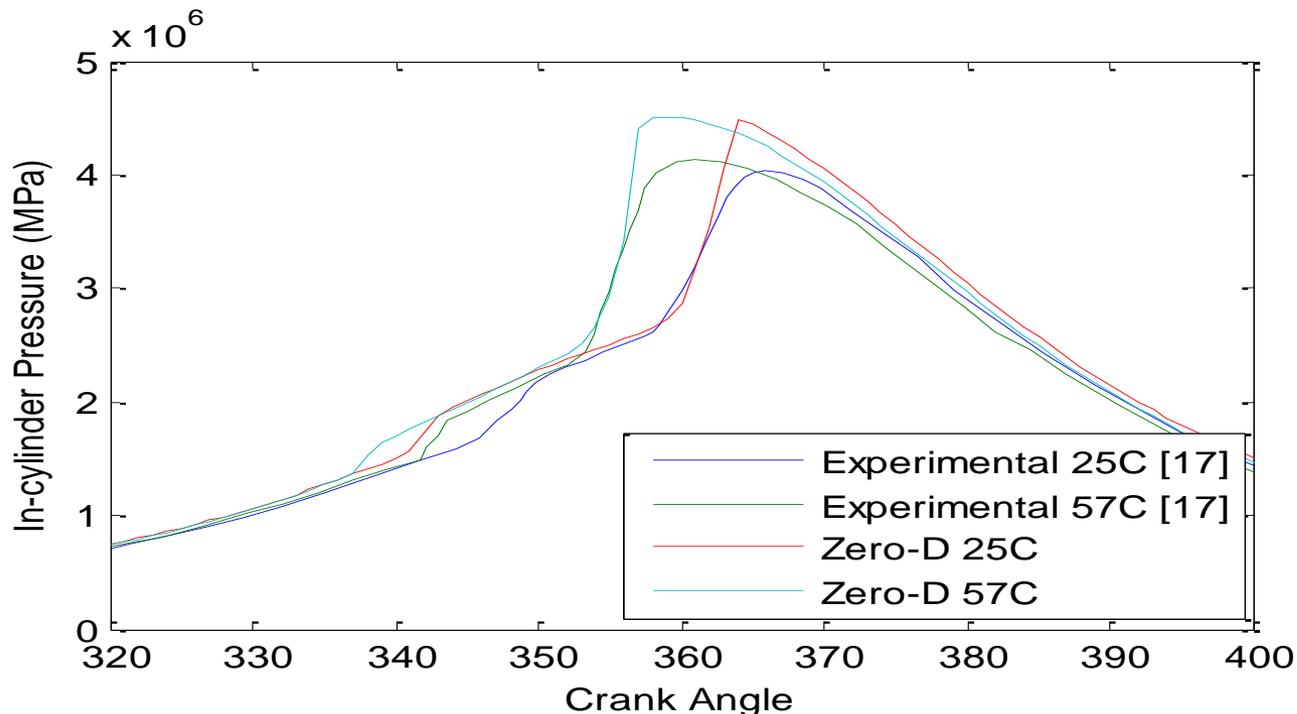
- The comparison between experimental and numerical data from Guo et al. [17] with the zero-dimensional model. The combustion phasing is in good agreement with the experimental data.



**Figure 1** Comparison between single-zone zero-dimensional model with experiment and another single-zone model using modified Woschni heat transfer model [17]. CR=10.0, N=900 rpm,  $T_{in}=40^{\circ}\text{C}$ ,  $P_{in}=95$  kPa, AFR=50.

# Results and Analysis: Effect of intake temperature

- Auto-ignition can be advanced once the intake temperature is increased.
- Results from the current simulation were compared with experimental results [17] in Fig. 2(a) to validate the model over different operating temperatures: The results agreed well as did in Fig. 1.

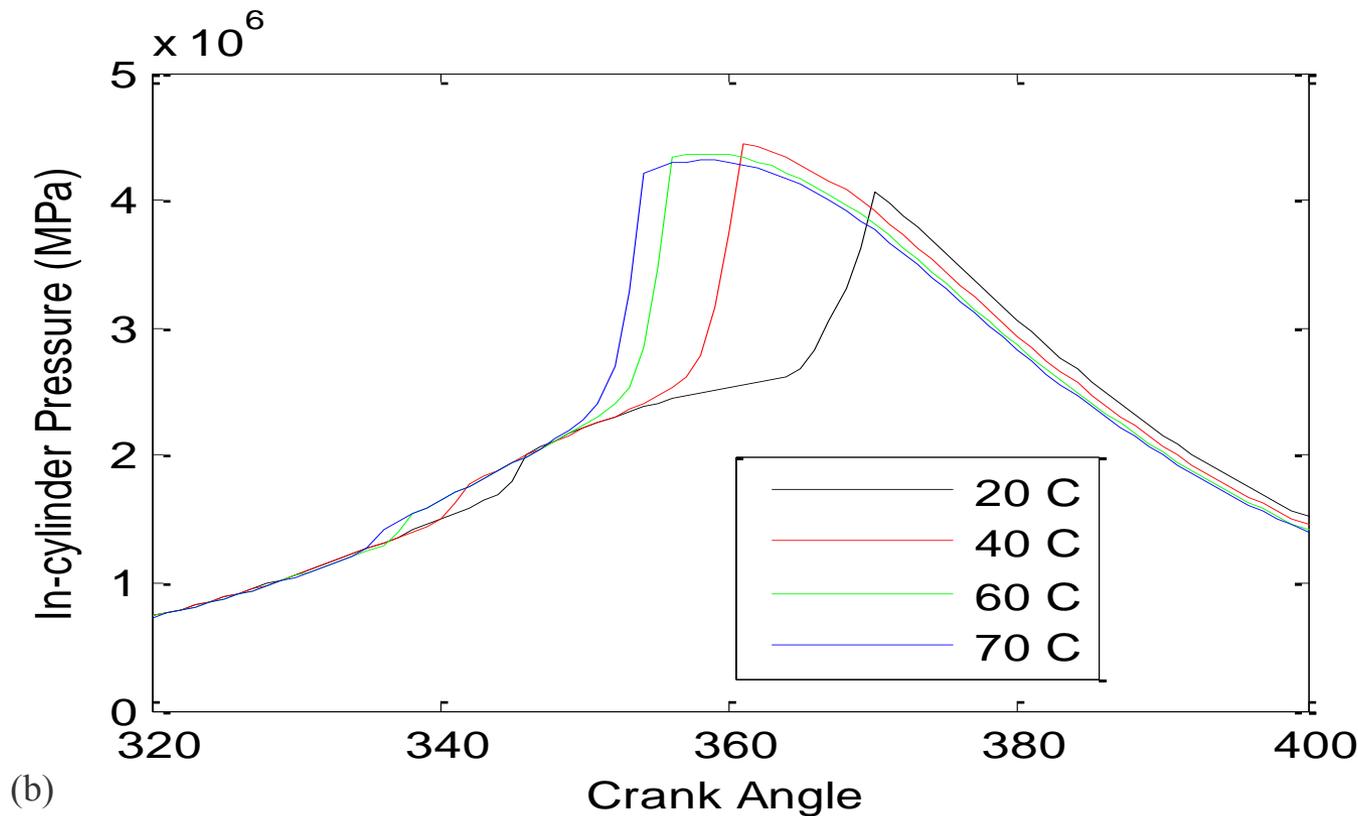


**Figure 2** Effect of intake temperature on the in-cylinder pressure: CR=10.0, N=900 rpm,  $P_{in}$ =95 kPa, AFR=50 (a) Validated varying intake temperature.

(a)

# Results and Analysis: Effect of intake temperature

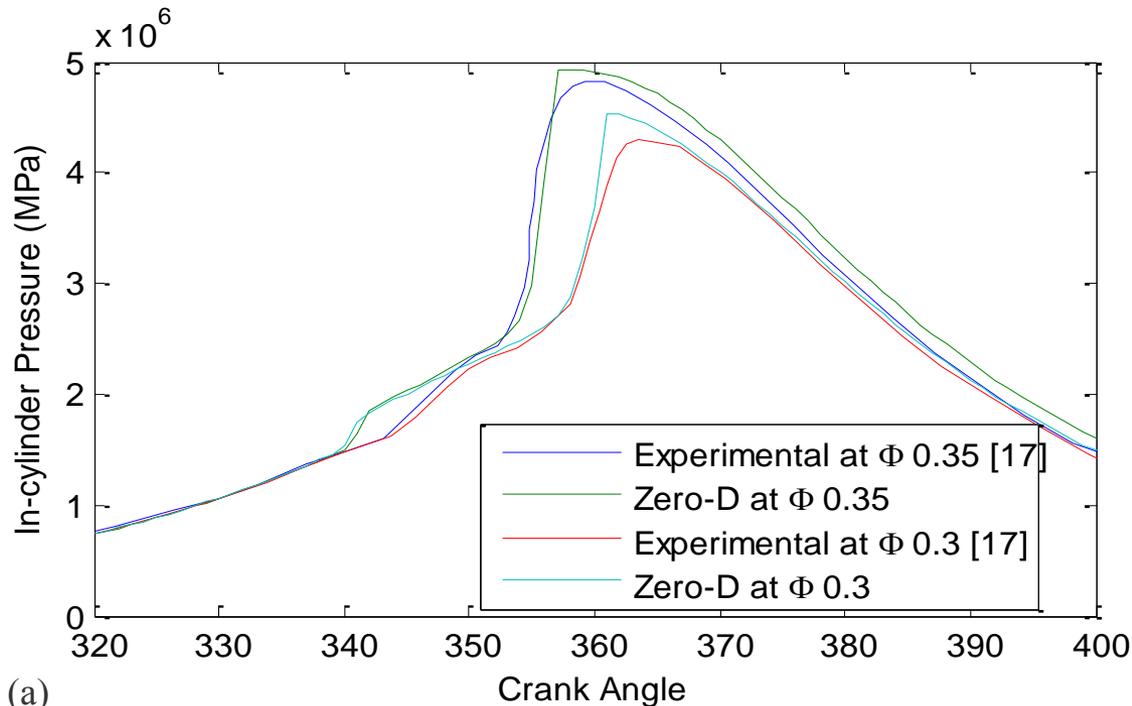
- The predicted in-cylinder peak pressure starts to decrease even though the auto-ignition is advanced (Fig 2b).



**Figure 2** Effect of intake temperature on the in-cylinder pressure: CR=10.0, N=900 rpm,  $P_{in}=95$  kPa, AFR=50 (b) Predicted in-cylinder pressure trend.

# Results and Analysis: Effect of equivalence ratio

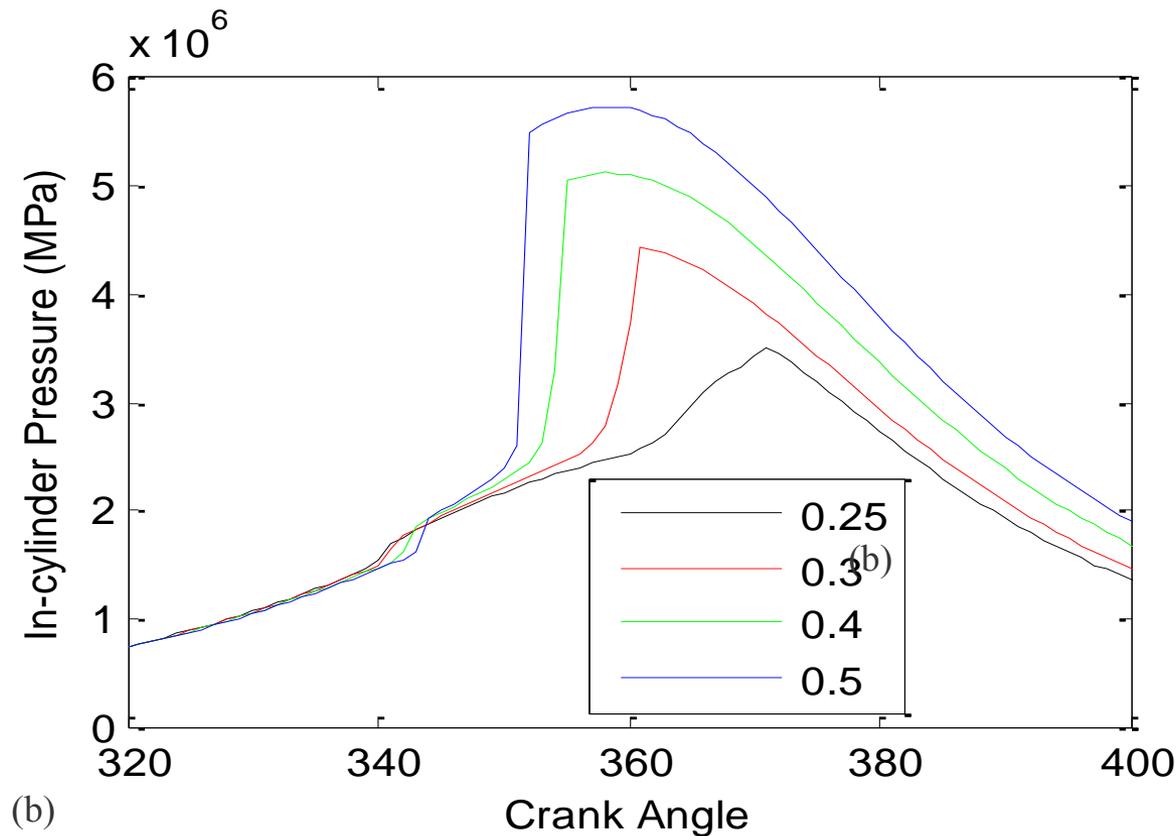
- The equivalence ratio ( $\Phi$ ) is a measure of how much fuel and air is being consumed in the combustion chamber.
- Figure 3(a) shows validated result of different equivalence ratios compared to the experiment, again showing good agreement.



**Figure 3** Effect of equivalence ratio on the in-cylinder pressure: CR=10.0, N=900 rpm,  $T_{in}=40^{\circ}\text{C}$ ,  $P_{in}=95$  kPa (a) Validated varying equivalence ratio.

# Results and Analysis: Effect of equivalence ratio

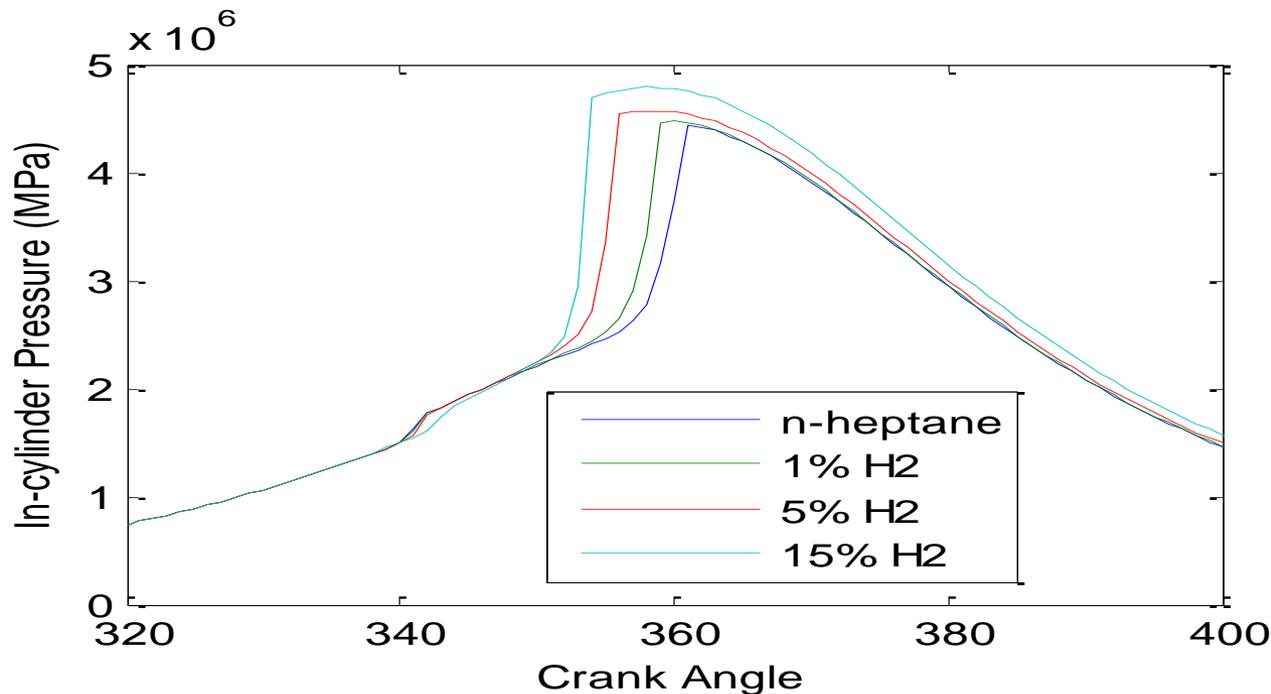
- The in-cylinder peak pressure trend keeps increasing with increasing equivalence ratio: will create knocking.



**Figure 3** Effect of equivalence ratio on the in-cylinder pressure:  
CR=10.0, N=900 rpm,  
 $T_{in}=40^{\circ}\text{C}$ ,  $P_{in}=95\text{ kPa}$  (b)  
Predicted in-cylinder pressure trend.

# Results and Analysis: Effect of hydrogen addition

- Effective way to reduce ignition delay and improves engine efficiency [19].
- Too much hydrogen will create knocking: the energy ratio should be less than 15% [20].
- The auto-ignition point is advanced significantly with 1% hydrogen and the in-cylinder peak pressure keeps increasing with increasing hydrogen content.



**Figure 4** Predicted effect of hydrogen addition on the in-cylinder pressure for fixed n-heptane injection: CR=10.0, N=900 rpm,  $T_{in}=40^{\circ}\text{C}$ ,  $P_{in}=95\text{ kPa}$

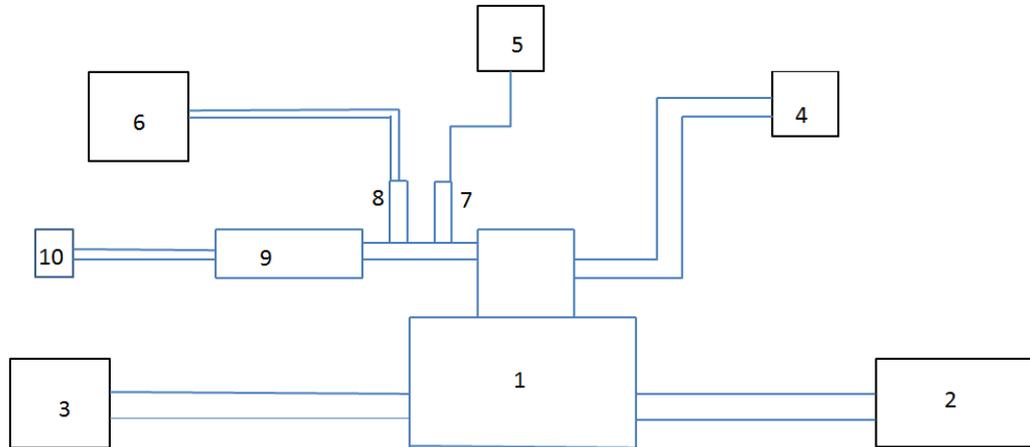
# Experimental Approach



- Engine: Single cylinder SI engine to be converted to HCCI engine
- External heater to be installed on the intake air manifold
- Hydrogen will be added later on: if the time like us!

# Experimental Approach

## ■ Engine diagram



1 Engine

2 Dynamometer

3 Data logger

4 Fuel tank

5 ECU

6 Hydrogen electrolyser

7 Fuel injector

8 Hydrogen injector

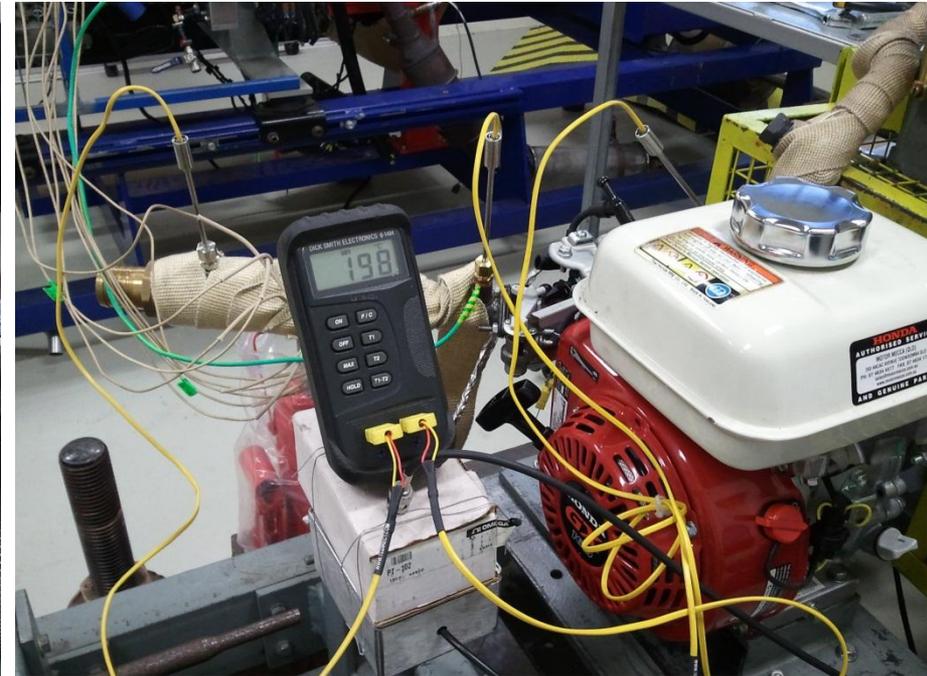
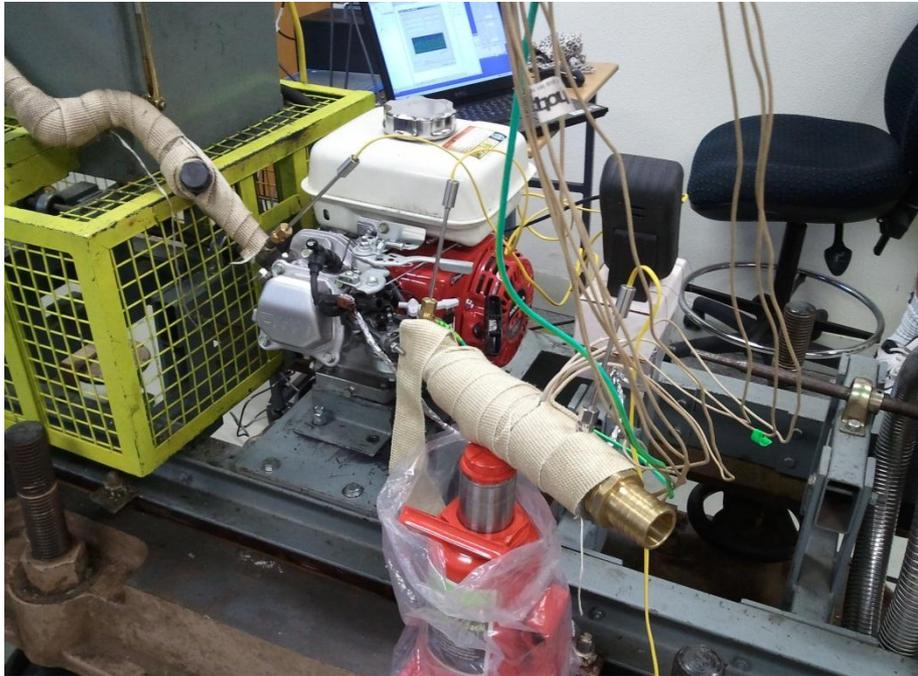
9 Air intake heater

10 Airflow meter

# Experimental Approach

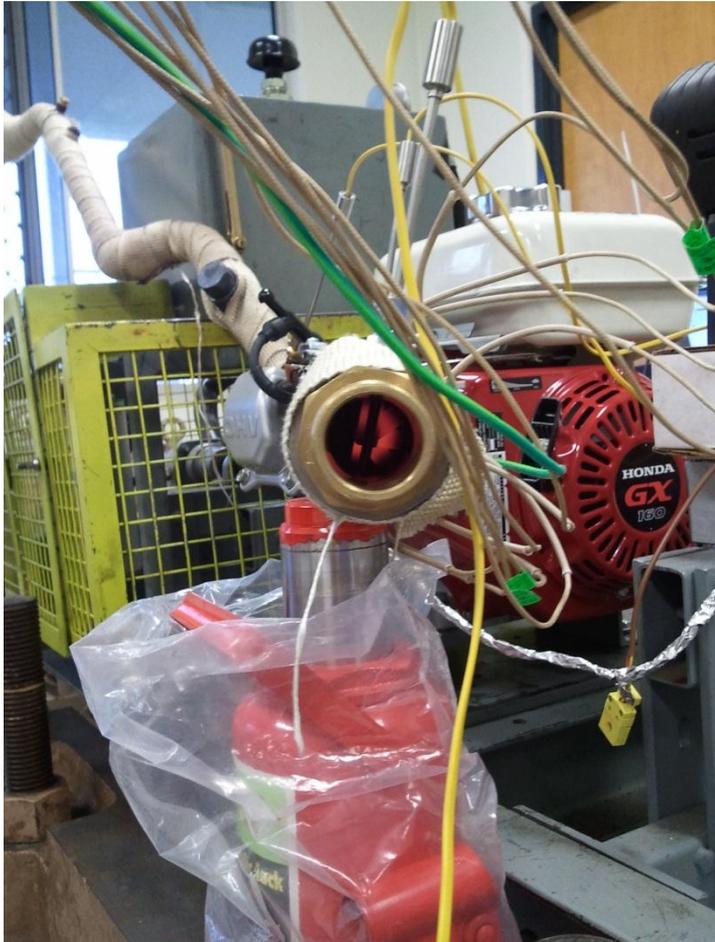
ENGINEERING  
SURVEYING

## ■ Preliminary test



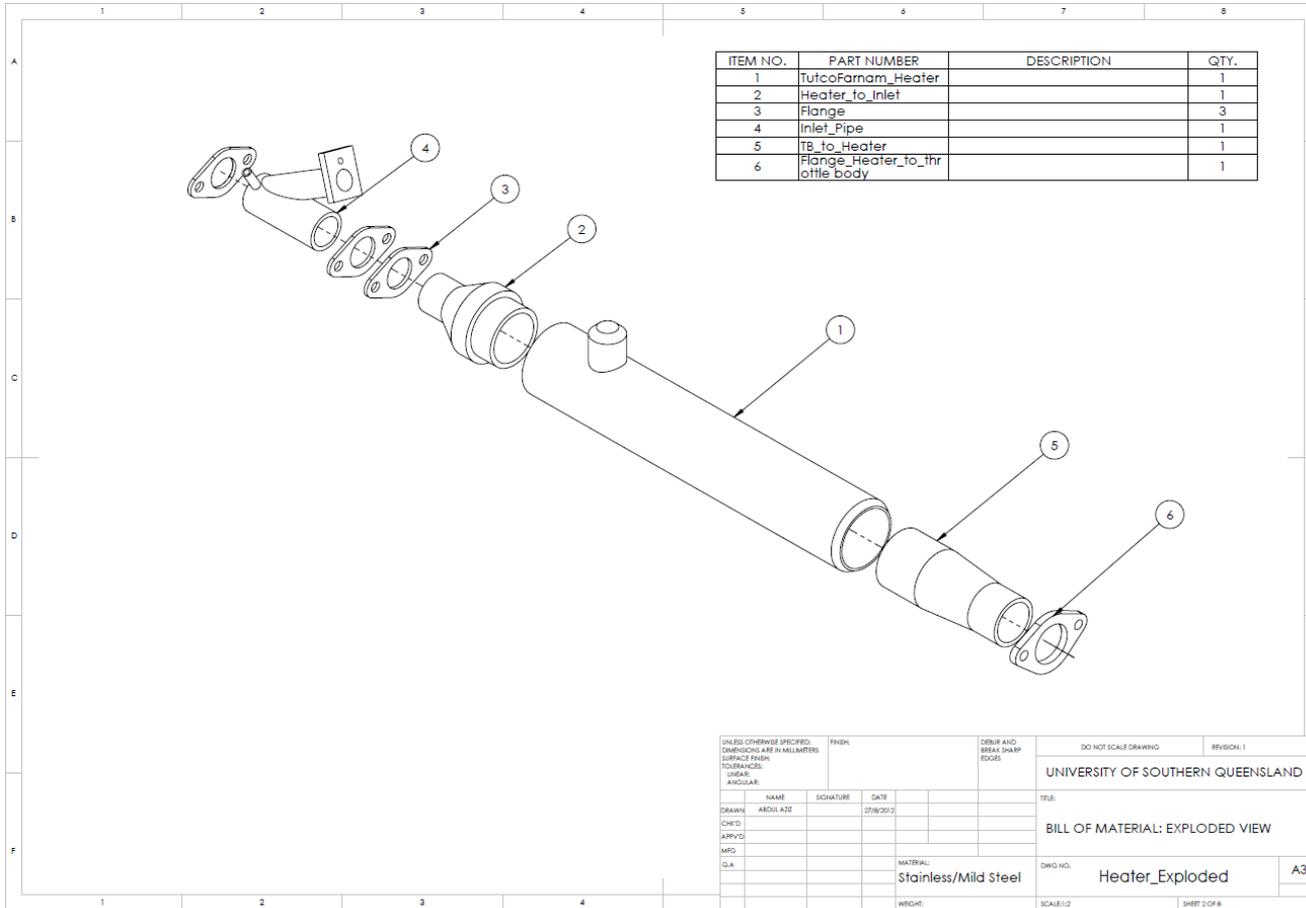
# Experimental Approach

## ■ Preliminary test: Problem



# Experimental Approach

## Next modification:



# Experimental Approach

## ■ Next modification:

- Carburetor system replaced by injector system
- New 2kW heater installed before the injector
- Wideband lambda sensor will be used



# Conclusion



- HCCI: high combustion efficiency, low emissions levels, can use any fuels
- Numerical:
  - Once the intake temperature is increased above a certain threshold, the in-cylinder peak pressure will decrease with increasing intake temperature.
  - The in-cylinder peak pressure keeps increasing with increasing equivalence ratio: will create knocking.
  - Increasing the hydrogen content will also increase the in-cylinder peak pressure: should be no more than 20%
  - In summary, the combustion phasing is advanced by increasing all the parameters (intake temperature, equivalence ratio and energy ratio).
- Experimental:
  - Engine setup has to be completed as soon as possible: workshop work for a new heater is pending. ETA in 2 - 4 weeks!
- Future work: Investigation of all these factors on HCCI engines' performance.