

Sustainable Construction

Potential Carbon Emission Reductions (PCER) in Australian Construction Systems through the Use of Bioclimatic Design Principles

A thesis submitted by

Sattar Sattary

B.Sc. (Architectural Engineering) M.Sc. (Architectural Engineering)

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ABSTRACT

The building sector is responsible for 40 per cent of global energy use. By 2030, a total of 60 Mt of carbon-reduction opportunities will be available in the Australian building sector. The reduction of carbon emissions from Australian buildings is thus a priority for the Federal Government, and thus the Australian government recently announced plans to cut emissions by 26 to 28 per cent by 2030 (Hasham, Bourke & Cox 2015).

This study focuses on the amount of energy consumed during building construction processes, and the degree to which carbon emissions can be reduced through the incorporation of bioclimatic design principles into these processes. These principles include the use of local facilities to reduce transportation, sustainable and efficient use of materials, replacement of Portland cement with geopolymer cement, and similar environmentally-friendly initiatives.

Criteria for the research model proposed in this study have been developed through the application of bioclimatic design principles to six case studies from Australia and the United Kingdom. This was done in order to measure the potential reductions in construction carbon emissions that might be achieved in the pre-construction and construction stages of the building life cycle.

The outcomes of this research demonstrate that use of bioclimatic criteria can achieve reductions in carbon emissions from 48 to 65 per cent for whole building systems, and from 57 to 93 per cent when applied to building elements of general Australian construction systems. However, a more significant finding is that application of the research tool to elements of general Australian construction systems consistently achieved significantly higher reductions in carbon emissions than in current building practice, or through application of a currently-used green rating system (i.e. Green Star tool) to building elements. The future of the green construction industry should thus include consideration of bioclimatic design principles.

CERTIFICATION OF THESIS

This thesis is entirely the work of Sattar Sattary except where otherwise acknowledged. The work is original and has not previously been submitted for any other award, except where acknowledged.

Student and supervisors signatures of endorsement are held at USQ.

Sattar Sattary

Principal Supervisor
Associate Professor David Thorpe

Associate Supervisor Doctor Ian Craig

PREFACE

I have worked in the building industry for more than two decades. When working in this field in Iran, I observed that materials that would construct one square metre of a building in Germany would produce two and a half square metres in Iran. However, whereas the average lifespan of a building in Tehran is 27.5 years, in the UK it is 102 years. Following these observations about the quantity of materials used, as well as the resulting quality of the buildings, I began studying in Australia and became involved in developing the Green Globe standards in Queensland. However, these standards can only be applied to a specific class of building.

In 2002, the Green Building Council of Australia launched the Green Star rating system. I began work with them in 2006, and was assigned to apply this rating system to the Administration Office at the Kelvin Grove QUT campus. This was a pilot study, field testing the Education Tool of the Green Star system. However, ultimately this Education Tool could not be fully applied as the heating and cooling systems in this building were conjoined and not individual. I also found that the Green Star system could be applied to only 5 to 10 per cent of a given building under limited conditions, and that all the sustainability features achieved in this particular building could not be evaluated. Nevertheless, this pilot project was considered one of the most successful environmental assessments for buildings at that time.

A second study in which I participated concerned the green infrastructure assessment tool of the Australian Green Infrastructure Council (AGIC), now the Infrastructure Sustainability Council of Australia (ISCA). I was involved in the initial trials of this tool, and in the evaluation and assessment of specific areas of sustainability. It was of interest to me that this tool could measure and provide for only a small sustainability credit in a given project, but nevertheless be of considerable importance to the construction industry. In fact, this was also the case for several other green infrastructure tools.

The limitations of these green tools led me to reflect on what other considerations might be applied to the assessment of sustainability in the construction industry. An additional impetus to my interest and study in this area were the global summits and various emission reduction targets proposed by some developed countries. For example, the UK intends to reduce carbon emissions by 47 per cent, and Australia has set targets of 26 to 28 per cent over the next twenty years (Hasham, Bourke & Cox 2015). Such emission reduction targets are driven by findings such as that there are some 1.7 trillion tonnes of steel in the existing building infrastructure of the UK that in many cases is recyclable. Also, in the construction industry up to 90 per cent of construction carbon emissions can potentially be reduced (UK Indemand 2014). Other research done in the European Union also notes that humans consume 20 per cent more than nature can produce (Edwards 1999).

The above considerations have driven me towards the development of generic sustainability assessment criteria, that can be applied to single cases or all areas of the construction industry and its activities. Such criteria can potentially assist Australia and other countries to meet the emission reduction targets set in the Paris Summit of 2015. The focus of this study is thus to develop criteria that can be applied towards reducing construction carbon emissions from any single building element system (floor, wall and/or roof) in an Australian construction system without having to consider building classes and typology.

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ABBREVIATIONS

ADAA	Ash Development Association of Australia
AECOM	Architecture, Engineering, Consulting, Operations, and Maintenance
AIBS	Australian Institute of Building Surveyors
AGIC	Australian Green Infrastructure Council
ASA	Australian Standard Associations
ASI	Australian Steel Institute
ASTM	American Society for Testing and Materials
BCSA	British Constructional Steel Association
BES	Building Environmental System
BRE	Building Research Establishment
BREEAM	Building Research Establishment Environmental Assessment Methodology
BFS	Blast Furnace Slag
CCAA	Cement, Concrete, Aggregates & Australia
CEEQUAL	Civil Engineering Environmental Quality
CSIRO	Commonwealth Scientific & Industrial Research Organization
EDG	Environmental Design Guide
EE	Embodied Energy
EEA	European Union Agency
EEC	European Economic Community
EC	Embodied Carbon
EDP	Energy Designs Partnership
EU	European Union
FSC	Forest Stewardship Council
GBCA	Green Building Council of Australia
GC	Geopolymer Cement
GHG	Green House Gas
GER	Gross energy requirement
GS	Green Star
ICE	Institution of Civil Engineers
IECC	International Energy Conservation Code
IMPACT	Integrated Material Profile and Costing Tool
IPCC	Intergovernmental Panel on Climate Change
ISCA	Infrastructure Sustainability Council of Australia
LEED	Leadership in Energy and Environmental Design
LEED-NC	LEED New Construction
LCA	Leftover Concrete Aggregate

LCLCRC	Low Carbon Living Capital Research Centre
LTU	Louisiana Technology University
MARSS	Materials from Alternative Recycled and Secondary Sources
NMSB	Nationale Milieu database Stichting Bouwkaliteit
NRMCA	National Ready Mixed Concrete Association
OECD	Organization for Economic Co-operation and Development
PC	Portland Cement
PCER	Potential Carbon Emission Reductions
PER	Process Energy Requirement
PFA	Pulverised Fuel Ash
PER	Process Energy Requirement
RCA	Recycled Concrete Aggregate
RA	Recycled Aggregate
RMIT	Royal Melbourne Institute of Technology
SCM	Supplementary Cementitious Materials
SEDA	Sustainable Energy Development Agency
SUT	Swinburne University of Technology
UNCED	United Nations Conference on Environment and Development
UNEPA	United Nations Environmental Protection Agency
UNFCCC	United Nations Framework Convention on Climate Change
UNEP	United Nations Environment Programme
UNEP-SBCI	UNEP Sustainable Buildings and Climate Initiative
UNSW	University of New South Wales
USGBC	US Green Building Council
USQ	University of Southern Queensland
VOA	Voice of America
WCED	World Commission on Environment and Development
WFEO	World Federation of Engineering Organizations

CHAPTER ONE

THE NECESSITY TO REDUCE THE CARBON EMISSIONS OF BUILDING CONSTRUCTION

1.1 Overview

The UN recognises climate change and global warming as major concerns of sustainable development. According to a past US President, Barack Obama, climate change has emerged as the greatest threat of the 21st century (Pande 2015). For example, several cities in the US, Mozambique, Bangladesh and other countries will disappear over the next hundred years; and New York, London, Rio de Janeiro and Shanghai will be among the cities that could flood in coming decades (Friedman 2009).

What mankind takes from nature cannot always be compensated, and can often only be produced by nature itself. Humans thus need to use less of the earth's natural resources to allow future generations to fulfil their own needs. The aim of the research presented in this thesis is to outline one area where it is possible to reduce the use of natural resources, that is within building construction. As will be seen in subsequent chapters, there is great potential for reduction of carbon emissions during building construction, but only where appropriate methods are used during the construction process. The focus of this study is the degree to which carbon emissions released from energy use in building construction can be reduced through use of bioclimatic principles.

The chapter is presented in seven sections. Section 1.1 introduces this study. Section 1.2 provides the background to this research. Section 1.3 considers the research problem. Section 1.4 discusses the scope and limitations of this research. Section 1.5 considers the aim of this research. Section 1.6 considers a number of questions that will be answered during conduct of the research. Section 1.7 provides an outline of the chapters in this thesis

1.2 Background to this Research

The United Nations Environment Program reports in its Sustainable Buildings and Climate Initiative (UNEP SBCI 2009) that the building sector is responsible for 40 per cent of global energy use. This sector also generates more than one third of global greenhouse gas (GHG) emissions, and is the largest emission source in most countries around the world. In Australia, the building sector is reported to be one of the largest contributors to Australian greenhouse gas emissions, and thus has the greatest potential for a significant reduction in GHG emissions as compared to other major emitting sectors (McKinsey 2008).

The UN maintains that it is necessary for countries to reduce their greenhouse gas emissions by half in the next forty years. Developed and developing countries have thus agreed to cut their emissions from between 26 to 47 per cent by 2030. To achieve this goal, there will be increasing restrictions on gasoline-powered vehicles on the streets of European countries over the next few years, and the United Nations proposes spending \$100 billion per year to achieve the Paris targets. In reference to this, the UN believes that reduced emissions from the building sector will have multiple benefits for both the global economy and society (Chini 2005; UNEP SBCI 2009; United Nations Framework Convention on Climate Change UNFCCC 2015).

According to the United Nations Environment Program (UNEP), the energy consumption of buildings could be reduced by between 30 to 50 per cent by 2020 (UNEP SBCI 2009). However, Treloar (1998) maintains that construction carbon emissions in the building industry can potentially be reduced by up to six times their current levels. Related to this, the UK government has funded research planning to achieve an 80 per cent reduction in construction carbon emissions in the near future (UK Indemand 2014). It remains to be seen whether these reductions can be achieved.

1.3 The Research Problem

This study proposes that the carbon emissions of building construction can be dramatically reduced through the use of bioclimatic design principles (BDP). These are known techniques that reduce the embodied energy and generated carbon emissions of building construction, but the question remains as to how great a reduction can actually be achieved.

This research focuses on three main areas that can measure potential carbon reduction during building construction – first, carbon emission from energy

consumed during the extraction and production of building materials; second, carbon emission from the energy consumed during the construction processes in building implementation; and finally, carbon emission from the energy consumed in transportation.

1.4 Scope and Limitations of this Research

The building lifecycle is considered as composed of five stages – Stage One, Extraction, covers the extraction of raw materials for the project including fuel used; Stage Two, Production, includes the production, pre-assembling and assembling of materials for the building project concerned; Stage Three, Construction, refers to activities during construction of the building; Stage Four, Operation, includes the use and maintenance activities required during operation of the building; and Stage Five, Demolition, encompasses the demolition and disposal of the building. These five stages are known as a 'cradle-to-grave' building lifecycle.

Within the building lifecycle, all energy used and carbon generated in extraction from mining (Stage One) until the construction products leave the manufacturing gate (Stage Two) are within the boundary condition known as 'cradle-to-gate' in the construction industry. A further boundary condition is termed 'cradle-to-site' which takes into consideration Stages One to Three of the building lifecycle, and includes all energy consumed and generated carbon emissions until the product has reached the point of use on the construction site (Greenspec 2015). This cradle-to-site boundary condition is the focus of this present research study.

This study thus takes as its focus construction carbon emission reductions during the first three stages of the building lifecycle, namely during extraction, production and construction. This presents one limitation of this present study in that the embodied energy and relevant carbon emission calculations will only be considered for these three stages, and not for stages four (operation) and five (demolition) of the building lifecycle. A second limitation is that the main building elements that will be examined in this study include only the floors, walls and roofs. The finishing, stairs, windows and doors will not be considered in the calculations.

1.5 Research Aims

Research is lacking on decreasing the embodied energy and carbon emissions of construction by consideration of criteria based on bioclimatic design principles. This present study proposes that consideration of bioclimatic principles during construction processes can reduce the energy consumption and carbon emissions in the pre-construction and construction stages of the building lifecycle (stages one to three).

This research aims to develop a research model with criteria identified from bioclimatic design principles; and apply that model to the floor, wall and roof construction systems of six selected case studies, and to general Australian construction systems. This will be to identify the potential reductions in carbon emission achievable in these scenarios.

1.6 Research Questions

Many organisations and legal entities that exist to control construction activities have produced a range of recommendations intended to reduce energy consumption and relevant carbon emissions during the building process. However, there are a number of problematic issues that remain unaddressed. For example, no established benchmarks exist to measure construction carbon emissions reduction. Each construction project is unique, and this limits the ability of governmental agencies to develop effective environmental regulations and incentives to control carbon emissions.

During the construction process, the amount of energy consumed and level of resulting carbon emissions are highly variable. Several concerns and questions can be raised about the construction process. These include:

1/ Is existing construction practice sustainable?

2/ What countries are the leaders in construction carbon emissions reduction?

3/ How can the construction industry assist governments to achieve the emission targets accepted in the Paris agreement?

4/ Can the building sector play a major role in an emissions reduction scheme, and would this be cost effective?

5/ What are the levels of embodied energy and associated carbon emissions of different elements of the construction process?

6/ To what extent are techniques to reduce carbon emissions of construction processes known and applied?

7/ What alternatives are available when the existing techniques for reduction of construction emissions are applied, but the results are not substantial?

8/ What percentage of current construction carbon emissions in the Australian construction sector be reduced?

These questions are answered in the research conducted for this thesis.

1.7 Outline of the Chapters in this Thesis

This research is presented in eight chapters. Chapter One presents an introduction to this thesis and sets the context for the remaining chapters. There is consideration of the research problem, background, and scope and limitations of this project.

Chapter Two reviews literature in relation to construction and sustainability, with a focus on the embodied energy of buildings and tools available for its measurement. Bioclimatic design principles are also introduced as a method to reduce the embodied energy and carbon emissions of construction.

Chapter Three reviews literature in relation to sustainable development and the environmental impact of construction. There is also consideration of the decisions and agreements made at several environmental conferences by a range of countries and agencies.

Chapter Four discusses the embodied energies of building materials in greater detail, the method for their conversion to equivalent carbon emissions, and a range of techniques for reducing the carbon emissions of construction.

Chapter Five provides greater detail on bioclimatic design principles, and their consideration in currently available green rating systems (LEED, BREEAM, Green

Star).¹ The research model based on bioclimatic design criteria is also described in this chapter.

Chapter Six outlines the research design and methodology used in this study, and identifies the sources of the embodied energy and carbon emissions data used in this research.

Chapter Seven presents the detailed results and analysis from applying the developed research model to construction elements of the floor, wall and roof in the six case studies selected for this research, and also within similar elements of general Australian construction systems.

Chapter Eight provides an overview to the conclusions made from this study, and makes associated recommendations that need consideration by the Australian construction sector. Recommendations are also made as to further research that should be undertaken to complement the findings from this project.

¹ LEED (Leadership in Energy and Environmental Design) and BREEAM (Building Research Establishment Environmental Assessment Methodology) are green building assessment tools.

CHAPTER TWO CONSTRUCTION, CLIMATE CHANGE AND SUSTAINABILITY 2.1 Overview

The energy consumption of the building sector across the world is substantial, around 40 per cent of global energy use (UNEP SBCI 2009), and this has significant related effects on the environment and climate change. It is thus imperative that the energy use and carbon emissions of the global building sector are reduced. Approaches towards achieving this are the focus of this chapter.

Section 2.1 provides the background to this chapter. Section 2.2 review relationships between the embodied energy of buildings and sustainable development. Section 2.3 considers how carbon emissions during construction may be reduced. Section 2.4 discusses tools that are available for measurement of embodied energy and carbon emissions of buildings. Section 2.5 considers Bioclimatic Design Principles and current research relating to their use. Section 2.6 summarises the content of this chapter.

2.2 Embodied Energy of buildings and Sustainable Development

In striving towards ecologically sustainable development, Lawson (1996) presents a study taking as its focus the embodied energies of common building materials and their assembly in various construction systems in the Australian context. The detail in this study presents useful and practical information, which assists in the development of a methodology for ecological sustainability in respect to building design and construction. This is achieved through the description of the manufacturing process and its environmental impact, as well as through the provision of the embodied energy ratings of Australian building materials and their assembly in a manner useful for building designers.

Lawson (1996) also provides detail on a method for assessment of the embodied energy of construction materials as combined in contemporary Australian building and construction systems. This method is useful when considering holistic evaluation of a given building, taking into account not only its embodied energies, but also the building's various environmental impacts. Lawson's (1996) method uses seven criteria – one relates to the siting of the building, five criteria are concerned with the choice and use of building materials, and the final criterion pertains to an estimate of the building's operational energy performance.

The original calculations in Lawson (1996) were based on a Process Energy Requirement (PER) analysis. This estimates the embodied energy directly related to the manufacture of the construction materials concerned (Milne & Reardon 2014). However, in later work on Australian construction systems, Lawson (2006) switched to the use of other calculation methods, including input-output (I-O) analysis, and hybrid methods combining PER and I-O, for embodied energy analysis. These latter methods calculate the total direct and indirect energy requirements for each output made by a construction system, and figures obtained for embodied energies are significantly higher than for PER calculations (Lawson 2006).

Mawhinney (2002) presents a consideration of sustainable development from the viewpoint of economists and environmentalists, and makes clear the impact that it may have on their workplace practice. It is noted that 'sustainable development' is an overused and sometimes misunderstood phrase. Four key questions are thus raised: these relate to whether sustainable development defines a starting point, a process, or the end-goal; whether sustainable development can provide a coherent theory of practice; whether it is a workable concept in practice; and, finally, whether sustainable development can provide a balanced solution, or whether balance forms part of the solution to sustainable development. Mawhinney (2002) strongly makes the point that ecologically sustainable construction practice must not be limited to the location of the project concerned, but consideration must also be given to environmental impacts over the entire life cycle of a project.

Craig and Ding (2001) present discussion of sustainable practice in the built environment. Various building scenarios are presented together with their proposed solutions whereby development can be undertaken in an environmentally efficient and sustainable manner. There is also consideration of the impact of environmental economics on the construction industry. These authors also stress that an assessment of environmental impact must consider not just the site location of construction, but the environmental impact of all aspects of the project concerned. Sabnis (2012) considers the use of concrete in sustainable design and construction, relating it to best practice in today's built environment. Given the current pressure on the construction industry to reduce waste, it is noted that there is increasing refurbishing, recycling and reuse of concrete in building construction as the least-waste option. Concrete as a construction material is also justified as having significant economic green benefits (Sabnis 2012).

It is becoming increasingly apparent that to be ecologically friendly, building design must consider the entire life cycle of a building project and the associated embodied energies. This is evidenced in a study by Crowther (2015) which found that by designing buildings for disassembly, the potential for embodied energy recovery could be as high as 25 to 50 per cent of the total life cycle energy. In relation to this, Haynes (2010) believes that if buildings were designed with their future deconstruction in mind, we could re-value the materials and components in them, and also recapture the energy embodied within them. This embodied energy of the built environment has been estimated at between 10 and 20 per cent of Australia's total energy consumption (Haynes 2010).

Volz and Stovner (2010) report on embodied energy in masonry construction. Traditionally, masonry takes a considerable amount of energy to produce, and fired materials are generally used which are energy intensive in their production (e.g. clay brick, Portland cement). In contrast to this, non-fired materials and related methods offer substantial energy savings. For example, fly ash has an embodied energy which is effectively zero (provided that the fly ash is considered as a readily-available waste product), and it can be combined with mineral oxide pigments and fine aggregate to produce fly ash bricks in a non-fired process. Fly ash brick production uses 85 per cent less energy than fired clay brick production. Fly ash can also be used as a partial replacement for Portland cement in concrete masonry units. Additional reductions in energy can also be achieved by using recycled products. For example, recycled steel can be used in the steel reinforcing of concrete, which can reduce embodied energy by up to 75 per cent as compared to new steel production (Volz & Stovner 2010).

Following the passage of legislation, the British construction industry are now legally obliged to reduce their carbon emissions by 80 per cent by 2050. In relation

to this, UK Indemand is an academic research centre based in the United Kingdom comprising more than 30 full-time researchers working across four universities (the University of Cambridge, the University of Leeds, Nottingham Trent University, and the University of Bath). UK Indemand is concerned with reducing the use of materials which have energy intensive production methods, this being towards trying to meet the 80 per cent reduction target (UK Indemand 2014).

UK Indemand identifies three main ways in which construction carbon emissions can be reduced. First, there is redesign which reconsiders the construction process to ensure than there is minimum material wastage. Second, there is reuse which involves construction of a new building from the components of an old building as far as is practical: this presupposes the deconstruction rather than the demolition of old buildings. Finally, there must be an intention to reduce materials usage by ensuring that, during the manufacturing and construction process, materials have been designed to last and are used for longer periods in order to slow down their rate of replacement (UK Indemand 2014).

A study by Myer, Fuller and Crawford (2012) from Deakin University found that the use of renewable materials in residential buildings can reduce their embodied energy by up to 28 per cent. However, even where renewable material alternatives could be located, there was often insufficient information available to accurately calculate their embodied energy. These authors concluded that while there is potential to reduce the embodied energy in construction by use of renewable materials, more widespread use of renewable energy in the stages of manufacturing and transportation would be required to maximise this potential reduction in embodied energy.

Thormark (2006) investigated how material choice may affect both embodied energy and recycling potential in an energy-efficient apartment-type housing project in Sweden. The calculated energy for operation was 45 kWh/m₂ of floor-area per year. The embodied energy component was 40 per cent of the total energy needed for a lifetime expectancy of 50 years. This author noted that in the design phase of buildings, it is of great importance to reduce both the overall operational energy needs and the choice of building materials in respect to their later recycling potential. While a material may be recyclable, the forms of that recycling and how disassembly is to be achieved must also be considered. Thormark (2006) concluded that if attention is paid to such factors in the design of buildings, then the embodied energy of conventional buildings can be decreased by up to 15 per cent using relatively simple means.

Ramesh, Prakash and Shukla (2010) investigated the life cycle energy use of a range of residential and office buildings from 73 case studies in 13 countries. The life cycle energy requirement of conventional residential buildings was in the range of 150–400kWh/m² per year compared to that of office buildings, which was 250–550kWh/m² per year. They identified that the operation (80–90 per cent) and embodied (10–20 per cent) phases of energy use were significant contributors to the life cycle energy demand of a given building.

Research from the Queensland University of Technology (QUT) by Crowther (1999) was concerned with design for disassembly to recover embodied energy. It was found that designing for disassembly may require an initial extra input of direct energy during the construction phase of a building. Disassembly requires more energy than demolition, but the potential recovery of embodied energy in the materials and components salvaged for reuse can be as high as one third of the total energy use of a building, a percentage much higher than that required for disassembly. There are also other relative benefits from reuse and recycling of materials represented by the saving of natural resources and a reduction in waste generation and pollution (Crowther 1999).

2.3 Reduction of the Construction Carbon Emissions of Buildings

The carbon emissions generated during the construction of buildings has become a topic of importance given the increasing attention being paid to the reduction of the construction carbon emissions in Australia and the rest of the developed world. A range of research that pertains to this area is presented in this section.

2.3.1 A common carbon metric

The United Nations Environment Programme's Sustainable Buildings and Climate Initiative (UNEP-SBCI) represents a partnership between the UN and public and private stakeholders in the building sector, formed to promote sustainable building practices globally. A study by the UNEP in 2009 proposed the use of a Common Carbon Metric that quantifies the weight of carbon dioxide equivalent (kgCO₂e) emitted per square metre per annum (kgCO₂e/m²/year) by building type and by climate region. The aim of this metric is to accurately measure and quantify greenhouse gas emissions during building operations. The Common Carbon Metric would allow for the collection of consistent data in respect to reporting on the climate performance of existing buildings. Additionally, such a consistent measure would support the formation of policies aimed at the reduction of GHG emissions from buildings. However, the Common Carbon Metric covers only stage four of the building lifecycle, that is carbon emitted during the operation (use and maintenance) of a building (Bisset 2007; UNEP SBCI 2009).

2.3.2 The use of wood in building construction

Research performed by the Centre for Sustainable Architecture with Wood (CSAW) has found that the use of timber in new building construction has a lower carbon and environmental impact than comparable building materials. Timber production was found to be a low energy and low impact process, and the use of timber in construction represents an efficient and economical alternative (CSAW 2010). In support of this, Australian research at the RMIT University investigated the environmental impact of a range of building materials in standard house design using life cycle assessment. This research found that the use of wood products rather than other construction materials could reduce greenhouse gas emissions by up to 51 per cent (Carre 2015).

2.3.3 GreenSpec: A green building resource in the UK

The foremost green building resource in the UK is GreenSpec, launched in 2003 with government funding. GreenSpec provides advice on sustainable building products, materials and construction techniques, this advice being independent of the interests of companies and trading bodies. This organisation suggests several factors that need to be considered when aiming to reduce the embodied carbon in construction activities. First, building design must aim to minimise the use of materials wherever possible, thus reducing embodied carbon. Second, the building elements with the highest carbon impact need to be identified, and where possible these should be

replaced with alternative materials with a lower carbon impact. For example, reduction in the use of cement in construction significantly reduces the carbon impact of the building process. Alternatives to cement include Pulverised Fuel Ash (PFA) and Ground Granulated Blast-Furnace Slag (GGBS) (Greenspec 2015).

In respect to concrete production, an investigation by Turner and Collins (2013) performed in Melbourne quantified the carbon dioxide equivalent emissions (CO₂-e) generated by all activities involved in the production of one cubic metre of concrete. This included all processes from obtaining raw materials through to the manufacturing and construction of the concrete. They compared the CO₂-e footprint generated by 100 per cent Ordinary Portland Cement (OPC) with concrete containing geopolymer binders. The CO₂-e footprint of geopolymer concrete was found to be approximately nine per cent less than comparable concrete containing 100 per cent OPC binder, a figure much less than predicted by earlier studies.

The factors that led to these higher carbon emissions for geopolymer concrete in the study by Turner and Collins (2013) were threefold. First, there was inclusion of the carbon emitted during the mining, treatment and transport of raw materials required for manufacture of the alkali activators required for geopolymers. Second, the actual manufacture of these alkali activators required a significant amount of energy use. Finally, there was a need for an elevated temperature during the curing of geopolymer concrete to achieve reasonable strength, again an energy-requiring process.

2.4 Measuring the embodied energy values of buildings

Note is made here of the Inventory of Carbon and Energy research database maintained at the University of Bath in the UK. This provides an inventory of embodied energy and carbon emissions for building materials in the UK (Inventory of Carbon & Energy 2011).

In respect to measurement of the embodied energy values of buildings, the ISO 14040:2006 and 14044:2006 Life Cycle Assessment (LCA) standards promote sustainable development, particularly in reference to embodied CO_2 -eq analysis. However, it is accepted that embodied CO_2 -eq values are probabilistic rather than

definite. This is due to weakness in the data gathering on product-related CO_2 use and emissions. To address this weakness, research by Acquaye, Duffy and Basu (2011) presents an analysis of hybrid embodied CO_2 -eq in building using stochastic analytical methods. These authors apply this stochastic analysis to a case study involving seven apartment buildings from the construction sector in Ireland. The details of this stochastic analysis are beyond the scope of this thesis. However, these authors conclude that:

Greater methodological and informational benefits are derived from the stochastic hybrid ECO₂-eq intensity analysis of buildings compared to deterministic analysis ... This can provide useful information if embodied CO₂-eq standards and regulatory measures are to be formulated ... [and] provides more useful information to building designers and policy makers (Acquaye, Duffy & Basu 2011, p. 1302).

The stochastic embodied emissions methodology employed by Acquaye, Duffy and Basu (2011) can be applied to any type of building, not only in construction but also other sectors. This methodology can also be applied internationally.

2.4.1 Tools to measure embodied energy and construction emissions

There are various tools that have been developed to measure construction carbon emissions and embodied energy during the five stages of the building lifecycle (extraction, production, construction, operation and demolition). Some of these tools are applicable to the international context, but others relate only to a specific country and region or context. A discussion of some of these tools is presented in this section.

The Building Research Establishment (BRE) group in the UK developed 'Envest', one of the first online software packages that aimed to assist in analysis of building design towards achieving optimum environmental impact and whole life costs. The Envest design tool first appeared in 2002, and went through two revisions to the Envest 2 version. However, Envest was a commercial tool that required companies to purchase a licence for use. There was consequently little uptake by the market, and Envest was discontinued in favour of a simple and free database tool called

'IMPACT' which stands for the Integrated Material Profile and Costing Tool (Watson, Jones & Mitchell 2004; Envest 2 2016).

In 2009 in the United Kingdom, the Technology Strategy Board (TSB) and the Engineering and Physical Sciences Research Council provided £4.8 million to encourage British companies to develop new green design and decision tools (TSB 2010). However, IMPACT is currently the tool that is most commonly used. IMPACT aims to integrate Life Cycle Assessment (LCA), Life Cycle Costing and Building Information Modelling (BIM). It is a tool that is integrated into existing 3D, CAD and BIM software, in a way that "allows construction professionals to measure the embodied environmental impact and life cycle cost performance of buildings ... The results generated by IMPACT can be used in whole building assessment schemes like BREEAM" (IMPACT 2016).

An Australian software provider called eTool has developed a life cycle assessment application (eToolLCD) that is compliant with IMPACT's LCA method. Consequently, use of eToolLCD can earn building designers two credits in the BREEAM New Construction UK, and up to six credits in BREEAM International. The eToolLCD application can be used for the design of all types of building projects from single houses to multi-residential buildings, to multi-billion-dollar infrastructural developments (eToolLCD 2015).

There are life cycle analysis tools available in other countries. For example, 'Elodie' is a tool developed in France to meet the demands of various French environmental declarations relating to life cycle analysis in construction. Similarly, in Germany the German Sustainable Building Council has developed the 'GaBi Build-it' tool for mandatory use in assessment of building LCA (GaBi Build-it 2010). Additionally, the Dutch government has developed several tools for use in its regulated embodied impact assessment for new housing and office buildings that covers all stages of the building lifecycle (Nationale Milieu Stichting Bouwkaliteit NMSB 2013).

In establishing the ISO-21930 International Standard, the Waste and Resources Action Programme (WRAP) in collaboration with the UK Green Building Council, launched the first embodied carbon database for UK buildings in 2007. This allows users to compare the embodied carbon results for their building with others in respect to the building life cycle and building elements, and companies and those involved in building and construction can benchmark their building designs. Such national benchmarks will assist in the assessment and measurement of the embodied carbon in building LCA, and thus identification of where reductions in carbon can be achieved during the building life cycle (ISO 21930 International Standard 2007; Brown, 2014).

In the United States, the 'Tally' application and database have been developed as a BIM plug-in to assist with building LCA. This application requires that architects and engineers use Revit software to quantify the environmental impact of building materials. Tally provides accurate life cycle analysis data for building design process in the USA, and the tool allows for comparative analyses of design options. While working on a Revit model, the user can define relationships between BIM elements and construction materials from the Tally database. The result is life cycle assessment on demand, and an important layer of decision-making information within the same period that building designs are generated. As a Revit application, Tally is easy to use and requires no special modelling practices (EPD-TALLY 2008).

2.5 Bioclimatic Design Principles

The design process that brings together the disciplines of human physiology, climatology and building physics (Olgyay 1963)

Bioclimatic design principles (BDP) were identified several decades ago in 1963 by the Olgyay brothers (Altomonte 2008). These twin brothers from Hungary defined bioclimatic design principles as those principles that bring together the disciplines of human physiology, climatology and building physics. They have been integrated into building design in the context of regionalism in architecture, and in recent years have been seen as a cornerstone for achieving more sustainable buildings (Hyde 2008).

Bioclimatic design principles have been used, investigated and analysed by different people and organisations in the construction industry. For example, the techniques and bioclimatic design principles of the Olgyay brothers provide the foundation for much of the building simulation software in use today, and they have also been used to analyse environmental factors and graphical representations of climate (Jones 2003; Hyde 2008).

The field of bioclimatic design is adding knowledge to the construction area where the flexible cooperation of several disciplines contributes to the well-being of the human and built environment. The focus of bioclimatic design principles is to develop a design method based on the integration of specialised and interconnected areas of knowledge (Altomonte 2008).

2.5.1 Background to Bioclimatic Design Principles

The Olgyay brothers published three books on bioclimatic architecture: *Application of Climatic Data to House Design* (1954); *Solar Control and Shading Devices* (1957); and in 1963 by Victor Olgyay only, the well-known *Design with Climate: Bioclimatic Approach to Architectural Regionalism* (1963). Although the three books share some text and illustrations, there are significant differences between them in respect to the trajectory of environmental building design. The little-known first book of the Olgyays, *Application of Climatic Data to House Design*, was used to prepare a report for the US Housing and Home Finance Agency. In that book, they suggested a new approach to house design based exclusively on environmental principles. Victor Olgyay (1910–1970) is best known today as the author of his 1963 publication, a book often referenced in the environmental building design field. (Leather & Wesley 2014).

As leaders in research in bioclimatic architecture from the early 1950s to the late 1960s, the Olgyay brothers can be considered as the fathers of contemporary environmental building design (Leather & Wesley 2014). Related to this, Pereira (2002) believes that building design should be inspired by nature, and aim to minimise environmental impact. To do this, issues that must be considered in the design include health and well-being, energy and sustainability.

2.5.2 Current research on Bioclimatic Design Principles

As noted, the research and publications of the Olgyays provided the inspiration for much of the building simulation software of today. For example, other than the difference between working on graph paper and using computer-generated graphics, Autodesk's Ecotect Analysis program (simulation and building energy analysis software) and the Olgyays' techniques for the analysis of environmental factors and graphical representation of climate are quite similar. The manner in which the Olgyays established connections between building design and climate science laid the foundation for the development of environmental simulation, one of contemporary architecture's leading methods of form generation. Victor Olgyay's teaching, however, represents another kind of thinking, a broader concern for architecture beyond energy performance.

Considerable progress in reducing the energy consumption of new buildings has been achieved through use of modern bioclimatic techniques. Attention has now turned to reducing the energy consumption of existing buildings. By use of appropriate technologies and techniques of bioclimatic retrofitting and design, it is possible to significantly reduce the energy consumption of existing buildings by a factor of five to six times as compared to a conventional building (Jones 2003; Hyde 2008).

Bioclimatic design principles have also been used for mitigation and adaptation strategies to achieve sustainable development in climate change and architecture. For example, the following is taken from a study by Altomonte (2008):

Site & Climate Analysis; comprising the analysis of the site, exposure, climate, orientation, topographical factors, local constraints and the availability of natural resources and ecologically sustainable forms of energy considered in relation to the duration and intensity of their use (Altomonte 2008, p. 105).

More recent research at the University of Sydney has used bioclimatic design principles in retrofitting of existing buildings and urban networks. The results show that substantial improvement in energy performance can be realistically achieved through the implementation of bioclimatic design principles in retrofitting of existing buildings (Liu 2010; Architecture 2015). Use of bioclimatic design principles has been integrated into building design in the context of regionalism in architecture, and in recent years has been seen as a cornerstone for achieving more sustainable buildings (Hyde & Yeang 2009). Research has found that appropriate bioclimatic design can significantly reduce energy consumption in a building as compared to conventional building design (Jong & Rigdon 1998). More detail and analysis of bioclimatic design principles is presented in Chapter Four.

2.6 Summary

This chapter identifies that there are numerous studies and research on embodied energy, carbon emissions and bioclimatic design principles in respect to building and construction. However, reducing embodied energy and carbon emissions through use of BDPs has received little attention in the Australian context. The focus of this research is thus on reducing embodied energy and carbon emissions during the building lifecycle through use of bioclimatic design principles in Australian construction systems.

CHAPTER THREE SUSTAINABLE DEVELOPMENT AND INTERNATIONAL AGREEMENTS 3.1 Overview

Climate change, depletion of natural resources and the rising global population have increased international attention to the problems facing the environment, and the increasing necessity to achieve sustainability in development and construction. This is reflected in the range of international conferences which have taken place over recent decades, culminating in the signing of the Paris Agreement in 2015.

Section 3.1 provides a brief overview to this chapter. Section 3.2 considers the notional of sustainability, and its relationship to sustainable development and construction. Section 3.3 discusses the environmental impact of building. Section 3.4 considers a range of key decisions and international reaction to environmental issues as demonstrated within a range of international agreements and protocols from the 1980s to the present. Section 3.5 provides a summary of the main themes within this chapter.

3.2 Sustainability

Sustainability is at the centre of any governmental discussion or decision related to energy crises, climate change or global warming. Such considerations have several times brought world leaders together for discussion and policy formation. Examples include the oil crisis summit in 1973; the UN Geneva Convention on Air Pollution in 1979; the Montreal Protocol on the ozone layer in 1987; and the Kyoto Protocol on the reduction of greenhouse gases in 1997 (Adams 2003). More recently, there has been the Intergovernmental Panel on Climate Change (IPCC) in 2007; and the Paris Agreement on Global Warming in 2015 (UNFCCC 2015).

In the past, the word 'sustainability' had a simple meaning related to the act of continuing (sustaining) a given behaviour or action for an ongoing period. More recently, sustainability has assumed a new meaning related to the quality of not being environmentally harmful. Hendriks (2001) extends this and argues that any definition of sustainability should include not only the notion of environment, but also social and economic interests such as health, wellbeing, safety, care for living space, prosperity and related concepts.

The resources humanity now takes from the earth increasingly cannot be balanced and reversed by nature. The rapidly increasing world population has led to overuse and increasing depletion of global resources from the natural environment. There is also global warming and increasing environmental problems. The health and wellbeing of future generations depends on sustainable environmental policies being established as soon as possible. The aim of such policies must be to create an ecologically healthy environment based on a program of sustainability and sustainable development (Hendriks 2001).

3.2.1 Sustainable Development

The Brundtland Report of 1987 issued by the World Commission on Environment and Development (WCED) identified the urgency of progressing towards a notion of economic development that could be sustained without depletion of natural resources or harm to the environment. The report defined sustainable development as "development that meets the needs of the present without compromising the ability of future generations to meet their own needs" (WCED 1987, para 1).

Three obligations follow on from this definition of sustainable development. First, there must be responsible use of resources now and into the future. This implies a responsibility to leave future generations with both natural resources and enough scientific/cultural capital to allow them to meet their needs. Second, there must be efficient protection of global resources. This implies a responsibility to protect and effectively manage all environmental resources including land, water, air and biodiversity. Thirdly, there must be equal sharing of global resources. This implies a duty to share resources locally and globally based on equal access for all (Edwards 1999; Mawhinney 2002).

Following on from these obligations, in 2000, a wider definition was suggested by the UN's National Strategies for Sustainable Development that encompasses not only sustainable development, but also the notion that there must be associated sustainable social and economic development. This allows for the needs of the present generation without threatening the ability of future generations to meet their needs. In respect to this definition, the UK Department of Environment and Transport believes that alongside sustainable social and economic development, there must also be environmental protection and wise use of natural resources (Mawhinney 2002).

The main notions within these various definitions of sustainable development are summarised in Table 3.1.

Definition	Message
Brundtland Report (WCED 1987)	 Responsible use of resources now and in the future Efficient protection of global resources Equal sharing of global resources
National Strategies for Sustainable Development (2000, cited by Mawhinney 2002)	• Similar to WCED definition, but with the added notion that there must be social and economic development along with sustainable development
UK Department of Environment and Transport (Mawhinney 2002)	• Promotes a definition of sustainable development that maintains social and economic growth alongside environmental protection and careful use of resources

Table 3.1: Main notions within definitions of sustainable development

Sources: WCED 1987; Mawhinney 2002.

3.2.2 Sustainable Construction

The Brundtland Report considers sustainable construction as part of the more general area of sustainable development. Sustainable construction may be defined as a way of designing and constructing buildings that provides a healthy, ecological environment, one that begins to address the effects of problems caused in the past, and that provides for the needs of existing and future generations. (WCED 1987). The Future Foundation in the UK extends this definition of sustainable construction to include refurbishment of existing structures. They note that sustainable construction and development promotes environmental, social and economic gains both for the present and future generations, and that our economy, environment and social well-being are interdependent (Future Foundation 2015).

Hendriks (2001) agrees that to be sustainable, construction must not only consider the impact of building on nature and the environment, but also support the physical, psychological and social aspects of human health. Additionally, this author notes that sustainable construction must also take the durability of construction materials into account, in that any materials used must serve for at least the expected lifetime of the building concerned. Edwards (1999) also argues that sustainable construction must integrate low energy design with materials that have minimal environmental impact at all points in the building lifecycle. Essentially, sustainable construction assumes careful consideration of resource efficiency, energy conservation, and environmental principles during the entire lifecycle of any building project from cradle to grave (Organization for Economic Co-operation and Development OECD 2003; Hui 2015).

The focus of this study concerns the carbon emissions generated by the construction industry in Australia, and their potential reduction through use of bioclimatic design principles. This is of increasing importance, as reducing construction carbon emissions has become a mandate for sustainable construction. The themes running through the various notions and definitions of sustainable construction discussed in this section reflect this: to be sustainable, building projects must consider conservation of resources used for construction, environmental impact, and protection of biodiversity. Sustainable construction must aim to provide an ecologically healthy environment and optimum living conditions to meet the needs of existing and future generations.

3.3 Environmental impact of building

Climate change and global warming have been recognized as major concerns of sustainable development. By 2100, sea levels are predicted to rise by two metres if current levels of carbon emissions are not reduced (DeConto & Pollard 2016). If this occurs, up to fourteen cities in the United States will disappear over the next century; and several countries including Mozambique and Bangladesh will be completely inundated by the rising ocean levels (Friedman 2009). The UN believes that humanity needs to reduce its greenhouse gas emissions by at least 50 per cent within the next forty years in order to avoid these worst-case scenarios of climate change (UNEP 2009; UNEP SBCI 2009).

The building process produces large amounts of greenhouse gas emissions during construction, demolition, reconstruction and/or restoration of buildings. These activities also produce large quantities of construction and demolition waste, and thus have a high environmental impact. They also consume large amounts of global

resources, not only minerals, but also water and energy in its various forms (UNEP SBCI 2009).

A report by Naik (2008) estimates that resources are being extracted from the earth at a rate of 20 per cent greater than the earth can produce or replenish. However, it is believed that if the principles of sustainable development are followed, this unsustainable level of resource consumption will be reduced. Environmental considerations must therefore take an equal part alongside economic considerations if the construction industry is to achieve development that is sustainable (Naik 2008). This is not an impossible expectation because, based on existing technology, the energy consumption in both new and existing buildings can be cut by an estimated 30 to 50 per cent without significant increase in the cost (UNEP SBCI 2009).

A study by the UN's Sustainable Buildings and Climate Initiative (UNEP SBCI 2009) considered the quantity of carbon emissions produced during the building lifecycle. It was found that the building sector generates more than one third of global GHG emissions, and in most countries, is the largest source of carbon emissions. Transportation of people, goods and services to and from the building site was also noted as one of the most significant ways in which energy was consumed. In global terms, the environmental impact of the construction process was considerable, being responsible for 40 per cent of energy use, 30 per cent of raw materials taken from nature, 25 per cent of total waste, 25 per cent of water use, and 12 per cent of land use (UNEP SBCI 2009)

The research in this thesis considers only the first three stages of the building lifecycle (extraction, production and construction). However, these stages produce only 10 to 20 per cent of the total carbon emissions during the entire lifecycle of a building, the remainder being produced in stages four and five (operation and demolition). In fact, most carbon emissions are produced during the operational phase (UNEP SBCI 2009). Future research will consider these last two stages of the building lifecycle as they are beyond the scope of the present research.

In Australia, buildings and their users are responsible for between 18 per cent (ClimateWorks Australia 2010) and 25 per cent (Commonwealth Scientific and Industrial Research Organisation CSIRO 2000) of Australia's greenhouse gas emissions, depending on the source of the estimate. Residential buildings account for around 58 per cent of these emissions, and commercial buildings for around 42 percent. It is estimated that the energy embodied in existing building stock in Australia is equivalent to around ten years of the nation's energy consumption. In this respect, the choice of materials and design principles has a significant, but previously unrecognised, impact on the energy required to construct a building (CSIRO 2000).

A report by the Intergovernmental Panel on Climate Change (IPCC) suggests that the Australian building sector has the greatest potential for a significant reduction of carbon emissions as compared to other major emitting sectors. Costs to reduce GHG emissions were also noted to be relatively lower in the building sector as compared to other emitting sectors (Levine & Urge-Vorsatz 2007). In respect to this, it has been estimated that a total of 60 Mt of carbon-reduction opportunities could be found in the Australian building sector by 2030 (McKinsey 2008). A decrease in carbon emissions from Australian buildings is consequently a priority for both the Green Building Council of Australia (GBCA 2008), and the Federal Government which has announced plans to cut emissions by 26 to 28 per cent by 2030 (Hasham, Bourke & Cox 2015).

In absolute figures, it is estimated that the Australian building sector has potential to contribute to around 11 per cent of the carbon reductions to be achieved by 2020. Around three quarters (77 perc cent) of these opportunities for reduction are within the commercial sector (including 16 Mt CO₂-e for existing building retrofits, and 4 Mt CO₂-e for new builds). Such reductions offer an average net saving to society of \$99 per tonne, and offer investors an average profit of A\$90 per tonne (ClimateWorks Australia 2010).

Drawing these themes about the environmental impact of the construction process together, some general figures can be identified in respect to the global context. The built environment worldwide accounts for some 40 per cent of global GHG emissions, and the construction sector accounts for around 40 per cent of the world's total energy consumption. Construction is also responsible for approximately half of

all resources taken from nature, and production and transport of building materials consumes up to 40 per cent of all energy used (UNEP SCBI 2009). These figures are predictably the greatest in developed countries (UNEP SBCI 2009; Technology Strategy Board 2010; Ecospecifier 2015; GreenSpec 2015).

Based on the reviewed environmental impacts of building, Table 3.2 is a summary of the environmental impacts of buildings on different levels: globally, in the UK, in the EU and in Australia.

Table 3.2: Summary of environmental impacts of global construction

Global figures

- Fourteen U.S. cities, Mozambique and Bangladesh may disappear over the next century (Huffington Post 2013).
- New York, London, Rio de Janeiro and Shanghai will be among the cities that could flood by 2100
- The built environment accounts for some 40 per cent of global GHG emissions
- Buildings are responsible for 40 per cent of global energy consumption
- Construction is responsible for nearly half of all resources taken from nature
- Resources are extracted at a rate of 20 per cent more than the earth produces

(UNEP SBCI 2009)

- Production and transport of building materials consumes 25 to 40 per cent of global energy use
- In the EU, building and transport use more than 65 per cent of total energy consumption (compared to 60 and 50 per cent in the US and Japan respectively

(OECD 2003)

• In the EU buildings are responsible for 50 per cent of energy use; production of 50 per cent of ozone depleting chemicals; and 50 per cent of raw materials used by industry (Edwards 1999).

UK figures

- Building accounts for around 45 per cent of the UK's total carbon emissions
- Up to 50 per cent of ozone depleting chemicals in the UK relate to construction
- Construction materials account for 420 million tonnes of material consumption (seven tonnes per person) (UNEP SBCI, 2009; Green Spec 2015)
- From 10 to 20 per cent of total construction emissions are produced during extraction of materials
- From 80 to 90 per cent of the energy used by construction is consumed during use of a building (Ecospecifier 2015).

Australian figures

- The building sector is one of the largest contributors to Australian greenhouse gas emissions
- Buildings and their users are responsible for almost a quarter of Australia's greenhouse emissions
- Australia spends around \$4 billion per year on energy, generating 46.4 million tonnes of CO₂ in 1999, and these emissions increase by 3 to 4 per cent annually (Energy Information Administration 2013)

Source: Extracted from Chapter Three

3.4 Key decisions and international reaction to environmental issues

In recent decades, the building and construction sector have caused considerable environmental problems, as well as a significant impact on the use of vital key resources such as water, air, climate, food supplies and energy resources. The environmental problems include ozone depletion, global warming, acid rain, air pollution and greenhouse gas emissions, as well as the need for energy in the transportation and demolition of waste materials. These issues have required international attention, as evidenced in the range topics that have been discussed at various summits over the last fifty years: for example, energy supplies in the 1970s; sustainable development in the 1980s; depletion of the ozone layer and global warming in the 1990s; sustainable construction in the 2000s; and greenhouse gas reduction in recent years (Edwards 1999; IPCC 2011).

Since the advent of the world oil crisis in 1973 and the start of the green movement, several important international summits and conferences have been convened in an effort to reduce the impact of human activity on the environment and climate. These include the World Commission on Environment and Development (WCED); the Earth Summit in Rio de Janeiro; the Kyoto Protocol in Japan; the European Environmental Agency (EEA); the Intergovernmental Panel on Climate Change (IPCC); the United Nations Environmental Program Sustainable Buildings and Climate Initiative (UNEP SBCI); and the Paris Agreement in 2015. These conferences and their main themes and outcomes are briefly reviewed in this section.

3.4.1 World Commission on Environment and Development – 1987

The WCED conference in 1987 produced the well-known Brundtland Report, titled as *Our Common Future*. This conference drew attention to the urgency of making progress toward economic development that could be sustained without depleting natural resources or harming the environment. A key statement (and warning) from this conference was that sustainable development is development that must meet the needs of the present generation, but without compromising the needs of future generations (WCED 1987).

Sustainable construction based on the notion of equity and social justice was a cornerstone of the Brundtland Report. The main aim of the WCED enshrined in the Brundtland Report was to promote economic development and growth, but at the same time ensuring that such development considered environmental and social factors within any construction or related program to meet society's needs for employment, food, energy, water and sanitation (Borowy 2013).

The report also recommended a major reorientation and refocusing of programs concerning sustainable development within the various sectors of the UN. It was proposed that in such a new system-wide commitment to sustainable development, the United Nations Environmental Program (UNEP) should be the primary source providing environmental data, assessment, reporting, and related support for environmental management. Additionally, the UNEP should be the main advocate and agent for change and cooperation on critical environment and natural resource protection in any project where sustainable development was to be a priority (WCED 1987).

The Brundtland Report also highlighted several major global challenges facing humanity including preserving the quality of the environment; stabilising global population; the conservation and enhancement of natural global resources; meeting energy needs; meeting water needs and providing sanitation; and finally the survival of species and ecosystems. Reducing the impact of construction projects on the environment and natural resources assists in meeting these challenges (Borowy 2013). This, in fact, provided the impetus for this present research project on reducing the carbon emissions of construction through application of bioclimatic design principles, thus promoting sustainable construction.

3.4.2 The Earth Summit – 1992 and 2012

The United Nations Conference on Environment and Development (UNCED), also known as the Earth Summit, was held in Rio de Janeiro in 1992 (UNCED 1992). A further related summit called the United Nations Conference on Sustainable Development, Rio+20, was held in 2012, also in Rio (UNCSD 2012). During these summits, the environment and ecology was the prime focus, with the aim being promotion of sustainable construction and design practices. The major issues discussed at these summits were reducing resource use in construction; minimising the impact of development on the environment; and protecting global biodiversity (UNCED 1992; UNCSD 2012).

The most important outcome resulting from the Earth Summit of 1992 was a document called 'Agenda 21', a non-binding action plan relating to sustainable development which was agreed to by the representatives of 178 governments

attending this conference. The subsequent UN Conference on Sustainable Development in 2012 saw the aims of Agenda 21 reaffirmed by 192 governments represented at this conference (UNCED 1992; UNCSD 2012).

The action plan in Agenda 21 included a range of environmental goals to be undertaken by signatories at the local, national and global level. A full consideration of Agenda 21 is beyond the scope of this thesis. Suffice to say here that Agenda 21 is a 350-page document with 40 chapters that sets out in detail how sustainable development might be achieved at every level of government. The main aims of Agenda 21 are that sustainable design is in harmony with nature, with responsible use of resources, and that design considers the needs of both the current and future generations in a socially, environmentally and economically friendly manner (UNCED 1992; UNCSD 2012).

3.4.3 The Kyoto Protocol – 1997

The Kyoto Protocol is an international agreement signed in Japan in 1997, but which did not take effect until 2005. The aim of the Protocol was to reduce global greenhouse gas emissions to reduce the impact of climate change. The Protocol also contained agreements to sustainable development within its clauses. These included that any materials produced or used for construction should be energy efficient and sustainable, with minimal impact on the environment; that new and renewable forms of energy should be developed; that there should be improved management of the products of building demolition; and that there should be associated reductions in greenhouse gases in the transport sector. Around 192 countries are currently signatories to the Kyoto Protocol, though at present these do not include the USA and China, two countries with significant greenhouse gas emissions (UNFCCC 1998).

Some of the key decisions of the Kyoto Protocol included the following.

- Enhancement of energy efficiency in relevant sectors of the national economy
- Protection and improvement of sinks and reservoirs of greenhouse gases not controlled by the Kyoto Protocol
- Promotion of sustainable forms of agriculture in light of climate change considerations

- Research into, and the promotion, development and increased use of, new and renewable forms of energy as well as research into carbon dioxide sequestration technologies
- Progressive reduction or phasing out of market imperfections, fiscal incentives, tax and duty exemptions and subsidies in all greenhouse gas emitting sectors that run counter to the objective of the convention
- Encouragement of appropriate reforms in relevant sectors aimed at promoting policies and measuring the limitation or reduction of emissions of greenhouse gases not controlled by the Montreal Protocol
- Measures to limit and reduce emissions of greenhouse gases not controlled by the Montreal Protocol in the transport sector

(UNFCCC 1998).

In conclusion, the Kyoto Protocol demonstrates that there have been a series of decisions relating to sustainable construction that include to use energy more efficiently; to reduce greenhouse gas emissions in all areas of the construction sector, including in transportation and waste management; and to increase use of renewable forms of energy and carbon dioxide sequestration technologies (UNFCCC 1998).

3.4.4 The European Environment Agency (EEA) – 1994

The European Environment Agency (EEA) is an office of the European Union (EU) which became operational in 1994. The Agency provides independent information on the environment to its 33-member countries in the EU. The aim is assist those countries to make informed decisions about environmental issues when considering major construction and other projects, and for sustainable environmental policies to be integrated into economic and social policy (EEA 2016).

Research has found that in the European Union, buildings and construction are responsible for around half of total energy use, with materials transport being largely responsible for the remaining component (Edwards 1999). The European Environment Agency (EEA) thus has sustainable construction as one of its major mandates, with related policies being established towards construction that has minimum environmental impact and maintains ecological diversity (EEA 2016).

EU environmental policy includes that pollution should be prevented at its source, and polluters should pay for environmental damage they cause; that environmental policy should be integrated with economic and social policy; that environmental effects of development should be taken into account in the technical planning and decision making stage; that environmental protection is a responsibility of the entire community; and that EU environmental policy should be harmonised with national policy (EEA 2016).

The European Environment Agency describes sustainable construction as a process that effectively integrates low energy design with materials which have minimum environmental impact and maintain ecological diversity. Based on this policy, the main objects of sustainable construction are to minimise non-renewable resource consumption; to reuse and recycle construction materials or waste; to enhance the natural environment through product selection; to minimise waste and prevent pollution at building sites; and to use outputs from one process as inputs to others (e.g. energy from materials) (EAA 2016).

3.4.5 The Intergovernmental Panel on Climate Change (IPCC) – 1988

The Intergovernmental Panel on Climate Change (IPCC) is a scientific body set up by the United Nations in 1988. It aims to provide an objective scientific perspective on the effects of climate change and its global economic impacts. A report by the IPCC in 2007 identified that global construction is responsible for 40 per cent of the world's energy consumption, and produces one third of global greenhouse gas emissions. The report also noted that most energy consumed in the construction sector was during use of a building (i.e. Stage Four, operation, of the building life cycle) at 80 to 90 per cent (Levine & Urge-Vorsatz 2007).

The report proposes that energy consumption in both new and existing buildings could be cut by 30 to 50 per cent, and that this could be done in a cost-effective manner using existing technologies, with potential to reduce construction carbon emissions by around 5.6 Gt CO_2 by 2030. However, achieving such reductions is going to require significant effort by the governments of the various countries of the United Nations (Levine & Urge-Vorsatz 2007).

The report concluded that the global construction sector has great potential to provide long-term, cost-effective reduction in greenhouse gas emissions. A significant portion of these savings could also be obtained in ways that reduce life-cycle costs, thus providing reductions in carbon emissions that have a net benefit rather than cost (Levine & Urge-Vorsatz 2007).

3.4.6 United Nations Environment Program, Sustainable Buildings and Climate Initiative – 2009

A report by the Sustainable Buildings and Climate Initiative within the United Nations Environment Program (UNEP SBCI 2009) reiterated several of the themes noted in the earlier publications of the various bodies involved in dealing with climate change. In particular, yet again there was identification of the fact that the global construction sector is one of the largest producers of greenhouse gas emissions, but that it also has the greatest potential for significant and cost-effective reductions in emissions through use of existing technologies. Such reductions have the potential to deliver both social and economic benefits to global society. However, emission reduction targets cannot be achieved without gains in energy efficiency in the building sector (UNEP SBCI 2009).

3.4.7 The Paris Agreement – 2015

In 2015, the UN Framework Convention on Climate Change (UNFCCC) brokered an agreement in Paris between 196 countries related to climate change. The agreement included action to promote low greenhouse gas and climate-resilient development, but in a fashion that will not impact on global food production. The Paris Agreement of 2015 is a legally-binding framework for a global effort to reduce the impacts of climate change. Of significant importance is that China is and the USA² were parties to the Paris Agreement (UNFCCC 2015).

The Paris Agreement allows the signatory countries to determine their own national contributions to meeting the aims of the document, but such contributions are expected to be ambitious and progressive over time. A specific aim is to achieve netzero emissions in the second half of this century. This assumes profound changes to the economies of some countries, particularly those in the developed world. A non-

² On 2 June 2017, the USA withdrew from the Paris agreement on climate change (ABC News 2017).

legally binding part of the Agreement is for private and public entities to provide an annual US\$100 billion to aid developing countries to meet their nationally determined targets (Hasham, Bourke & Cox 2015; UNFCCC 2015).

Other highlights of the Paris agreement of interest to this study include that Nationally Determined Contribution (NDC) countries can meet their targets by transferring 'mitigation outcomes' internationally, that is by sharing mitigation targets. Related to this, public and private organisations can support sustainable development projects that generate transferable emissions reductions (Hasham, Bourke & Cox 2015; UNFCCC 2015).

The Paris Agreement thus provides a common framework for individual countries to consider their own capacities for reducing climate change. The Agreement has the potential to provide a basis for long-term international action on climate change, particularly as the technologies and alternative energy systems to do this become further developed and economically more viable (UNFCCC 2015).

Emissions in 2005 were determined as the base point from which reductions would be measured. The Australian Federal Government has pledged to reduce emissions by 26 to 28 per cent by 2030, a figure which provides justification for this present research whose outcomes have potential to assist in this process. The USA has pledged to reduce emissions by 41 per cent (but has since withdrawn from the agreement), and Canada by 30 percent. The European Union has pledged a reduction of 40 percent, but relative to their emission levels in 1990 (Hasham, Bourke & Cox 2015). Details of these targets are presented in Table 3.3.

Country	Change on base year	Rate of reductions to achieve target	
	2005	2010-2020	Post 2020
Australia	-26%-28%	-0.8%	-1.6%/-1.9%
USA	-41%	-1.4%	-2.3%
EU	-34%	-0.4%	-2.6%
United Kingdom	-48%	-1.6%	-5.1%
Germany	-46%	-2.4%	-2.6%

Table 3.3: Post-2020 emission reduction targets for major developed countries

Source: The Climate Institute (cited in Hasham, Bourke & Cox 2015)³

³ On 2 June 2017, the USA withdrew from the Paris agreement on climate change (ABC News 2017).

3.5 Summary

In the face of global environmental problems. existing construction practices are not sustainable, and it is necessary to rethink current methods and establish new building construction processes. The efficient use of natural resources (energy and construction materials), the prevention and reduction of the environmental impact of construction activities, and the protection of biodiversity must be major considerations in any move towards achieving sustainable construction practices.

This chapter has considered an extended notion of sustainability suitable for use when a focus is taken on achieving sustainability in construction practices. The major findings from a range of international conferences and agreements have also been discussed, with common themes being identified as to how reduction in greenhouse gases and carbon emissions might be achieved. The main theme that informs this present research is that the construction sector is a major site of global energy use, but one where significant reductions in carbon emissions can be achieved in a costeffective manner using existing technologies. This is the case for the Australian construction sector, which has the greatest potential for significant reduction of greenhouse gas emissions as compared to other major emitting sectors in this country. The next chapter considers specific ways in which reduction in the carbon emissions of construction in Australia and elsewhere may be achieved.

CHAPTER FOUR EMBODIED ENERGY AND REDUCING CARBON EMISSIONS OF CONSTRUCTION

4.1 Overview

One third of the world's energy is used by industry to make products – the buildings, infrastructure, vehicles, capital equipment and household goods that sustain our lifestyles. Most of this energy is needed in the early stages of production to convert raw materials, such as iron ore or trees, into stock materials like steel plates or reels of paper (UK Indemand 2015). The key materials with which we create modern lifestyles – steel, cement, plastic, paper and aluminium in particular – are thus the main carriers of this 'embodied energy', and if we want to make a significant reduction in this industrial energy use, we need to reduce our demand for these materials.

The purpose of this chapter is to present the concept of embodied energy in building materials, how this can be measured, and how embodied energy and carbon emissions might be reduced. Section 4.1 provides an overview to this chapter. Section 4.2 considers the embodied energy of building materials and their measurement. Section 4.3 identifies the carbon emissions within construction processes. Section 4.4 considers how embodied energy can be converted to its equivalent in carbon emission. Section 4.5 discusses various techniques that can reduce the carbon emissions from construction. Section 4.6 identifies barriers that exist to emissions reduction in construction. Finally, Section 4.7 presents a summary of this chapter's content and links to the next chapter.

4.2 The Embodied energy of building materials

Embodied energy represents the energy consumed by all processes associated with the production of a building, from the mining and processing of natural resources, to manufacturing transport and product delivery (Milne & Reardon 2014). Embodied energy can be broken down into direct and indirect energies. Direct embodied energy relates to the energy involved in transportation of construction materials, and then assembling those materials on site. Indirect embodied energy relates to the energy put 'into' the component itself, in terms of extracting it from the ground, then the energy consumed in its processing and manufacturing, together with generated carbon emissions (Bull 2012). It also includes any energy used to transport subcomponents or equipment in any of these stages.

Embodied energy varies for any given material depending upon the efficiency of the production processes. If the source of any given material and the performance of the company producing the material are known, it is possible to establish specific embodied energy and greenhouse emission factors for particular materials, considering exact fuel type, mining place, transportation and delivery consumed energy, and generated carbon emissions. For example, a material manufactured and used in Brisbane has a different embodied energy if the same material is transported by road to Perth.

The quantification of embodied energy and associated greenhouse gas emissions is thus related to process location and is company specific. Embodied energy and carbon emissions can vary from country to country – for example, embodied energy of steel in Australia is 34 MJ/kg (Lawson 2006); in Canada it is 32 MJ/kg (Canadian Architects 2015); and in the US is 40 MJ/kg (Jong & Rigdon 1998). In this regard, for this research, specifications of materials used in Australia, the UK, the US and Canada is provided together with their relevant carbon emissions.

In the case where the source of a material is known, the company can be contacted to provide the information required to calculate accurate embodied energy and carbon emissions for that building material or element. However, the embodied energy of the materials used in Australian construction systems which provide the basis for this study (Table 4.1) have been converted to carbon emissions based on the Australian Government's global average equation of 0.098 kg CO₂ eq = 1 MJ (CSIRO 2014).

4.2.1 Embodied energy and operational energy

It was thought until recently that the embodied energy content of a building was small compared to the energy used in operating the building over its life. Most effort, therefore, was put into reducing operating energy by improving the energy efficiency of the building envelope. However, this is not always the case. For example, research on office construction shows that embodied energy can approach 37 years of operational energy (Moncaster 2007). Embodied energy can therefore be the

equivalent of many years of operational energy. Research by CSIRO has also found that the average house contains about 1,000GJ of energy embodied in the materials used in its construction. This is equivalent to about 15 years of normal operational energy use. For a house that lasts 100 years, this is over 10 per cent of the energy used in its life (Milne & Reardon 2014).

4.2.2 Types of embodied energy and methods of calculation

As already noted, embodied energy includes the energy consumed in mining and processing of natural resources, and then in the manufacture, transport and product delivery. Final energy calculation also depends on where boundaries are drawn in the assessment process. For example, embodied energy will vary if all possible energy use is included – for example, in transporting the materials and workers to the building site; in factory and office lighting; the energy used for the machines that make the materials; and the energy used for urban infrastructure (roads, drains, water and energy supply). Based on these considerations, there are two types of embodied energy which can be considered – the gross energy requirement (GER); and the process energy requirement (PER).

Gross energy requirement (GER) is a measure of the true embodied energy of a material, which would ideally include all the embodied energy used, directly and indirectly. However, measurement of GER is usually impractical.

Process energy requirement (PER) is a measure of the energy usage that is directly related to manufacture of the material. This is simpler to quantify. Consequently, most figures quoted for embodied energy are based on the PER. This would include the energy used in transporting the raw materials to the factory, but not the energy used to transport the final building materials and elements to the construction site.

PER has been used in this study, and accounts for 50 to 80 per cent of GER. Even within this narrower definition, arriving at a single figure for a material is impractical as it depends on the efficiency of the manufacturing process; the fuels used in the manufacture of the materials; the distance materials are transported; and the amount of recycled product used (Milne & Reardon 2014). Each of these factors varies according to product, process, manufacturer and application. They also vary

depending on how the embodied energy has been calculated. Considering these factors, any improvement in the manufacturing and processing stages can cause variation in the embodied energy figures.

Embodied energy calculation can thus vary based on several factors. As a result, figures quoted for embodied energy are broad guidelines only. For example, material manufactured and used in Melbourne has a different embodied energy if the same material is transported by road to Darwin. Thus, one way to reduce relative embodied energy is to use local materials.

Tables 4.1 provides the embodied energies of common building materials in Australian construction systems; these are based on embodied energies of building materials used in British and Canadian construction systems (further detail on these is provided in Appendix A). Australian standard/basic carbon emissions are calculated using the Australian government's global average of 0.098 kg CO_2 eq = 1 MJ (CSIRO 2014), and are presented in column three of Table 4.1.

Australian Building Materials	Standard/Basic Embodied Energy MJ/kg	Standard/ Basic Carbon Emissions Kg/MJ
Kiln dried sawn softwood	3.4	0.333
Kiln dried sawn hardwood	2.0	0.196
Air dried sawn hardwood	0.5	0.049
Hardboard	24.2	2.372
Plywood	10.4	1.019
Stabilized earth	0.7	0.069
Plasterboard	4.4	0.431
Fibre cement	4.8	0.470
Cement	5.6, 5.4 ¹	$0.549, 0.82^{1}$
In situ concrete	1.9	0.186
Precast steam-cured concrete	2.0	0.196
Precast tilt-up concrete	1.9	0.186
Clay bricks	2.5	0.245
Concrete blocks	1.5	0.147
Aluminium	170	16.660
Galvanized steel	38	3.724
Steel	341	AU 3.33, AU 2 ¹

Table 4.1: Embodied energy and carbon emissions of common Australian building materials

Source: Lawson 1996; 2006¹; Sattary & Cole 2012.

Embodied energy values for materials used in Canadian construction systems have been studied for the past several decades by architectural researchers interested in the relationship between building materials and their environmental impacts. These include the embodied energy of building materials based on units of weight (MJ/kg) and volume (MJ/m³) (Canadian Architects 2015). These are further detailed in Appendix A.

Table 4.2 presents embodied energy and relevant carbon emission values from data within the Inventory of Carbon and Energy (2011) database, provided by the Department of Mechanical Engineering in the University of Bath in the United Kingdom.

United Kingdom common building materials	Standard/Basic Embodied Energy MJ/kg	Standard/ Basic Carbon Emissions Kg/MJ
Aggregate	0.083	0.0048
Concrete (1:1.5:3)	1.11	0.159
Bricks (common)	3	0.24
Concrete block (Medium density)	0.67	0.073
Aerated block	3.5	0.3
Limestone block	0.85	
Cement mortar (1:3)	1.33	0.208
Cement	-	1.0^{1}
Steel (general, av. recycled content)	20.1	1.37
Steel	-	2.7
Stainless steel	56.7	6.15
Timber (general, excludes sequestration)	8.5	0.46
Timber		0.30 ¹
Glass fibre insulation (glass wool)	28	1.35
Expanded Polystyrene insulation	88.6	2.55
Polyurethane insulation (rigid foam)	101.5	3.48
Wool (recycled) insulation	20.9	
Slate	0.1–1.0	0.006-0.058
Clay tile	6.5	0.45
Aluminium (general & incl 33% recycled)	155	8.24
Aluminium	-	11.5 ¹

Table 4.2: Embodied energy and carbon emissions of common UK building materials

Source: Inventory of Carbon & Energy (2011); Wilson (2014) (figures with superscript ¹ are from the latter source).

Table 4.3 presents Australian, UK and Canadian PER data (further detailed in Appendix A) relating to building materials and relevant carbon emissions. These are for items produced from 'raw material and virgin natural resources' and 'recycled

materials and recycled content'. Some of these embodied energy figures have been used in the carbon emissions reduction calculations of the case studies in Chapter Six of this research.

Building Materials in AU, UK and Canada	Standard/Basic Embodied Energy MJ/kg	Standard/ Basic Carbon Emissions per Kg/MJ	Standard/Basic Embodied Energy MJ/kg	Standard/ Basic Carbon Emissions per Kg/MJ
	From raw materials &	virgin natural resources	From recycled mater	rials and recycled content
Aggregate	AU, CA 0.1, UK 0.083	CA 0.009 ² UK 0.0048 ¹		
Kiln dried sawn softwood	3.4	0.333		
Kiln dried sawn hardwood	2.0	0.196		
Particleboard	8.0	0.784		
Plywood	10.4	1.019		
Stabilized earth	0.7	0.069		
Gypsum plaster	2.9	0.284		
Plasterboard	4.4	0.431		
Fibre cement	4.8	0.470		
Cement	5.6	0.549		
In situ concrete	1.9	0.186		
Precast steam-cured concrete	2.0	0.196		
Precast tilt-up concrete	1.9	0.186		
Clay bricks	AU 2.5, UK 3	AU 0.245, UK 0.24		
Concrete blocks	AU 1.5, UK 0.67	AU 0.147, UK 0.073		
Polyethylene	US 98, AU 103		US 56, AU	
Thermal insulation			0.5851	
Polypropylene expanded	117			
Aluminium	US 196, AU 170, AU 191 ³	AU 16.660, UK 11.5 ⁴	US 27, AU 8.1, AU8.1 ³ CA 8.1, UK 155,	UK8.25 (33% recycled)
Steel	AU 32 ³ , US40, CA32	UK2.7 ⁴	AU 10.1 ³ , US 18, CA8.9	CA0.872
Steel (general - average recycled content)	AU 32 ³ , US40, CA32		UK 20.7, 20.50 ¹	UK 1.37
Steel (section - average recycled content)	AU 32 ³ , US40, CA32		UK 21.5	UK 1.42
Steel (pipe-average recycled content)	AU 32 ³ , US40, CA32		UK 19.8	UK 1.37
Galvanized steel	AU38	3.724	AU 10.1	
Stainless steel	UK 56.7	UK 6.15		

Table 4.3: Embodied energy and carbon emissions of building materials derived from 'raw material and virgin natural resources' and 'recycled materials and recycled content'

Sources: Australian data – Lawson 1996, 2006; O'Halloran, Fisher & Rab 2008; US data – Jong & Rigdon, 1998; Canadian data – Canadian Architects 2015 | Superscripted sources: 1. Greenspec 2015; 2. Canadian Architects 2015; 3. O'Halloran et al 2008; 4. Institution of Civil Engineers 2012

Lawson (1996) studied the embodied energies of Australian Floor, Wall and Roof construction systems. The embodied energy figures are converted using the Australian global average as previously described, and presented in column three of Tables 4.4, 4.5 and 4.6. These figures have been used in the case studies described in Chapter Six.

Anstrolion Floor construction sustains	Basic Embodied	Basic Carbon
Australian Floor construction systems	Energy MJ/m ²	Emissions Kg/m ²
a. Elevated Timber Floor (lowest level)	293	28.7
b. Elevated Timber Floor (upper level)	147	14.4
c. 110 mm Concrete Slab on ground	645	63.21
d. 125mm Elevated Concrete Slab (temporary framework)	750	73.5
e. 110mm Elevated Concrete Slab (permanent framework)	665	65.17
f. 200mm Precast Concrete Tee Beam/Infill flooring	602	59
g. 200mm Hollow Core Precast Concrete flooring	908	88.98

Table 4.4: Embodied energy and carbon emissions in Australian Floor construction systems

Source: From Lawson (1996) and the case study analyses (Chapter Seven)

Table 4.5: Embodied energy and carbon emissions in Australian Wall construction systems

Australian Wall construction systems	Basic Embodied Energy MJ/m ²	Basic Carbon Emissions Kg/m ²
a. Timber Frame, Single Skin Timber Wall	151	14.8
b. Timber Frame, Timber Weatherboard Wall	188	18.4
c. Timber Frame, Reconstituted Timber W/board Wall	377	36.9
d. Timber Frame, Fibre Cement Weatherboard Wall	169	16.6
e. Timber Frame, Steel Clad Wall	336	32.9
f. Steel Frame, Steel Clad Wall	425	41.7
g. Timber Frame, Aluminium Weatherboard Wall	403	39.5
h. Timber Frame, Clay Brick Veneer Wall	561	63.8
i. Steel Frame, Clay Brick Veneer Wall	650	63.7
j. Timber Frame, Concrete Block Veneer Wall	361	35.4
k. Steel Frame, Concrete Block Veneer Wall	453	44.4
1. Steel Frame, timber weatherboard Wall	238	23.3
m. Cavity Clay Brick Wall	860	84.3
n. Cavity Concrete Block Wall	465	45.6
o. Single Skin Stabilised Rammed Earth Wall	405	39.7
p. Single Skin autoclave Aerated Concrete Block wall	440	43.1
q. Single Skin Cored Concrete Block Wall	317	31.1
r. Steel Frame, Compressed Fibre Cement Clad Wall	385	37.7
s. Hollow-Core Precast Concrete Wall	729	71.4
t. Tilt-up Precast Concrete Wall	818	80.1
u. Porcelain-Enamelled Steel Curtain Wall	865	84.8
v. Glass Curtain Wall	770	75.5
w. Steel Faced Sandwich Panel Wall	1087	106.5
x. Aluminium Curtain Wall	935	91.6

Source: From Lawson (1996) and the case study analyses (Chapter Seven)

Table 4.6: Embodied energy and carbon emissions in Australian Roof construction systems

Australian Roof construction systems	Basic Embodied Energy MJ/m ²	Basic Carbon Emissions Kg/m ²
a. Timber Frame, Timber Shingle Roof	151	14.8
b. Timber Frame, Fiber Cement Shingle Roof	291	28.5
c. Timber Frame, Steel Sheet Roof	330	32.3
d. Steel Frame, Steel Sheet Roof	483	47.3
e. Timber Frame, Concrete Tile Roof	240	23.5
f. Steel Frame, Concrete Tile Roof	450	44.1
g. Timber Frame, Terracotta Tile Roof	271	26.6
h. Timber Frame, Synthetic Rubber Membrane Roof	386	37.8
i. Concrete Slab, Synthetic Rubber Membrane Roof	1050	102.9
j. Steel Frame, Fibre Cement Sheet Roof	337	33
k. Steel Frame, Steel Sheet Roof (commercial)	401	39.3

Source: From Lawson (1996) and the case study analyses (Chapter Seven)

4.2.3 Input-Output embodied energy and hybrid methods

Input-Output embodied energy analysis is the main method used today, and originates from the input-output model described in Leontief (1995). This I-O analysis method was adapted for embodied energy to describe ecosystem energy flows. This adaptation tabulated the total direct and indirect energy requirements (the energy intensity) for each output made by the system. The total amount of energies, direct and indirect, for the entire amount of production was called the Input-Output embodied energy (Leontief 1995).

The I-O method calculates data obtained from industrial manufacturing processes. The Process Energy Requirement (PER) was the focus, even though this was often considered in the context of the Gross Energy Requirement (GER) – and earlier research had found that the PER was usually only 50 to 80 per cent of the GER. However, if rough comparisons of the embodied energy of different materials were required to assist designers to decide between high embodied energy and low embodied energy materials, then the I-O method gave easily comprehensible information. Nevertheless, the approach was clearly incomplete – for example, energy used in transport, a significant consideration as building materials are often heavy or bulky, was often omitted.

Today, there is an increasing need for more accurate and comprehensive analysis of embodied energy, rather than mere relativities. The input-output approach, based on gross national economic data, was initially seen as a way of achieving the completeness that the process approach lacked. However, the modelling of supply and demand, then its translation into energy requirements and greenhouse gas emissions, involves quite sophisticated mathematics, making the method difficult to understand. This has led to development of a hybrid input-output method that enables any amount of industry data to be incorporated within a consistent input-output model. The Centre for Design at RMIT believes the hybrid input-output method is now the preferred technique of assessing embodied energy (Lawson 2006).

Tables 4.7 and 4.8 present a comparison of the embodied energy of some common Australian building materials calculated using the PER approach and the hybrid input-output approach. The I-O figures for Australian building materials are obtained from Lawson (2006) where he used I-O calculations rather than PER calculations used in his earlier 1996 paper. The carbon emissions are calculated based on the Australian government's global average.

The higher accuracy of the I-O approach is indicated by the consistently higher figures, which incorporate upstream requirements for goods and services. For example, in the production of cement, limestone, shale and probably coal have to be mined, processed and transported to the cement works, and this is taken into account in I-O calculations.

This present research and the developed model is based on calculations of embodied energy using process energy requirements (PER). However, calculations using the input-output embodied energy method can also be applied within the research model. Future research using Building Information Modelling (BIM) will make it easier to replace PER with I-O embodied energies

I	PER	Hybrid Input-Output		
Embodied Energy MJ/kg	Carbon Emissions Kg/MJ	Embodied Energy MJ/kg	Carbon Emissions Kg/MJ	
			1	
2	0.196	25.1	2.46	
3.4	0.333	19.9	1.95	
90	8.82	163.4	16.01	
5.6	0.549	16.4	1.607	
1.7	1.167	4.1	0.401	
3.6	0.353	4.0	0.392	
2.5	0.245	2.7	0.265	
12.7	1.245	160.0	15.68	
170.0	16.66	252.6	24.75	
100.0	9.8	378.9	37.1	
34.0	3.332	85.3	8.36	
115.0	11.27	445.2	43.43	
	Embodied Energy MJ/kg 2 3.4 90 5.6 1.7 3.6 2.5 12.7 170.0 100.0 34.0	Energy MJ/kgKg/MJ20.1963.40.333908.82908.82901.1071.1671.1673.60.3532.50.24512.71.245170.016.66100.09.834.03.332	Embodied Energy MJ/kgCarbon Emissions Kg/MJEmbodied Energy MJ/kg20.19625.13.40.33319.9908.82163.4908.82163.4908.82163.4900.54916.41.71.1674.13.60.3534.02.50.2452.712.71.245160.0170.016.66252.6100.09.8378.934.03.33285.3	

Table 4.7: Comparison of PER and hybrid I-O methods for embodied energy and carbon emissions of common building materials

Source: Lawson (1996; 2006).

•	P	ER	Hybrid In	Hybrid Input-Output	
Australian Floor, Wall and Roof construction systems	Embodied Energy MJ/kg	Carbon Emissions Kg/MJ	Embodied Energy MJ/kg	Carbon Emissions Kg/MJ	
Floor					
Elevated timber floor (lowest level)	293	28.71	1289	126.32	
Elevated timber floor (upper level)	147	14.41	873	85.55	
110 mm concrete slab on ground	645	63.21	960	94.08	
110 mm elevated concrete slab (permanent framework)	665	65.17	1617	158.47	
Wall					
Timber frame, timber weatherboard, plasterboard lined wall	188	18.42	999	97.90	
Single skin AAC block, plasterboard lined wall	472	46.26	805	7.73	
Timber frame, clay brick veneer, plasterboard lined wall	561	54.98	1207	118.29	
Steel frame, clay brick veneer, plasterboard lined wall	604	59.19	968	94.86	
Double clay brick, plasterboard lined wall	906	88.79	1243	121.81	
Roof			-		
Timber frame, concrete tile roof, plasterboard ceiling	251	24.6	1269	124.36	
Timber frame, terracotta tile roof, plasterboard ceiling	271	26.56	2200	215.6	
Timber frame, steel sheet roof, plasterboard ceiling	330	32.34	1302	127.6	
Steel frame, steel sheet roof, plasterboard ceiling	483	47.33	1471	144.16	

Table 4.8: Comparison of PER and hybrid I-O methods for some typical residential wall, floor and roof systems

Source: Crawford and Treloar (2004); Lawson (1996; 2006).

4.2.4 Guidelines for reducing embodied energy and carbon emissions

Lightweight construction materials such as timber frames are usually lower in embodied energy than heavyweight construction materials. This may not be the case if large amounts of light but high energy materials such as steel or aluminium are used. There are many situations where a lightweight building is the most appropriate and may result in the lower lifecycle energy use (i.e. in hot, humid climates, sloping or shaded sites, or sensitive landscapes) (Milne & Reardon 2014).

In climates with greater heating and cooling requirements, and significant day/night temperature variations, embodied energy in a high level of well insulated thermal mass can significantly offset the energy used for heating and cooling. However, there is little benefit in building a house with high embodied energy in the thermal mass or other elements of the envelope in areas where heating and cooling requirements are minimal, or where other passive design principles are not applied. Each design should select the best combination for its application based on climate, transport distances, and availability of materials and budget, balanced against known embodied energy content (Milne & Reardon 2014).

The following is a summary of guidelines, tips and techniques for reducing embodied energy.

- Reduce building elements with the highest impact on embodied energy for example, replacing the high embodied energy Portland cement component of concrete with an appropriate lower embodied energy alternative will reduce the embodied energy of concrete. As concrete is such a common building material, such energy savings may be significant (Greenspec 2015).
- Select low embodied energy construction materials (which may include materials with a high recycled content), preferably based on supplier-specific data (Greenspec 2015).
- Give preference to materials manufactured using renewable energy sources (Greenspec 2015).
- Select materials that can be reused or recycled easily at the end of their lives using existing recycling systems (Greenspec 2015), and ensure materials from demolition of existing buildings, and construction wastes, are reused or recycled (Milne & Reardon 2014).
- Use locally sourced materials (including materials salvaged on site) to reduce transport (Milne & Reardon 2014).
- Reduce material use by appropriate design, and increase the resource efficiency of materials and elements (Milne & Reardon 2014). Some very energy intensive finishes, such as paints, often have high wastage levels (Lawson 2006).

The advice, guidelines and tips provided here may result in substantial reductions in embodied energy and related carbon emissions. In respect to reuse and recycling of building materials, this can save up 95 per cent of embodied energy that would otherwise be lost (Milne & Reardon 2014).

4.3 Carbon emissions of the construction process

In the construction industry, designers and other interested parties must be aware that carbon dioxide can be emitted through a variety of mechanisms other than by simply burning fossil fuels to provide a power supply to a building. For example, carbon emissions result from burning fossil fuels in transporting construction workers and materials in both pre-construction and construction stages. Once all contributing factors to embodied energy and generated carbon emissions have been identified, the total embodied energy and relevant carbon emissions can be calculated (UK Indemand 2015).

There are two types of carbon emissions that need to be considered in construction: the operational carbon and the embodied carbon. Operational carbon is the carbon dioxide released over the lifetime use of a building, including that generated by heating, cooling, lighting, and so on. Embodied carbon refers to the carbon dioxide released from materials extraction, transport, manufacturing, and related activities, including end of life emissions (Sustain 2014; Wynn 2012).

Embodied energy has a significant impact on a building's (embodied) carbon emissions, and this proportion has been steadily increasing over recent decades as technology has developed and operational energy use has reduced. In addition, the recurring embodied energy also needs to be considered, this being defined as the energy required for maintenance, refurbishment and replacement of components during the lifetime of the building, a process which also releases (operational) carbon. The ratio of embodied carbon to operational carbon has grown to approximately 40:60 as shown in Table 4.9 (Bull 2012).

Initial material investment 1-2 years construction		Deconstruction 0-6 months	Building in use 30 years operation	Operation (increased efficiency and fabric improvements) 15-20 Years
21%	8.5%	8.5%	45%	17%
38% Total Embodied Carbon		62% Tot	tal Operational Carbon	

Source: Bull (2012)

Currently embodied carbon can be equivalent to as much as 37 years of operational carbon (Moncaster 2007). This figure will increase as operational carbon is decreased with implementation of zero carbon operational strategies (Centre for

Sustainable Development 2014). Under such circumstances, the impact of the building sector on the environment could be reduced significantly by taking into account bioclimatic design principles.

Carbon emissions generated by a specific material or construction element can vary considerably – for example, if the energy and electricity used for the processes were generated by hydro or coal generation, with a ratio of around 1/250 (Table 4.10). The type of energy resources used in production and construction processes can thus play a major role in carbon emissions reduction, a factor considered in the bioclimatic design principles of the developed model.

Table 4.10: The carbon intensity of electricity generation (all figures in g co₂eq/kwh)

Hydro	Ocean	Wind	Nuclear	Biomass	Solar CSP	Geothermal	Solar PV	Natural Gas	Oil	Coal
4	8	12	16	18	22	45	48	469	840	1001

Source: Intergovernmental Panel on Climate Change (IPCC 2011); Wilson 2014

As Table 4.10 shows, alternatives to fossil fuels are many and varied, ranging from solar energy in its various forms, to wind, geothermal, natural gas, nuclear fission and so on. It is sometimes suggested that nuclear energy is not associated with the production of greenhouse gases. This is untrue. The energy associated with mining, transport of uranium, and nuclear waste generates substantial quantities of greenhouse gases. Additionally, when the nuclear fuel cycle is examined, it is clear that considerable amounts of other potential pollutants are produced at various stages. For example, while a 1000MW nuclear power plant consumes only 36 tonnes of processed and enriched uranium fuel, this necessitates the mining of 85.5x10³ tonnes of ore which produces toxic tailings containing arsenic, cadmium, and mercury as well as radionuclides (Masters 1991).

4.4 Converting embodied energy to carbon emission (CO₂) equivalent

The term 'carbon' is frequently used as shorthand for either carbon dioxide (CO_2) or carbon dioxide equivalents (CO_2 -e), which includes both CO_2 and other gases with significant global warming potential, meaning that they tend to trap heat in our atmosphere. Once each greenhouse gas is on the same carbon-equivalent scale, emissions for a specific material can be added up to get its total embodied CO_2 -e. A lot of the embodied carbon of a product or building comes from energy consumption (embodied energy), but not all of it.

The embodied carbon of a product usually includes CO₂-e emitted from the extraction of raw materials through to the final manufacture of the product, sometimes referred to as 'cradle-to-gate'. The embodied carbon of new construction includes this, plus transport and installation of all products and materials that make up the building.

Some measures (gross energy requirement, input-output and hybrid method) include emissions from construction activity, such as equipment use, transportation of workers to and from the job site, and even land disturbance in construction (which causes loss of carbon stored in healthy soils). As with the more comprehensive lifecycle analysis, the definition of what is and is not included in the calculation has to be consistent to be useful. For building products, work is ongoing in defining these boundaries through product category rules, which clearly explain the types of embodied energy used.

An increasing proportion of the total energy used and carbon emissions for highperformance buildings come from its materials and products. This is not only because less energy is used in operation, but also because buildings may be using more carbon-intensive materials to achieve lower energy use. To minimise climate change, the goal is to reduce the total quantity of greenhouse gases emitted into the atmosphere, and reducing the embodied carbon of building materials has an important role (Building Green 2014).

The embodied energy of a building or building material is the simple and most convenient measure of its environmental impact. The greater the embodied energy, the greater are its carbon emissions and environmental impacts. Another reason to address embodied carbon is that reductions in carbon emissions of materials have an immediate benefit, whereas the carbon reductions through operations accrue over a long period of time. By taking embodied carbon into account, design is for carbon emissions reduction. Embodied energy, like operational energy, can be directly related to the generation of greenhouse gases such as CO₂, although energy derived from different fossil fuel sources will vary in its associated CO₂ emissions. On average, approximately 0.1 tonnes of CO₂ are produced per gigajoule of embodied energy (Lawson 2006). Typical embodied energy units used are MJ/kg (megajoules of energy needed to make a kilogram of product), and tCO₂/kg (tonnes of carbon dioxide created by the energy needed to make a kilogram of product).

Converting MJ to tCO₂ is not straightforward because different types of energy (oil, wind, solar, nuclear, and so on) emit different amounts of carbon dioxide, so the actual amount of carbon dioxide emitted when a product is made will be dependent on the type of energy used in the manufacturing process. For example, the Australian Government gives a global average of 0.098 tCO₂ = 1 GJ. This is the same as 1 MJ = 0.098 kg CO₂ = 98 g CO₂, or 1 kg CO₂ = 10.204 MJ (CSIRO 2014).

4.5 Review of techniques to reduce construction carbon emissions

This section discusses potential ways in which carbon emission reductions can be achieved in the construction process. There are several illustrative examples given which are identified from the six case studies which are considered in this research.

4.5.1 Reuse and recycling of construction materials

The 'throw-away' mentality of the past needs to change in order to preserve our environment. One important facet relating to this is that reusability of building materials and elements must be implemented in global construction activities. Reusability is often misinterpreted for recycling. Recycling refers to taking the construction materials, breaking them down into their raw materials, and creating new construction products. Reuse refers to extending the life of a building material or element (Waste Watch 2004). Additionally, reuse of construction materials and elements does not require more energy like recycling, because it relies on the embodied energy present within the materials (Danciu 2012).

Construction materials have a limited life cycle before they become waste. Reuse thus extends the lifespan of a construction product. This means that through reuse, materials can last longer and pollution and waste can be reduced. Reusability has become globally prominent, and more integrated into the policies and procedures of governments, industries, and communities through advances in technology and globalisation (World Federation of Engineering Organizations 2011).

The common theme in any reusability project is to reduce waste, reduce emissions, and decrease the environmental impact of construction (World Federation of Engineering Organization 2011). In fact, up to 80 per cent of construction waste is actually made up of discarded materials which are ideal for re-use or recycling, and which represent significant potential for use in this market. This market is already developed in the United States, Germany, Britain and some European countries, but has not yet to be fully developed in Australia (UN Environmental Protection Agency UNEPA 2015).

Most of the resources used in house construction are suitable for reuse or recycling. Table 4.11 identifies materials suitable for recycling or reuse in a typical Australian house.

Comments			
Almost all bricks and concrete – the heaviest building materials – can be recycled, making significant savings on landfill fees.			
Depending on their condition, terracotta tiles can be either sold for re-use or collected free for recycling. Like bricks and concrete, landfill fees for disposal of heavy tiles can be easily avoided.			
Up to 75 per cent of wood products can be re-used or recycled.			
Easily accessible items of value can be resold.			

Table 4.11: Higher value materials typically recovered in house deconstruction

Source: Environment Protection Authority NSW (EPA 2015).

Of the total building-related materials generated during construction and demolition, the United Nations Environmental Protection Agency (UNEPA) estimates that only 40 per cent are reused, recycled, or sent to waste-to-energy facilities; the remaining 60 per cent are sent to landfill (UNEPA 2015). Reuse and recycling of building materials commonly saves about 95 per cent of embodied energy that would otherwise be wasted (Milne & Reardon 2014). There is thus great potential to reduce carbon emissions through recycling and reuse of construction materials, as will be considered in the following sections of this chapter.

4.5.2 Reduce materials use in design

The Green Building Council of Australia aims to work with customers and design consultants in the design and tender stage to reduce the tons of steel and other resources used in projects through design efficiency. Both environmental improvement and project cost savings are the result. (Green Building Council of Australia GBCA 2014a).

As an example of reduced materials in design, the London Olympics stadium (Figure 4.1) was constructed using only one tenth of the steel required to build Beijing 'Bird's Nest' stadium. Additionally, the amount of carbon output of the stadium is only an eighth of the Beijing stadium (Cable News Network 2012; Craven, 2012). On a similar note, aluminium in the roofs of the London Aquatics Centre and the velodrome has a high percentage of recycled content; and leftover gas pipes make up the Olympic Stadium's ring beam, reducing the need for new steel to be produced (Inventory of Carbon & Energy 2011).

Calculating the reduction of carbon emissions achieved in the London Olympic Stadium through the decreased materials in design as follows – the basic carbon emissions level of 39.3 Kgs CO_2/m^2 was reduced to 8.02 Kgs CO_2/m^2 . There was thus a 79.6 per cent reduction in released carbon emissions from the London Olympic stadium.



Figure 4.1: London Olympic Stadium Source: London attractions information (2016)

4.5.3 Use of appropriate construction materials

There is significant potential for improving resource efficiency within the construction industry by using construction materials and elements with a high recycling and 'complete reuse' potential. On a much larger scale, complete steel buildings can be reused. An example is the British Pavilion at the Seville Expo in 1993 (Figure 4.2). This innovative, energy efficient steel building was designed to be

reused after the Expo (Steel Construction Information 2014) in fact it was designed for deconstruction and use elsewhere.

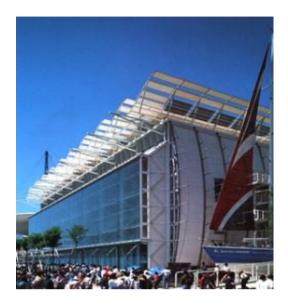


Figure 4.2: British Pavilion, Seville Expo 93 Source: Steel Construction Information (2014)

To reduce environmental impact, a system is needed that facilitates reuse through a range of mechanisms including – a reuse management model; careful demolition; establishment of storage sites; maintenance of a stock of reusable members; creation of performance evaluation and fabrication procedures for reusable members (Frangopol 2011).

A study done by Aye et al. (2012) demonstrated that use of a prefabricated steel system produces significant reductions in the consumption of raw materials of up to 50.7 per cent by weight. A further benefit of a prefabricated system is that a significant portion of the structure can be reused at the end of the building's life. This may result in a significant reduction in waste being sent to landfill, and reduced requirements for additional new materials. However, the energy embodied in the prefabricated steel buildings was up to 50 per cent greater than that for concrete buildings. This was offset by the fact that at the end of the building's useful life, up to 81.3 per cent of the embodied energy of the initial steel building can be saved by reuse of the main steel structures of the prefabricated modules and other components in further construction (Aye et al. 2012).

4.5.4 Reuse of building elements and building spaces

In the last decade, reusability has become a rising global trend and countries have been actively pursuing policies of reusability to prolong the use of construction materials and other items of what was once 'waste'. The common theme in any reusability project is to reduce waste, reduce emissions, and decrease the environmental impact of construction (World Federation of Engineering Organizations 2011). New technologies for demolishing buildings also contribute to reducing waste because most building elements can be reused in the deconstruction materials market (Architecture & Engineering 2015). This market is already developed in the United States, Germany, Britain and some European countries, but has not yet to be fully developed in Australia (UNEPA 2015).

Reuse and recycling of structural building elements can play a significant role in reducing the depletion of natural resources, not only through compliance with new standards, but also by minimising costs through efficient use of resources, solving problems interactively within design teams, having the knowledge and skills to assess and adapt existing buildings, and bringing an open-minded and innovative approach to design (Steel Construction Information 2014).

Where a building has been designed with deconstruction in mind, much of the building material and elements can be reused. An example is provided in family housing units in Berlin which reused the complete walls, floor plates and ceilings from a demolished communist-era 11-storey tower block (Figure 4.3). The only significant energy costs arose from the transportation of the five-tonne panels and the use of a portable crane to lift them into place on site. For the residential project, the demolition firm provided the panels free of charge, which saved them the disposal cost and the architects the materials cost (CCAA 2015).

Another German example is where the prefabricated concrete walls of Stalin-era apartment buildings were upcycled into two-story villas (Figure 4.4). After deconstruction, the panels were resized or taken as designed after stripping the wallpaper (High Concrete Group 2014).



Figure 4.3: Upcycled prefabricated concrete walls – the prefabricated concrete walls of an eleven-story Stalin-era apartment buildings were upcycled into two-story villas Source: High Concrete Group (2014).



Figure 4.4: Reused prefabricated concrete walls – designing future buildings for deconstruction is vital for facilitating higher levels of reclamation and re-use. Source: High Concrete Group (2014).

The basic carbon emission of a square metre tilt-up precast concrete wall is 80.16 kg CO_2/m^2 – which was decreased to 16.26 kg CO_2 / m^2 by deconstructing and downsizing the prefabricated concrete walls of these Stalin-era apartment buildings. Thus, a potential reduction of 79.72 per cent in possible carbon emissions from the two-story precast concrete walls was achieved. Additionally, this program also saved 14.7 million tonnes of waste from ending up in landfill (Fischer 2006; Adaptivereuse 2015).

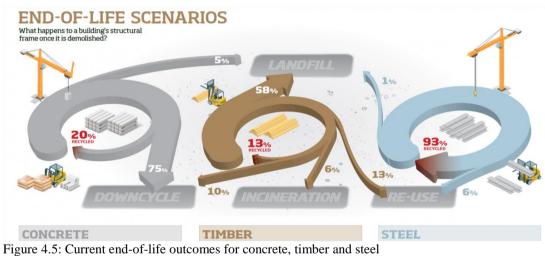
Research on residential case studies has shown that costs for salvaged materials are 20 to 50 per cent less than the cost of new materials. Economic benefits are mainly from salvaged materials, but also include lower landfill fees, and less future cost for replacement of materials. The cost of deconstruction was also 37 per cent lower than for demolition (Kernan et al. 2001).

According to Morgan and Stevenson (2005), economic benefits of deconstruction include increased flexible use and adaptation of property at minimal future cost; maximized value of building elements; reduced quantity of materials going to landfill; and reduced risk of financial penalties in the future through easily

replaceable building elements. Deconstruction and design for deconstruction can redirect waste back into the building life cycle, thus conserving resources, energy and landfill space, as well as providing other associated environmental, economic and social benefits (Bales 2008).

4.5.5 Recycling and reuse of steel from recycled content

It is estimated that the construction industry consumes some 420mt of materials annually, and generates some 90mt of construction, demolition and excavation waste, of which 25mt ends up in landfill. A significant proportion of this are waste steel products. In construction, most steel products are large, and can be easily captured at the end of a building's life. Capture rates are on average 96 per cent (Steel Construction Information 2014) (Figure 4.5).



Resource: (Steel Construction Information 2014)

The primary method used in the production of structural steel shapes and bars is the electric arc furnace, which uses 95 to 100 per cent old steel to make new steel. In this process, producers of structural steel are able to achieve up to 97.5 per cent recycled content for beams and plates, 65 per cent for reinforcing bars, and 66 per cent for steel decks. Total recycled content varies from mill to mill. Steel for products such as soup cans, pails, drums and automotive fenders is produced using the basic oxygen furnace process which uses 25 to 35 per cent old steel to make new products (Kang & Kren 2007).

4.5.6 Reuse of structural steel

Steel buildings and steel construction products are generally deconstructable and reusable. This potential is illustrated by the large number of temporary works systems that use steel components, e.g. scaffolding, formwork, sheet piles, and so on. Provided that attention is paid to eventual deconstruction at the design stage, there is no reason why nearly all of the steel building elements should not be regarded as a vast 'warehouse of parts' for future use in new applications.

Research carried out by the Steel Construction Institute (SCI) has estimated that there is around 100 million tonnes of steel in buildings and infrastructure in the UK. This stock of steel is an important and valuable source for materials reuse, and there is research currently being conducted to identify how this can be done in the most effective fashion (Steel Construction Information 2014).



Figure 4.6: Steel elements from demolition in Toowong, Australia Source: Author (2015).



Figure 4.7: Materials from house demolition in Australia Source: EPA (2015).



Figure 4.8: Floating shipping container apartments in Denmark Source: Stella (2016).

Figures 4.6, 4.7 and 4.8 illustrate examples of sources and uses of steel elements and products that can be reused at both the product and the building level. One innovative example is the use of old shipping containers to assist in solving the student housing shortage in Denmark (Stella 2016).

Many industries commonly reuse steel components. Steel construction products are often reusable including steel piles (sheet and bearing piles); steel structural components including hollow sections; and light gauge steel products such as purlins and rails (Steel Construction Information 2014). Structural steel reuse can occur either on an individual element level, for example in the reuse of steel beams (e.g. in the BedZED project [Bioregional n.d.]), or on a component level, (e.g. a steel trusses, as demonstrated in the construction of the Ottawa Convention Centre, which reused

nine 160ft long trusses from old buildings on that site [O'Connor 2004]). Steel is particularly suited for reuse due to its durability and robustness during deconstruction (UK Indemand 2014). Figure A.1 in Appendix A presents possible structural construction systems made of reused materials.

There are three barriers to reuse of structural steel. First, although new steel is certified based on a process audit, reused steel must be re-certified by mechanical testing to confirm its grade, and this is a costly process. Second, although deconstruction rather than demolition can be profitable due to the value of reclaimed materials and components, it still takes longer, and delays to a construction project program are undesirable. Third, because reuse of components is still relatively uncommon, there is a supply problem – for example, finding the appropriate steel section sizes and lengths can be difficult and expensive (Steel Construction Information 2014). In contrast, non-structural materials can also be salvaged and reused, and this is more common than structural steel reuse as re-certification is not required (UK Indemand 2014). Other technical and logistical barriers to reuse of structural steels are summarised in Table 4.12.

Table 4.12: Barriers to reuse of structural steel

Technical barriers

- Lack of standardisation of components
- Ensuring and warranting the performance of reused components
- Lack of detailed knowledge of a product's properties and in-use history (this may be important, for example, if the component has been subject to fatigue loading)
- Quality assurance of reused products

Logistical barriers

- Lack of commercial drivers for reuse
- Cost of storage, cataloguing, refurbished products, etc.
- Cost of testing to verify and guarantee properties
- Client expectation that 'second-hand' products should be cheaper than new ones

Source: Sattary and Thorpe (2011); Steel Construction Information (2014).

Structural engineers have an important role in respect to this process – to produce construction designs that allow for reuse of steel and other components (Bull 2012). Steps that they can take to maximise the opportunities for reusing structural steel include:

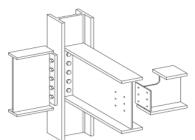


Figure 4.9: Reuse strategy, End plate beam to column, beam-to-beam connections Source: (Steel Construction Information 2014)

- Using bolted connections in preference to welded joints to allow structures to be dismantled during deconstruction (Figure 4.9)
- Using standard connections including bolt sizes and spacing of holes
- Ensuring easy and permanent access to connections
- Where possible, ensuring that the steel is free from coatings or coverings that would prevent visual assessment of its condition
- Minimising use of fixings to structural steel elements that require welding, drilling of holes, or fixing with Hilti nails – clamped fittings are preferable where possible
- Identifying the origin and properties of components (e.g. by bar-coding, etagging, or stamping) and keeping an inventory of products
- Use long-span beams as they are more likely to allow flexibility of use and to be reusable (Steel Construction Information 2014).

In conclusion, reuse of steel construction elements is becoming more prominent across the world. Particular countries may implement reuse in different ways and for different reasons. However, this trend will help create a better future for everyone (World Federation of Engineering Organizations 2011).

4.5.7 Recycling and reuse of bricks

Reuse and recycling options for bricks are economically viable because costs associated with sending bricks and concrete to landfill are rising. Demolition is also more expensive than deconstruction – brick disposal costs to landfill are \$115/tonne, recycling uncontaminated material costs \$24/tonne. Many companies will also collect bricks free of charge and typically sell them for \$0.50 each, making reuse an attractive option (Brick Development Association [UK] BDA 2014; Department of Environment, Climate Change and Water NSW 2014).

In the building of the London Olympics, 28 per cent of construction used recycled materials. Some materials were reclaimed for re-use as aesthetic and practical features in the Olympic Park – including 660 tonnes of various brick types, 176 tonnes of paving material, and 5,400 m of kerbing (Smith 2012).

Since the early days of ecologically sustainable building, most brick manufacturers have incorporated recycled materials into their brick production in different ways. Materials used as recycled content can come from either pre-consumer or post-consumer sources. For example, 'Green Leaf Bricks' are newly manufactured fired masonry bricks composed of 100 per cent recycled materials, designed and engineered especially for sustainable construction (Green Leaf Brick 2016).

Bricks may incorporate recycled materials such as overburden from mining, washings from aggregate processing, grog, sawdust and metallic oxides (BDA 2009). Research demonstrates a potential 40 per cent energy saving in brick manufacturing by using 67 per cent recycled container glass brick grog (BDA 2014; Tyrell & Goode 2014).

4.5.8 Use of fly ash in bricks and concrete

In a standard concrete mix, the cement component commonly accounts for approximately 70 to 80 per cent of the embodied energy. Fly ash, being a by-product of coal fired electricity generation, has a relatively low embodied CO_2 content related to its manufacture, estimated at 0.027kg of CO_2 emissions per tonne, 3 per cent that of Portland cement manufacture (Ash Development Association of Australia 2013).

The manufacture of Portland cement is an energy intensive process that releases approximately 0.820 tonnes of CO_2 emissions for each tonne of cement produced. A strategy to produce more sustainable concrete is to replace a portion of the cement component with one or more supplementary cementitious materials such as fly ash. The benefits of using fly ash include reduction in CO_2 emissions and embodied energy; reduction in resource use; re-use of industrial by-products as alternative raw materials; and sustainability achieved through efficient design and enhanced durability (Ash Development Association of Australia 2013). In respect to bricks, US-made fly ash brick gains strength and durability from the chemical reaction of fly ash with water. However, 85 per cent less energy is used in fly ash brick production than in fired clay bricks. A potential 85 per cent reduction in released carbon emissions in brick manufacturing can thus be achieved (Volz & Stovner 2010; Structure Magazine 2014) (Figure 4.10).

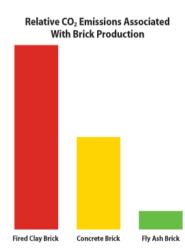


Figure 4.10: CO₂ emissions of different brick types Source: Volz and Stovner (2010); Structure Magazine (2014);

As fly ash brick technology produces bricks without using coal, it has the potential to eliminate carbon emissions from the brick-making industry which burns huge amounts of coal and emits millions of tons of carbon dioxide annually. Additionally, the process uses fly ash, previously an unwanted residue from coal-fired power plants. The World Bank is supporting fly ash brick production by allowing entrepreneurs to earn carbon credit revenues. So far, the project has allowed 108 fly ash brick plants to earn around \$3.2 million (World Bank 2012).

4.5.9 Use of recycled aggregate in concrete

Recycling concrete and using aggregates is an increasing practice at construction sites. For example, in 2006 the Brookhaven National Laboratory saved over \$700,000 in construction costs by using Recycled Concrete Aggregate (RCA) from the demolition of ten structures (Craven 2012). Another example was in construction of the 2012 London Olympics Park, where over 200 buildings were dismantled, and the materials reused (Ingenia 2014; Learning Legacy 2014).

The sustainability summary of the London Olympics notes that a quarter of all materials used in the buildings were recycled – this included 400,000 tonnes of concrete which used up to 76 per cent recycled aggregate ('stent', a by-product of the Cornish china clay industry), and 40 per cent recycled cement substitute (granulated blast furnace slag) in the concrete. Sixty per cent of recycled content was used in the interior block work; recycled glass in the wall insulation; and recycled plastic for the seats. Additionally, the foundations of the Aquatics Centre, Handball Arena, and Olympic Stadium all used concrete containing more than 30 per cent recycled materials in place of gravel, which otherwise would have had to be mined and transported to the site. Overall, around 90 per cent of materials left over from construction, demolition and excavation works were reused or recycled on site (Ingenia 2014; Learning Legacy 2014).

The Gulf Organisation for Research and Development has found that the recycling of concrete, brick and masonry rubble as concrete aggregates is an important way to contribute to a sustainable material flow. Experimental studies were carried out on the improvement of RCA performance. Beneficial effects from polymer based treatments applied to RCA were obtained, especially lower water absorption and better fragmentation resistance (Spaeth & Tegguer 2013).

To achieve emissions reduction in construction, many countries are focusing on recycled concrete aggregates as they are proven to be practical for non-structural concrete, and to a limited extent for some structural-grade concrete. In Australia, there are a number of manufactured and recycled aggregates readily available in certain localities, and these have potential to be used in construction. Air-cooled blast furnace slag and manufactured sand are two good examples of concrete aggregates (Cement Concrete & Aggregates Australia CCAA 2015). Additionally, the use of milled waste glass as partial replacement for cement is estimated to effectively overcome the limitations of recycled aggregate (Nassar & Soroushian 2012).

Recent research (e.g. Katz 2003; Tam, Gao & Tam 2006; Kotrayothar 2012) has demonstrated that the use of recycled aggregate in both structural and non-structural concrete applications has become technically feasible and commercially viable (Eguchi et al 2007). For example, recycled concrete aggregate has now been used in

a wide range of construction projects in Germany, Hong Kong, Britain, Norway and Australia, confirming the practicality of its use. Many countries including Australia have thus established specialised standards for recycled concrete aggregates (Yiu, Tam & Kotrayothar 2009; Kotrayothar 2012; Tierney 2012). Concrete recycling is thus a method that is an attractive option to achieve greater sustainability and cost savings in construction. Using concrete waste as aggregate also solves the critical shortage of natural aggregate anticipated in the near future (Portland Cement Australia 2014)

It is generally accepted that when natural sand is used, from 30 to 80 per cent of natural crushed coarse aggregate can be replaced with coarse recycled aggregate without significantly affecting any of the mechanical properties of the concrete. As replacement amounts increase, drying, shrinkage and creep will increase, and tensile strength and modulus of elasticity will decrease. However, compressive strength and freeze-thaw resistance are not significantly affected (Uche 2008; Kwan, et al. 2012; Portland Cement Australia 2014). When the mix design method proposed by the Department of Environment in the UK was used, a target strength was achieved even when 80 per cent of the total coarse aggregate content was replaced by the RCA (Kwan et al. 2012). It is also apparent that at 75 per cent or less RCA replacement, the concrete compressive strength is well above the designed characteristic strength of grade 30 concrete, hence it can be used for structural grade concrete work (Uche 2008).

According to Tam (2009), from experience gained in Japan in recycling of concrete, Australia should develop a unified policy on concrete recycling; seek financial support from the government to implement recycled concrete use; and develop clear technical specifications and standards on the use of recycled aggregate for structural applications. Table 4.13 presents the current recycled aggregate concrete codes in the US, UK and Australia.

Country	Recycled Aggregate (Type/Name/Classification)	Maximum RCA Substitution	Maximum RCA 28 Day, Cylinder Strength
		100%	20MPa
USA	LCA	25%	50MPa
		60%	NS Concrete
	DCA	No restriction	40MPa
UK	RCA	20%	Designated concrete, 20 to 40 MPa
UK	LCA	No restriction	No restriction
	RA		16 MPa
AU	Class 1A - RCA	30%	40 MPa
	Class 1B - RCA	100%	25 MPa

Table 4.13: Summary of recycled aggregate concrete codes in the US, UK and Australia

Source: Chisholm (2011). LCA = Leftover Concrete Aggregate; RCA = Recycled Concrete Aggregate; RA = Recycled Aggregate; NS = Non-Structural Concrete,

4.5.10 Replacement of cement with geopolymers

Geopolymer has a history starting in the 1940s, and has attracted significant academic research, but has yet to achieve significant market use. However, the use of geopolymer concrete is increasing, in part motivated by the sustainability benefits of using a binder system composed almost entirely of recycled materials. Wagners are an Australian company supplying a proprietary geopolymer concrete for both precast and in-situ applications in the construction industry (Aldred & Day 2012).



Figure 4.11: 10.8 metre geopolymer beam with vaulted soffit being craned into position Source: Aldred and Day (2012)

Geopolymers were first used in some concrete applications in the Soviet Union after World War Two, being known then as 'soil-cements'. Numerous structures have been constructed since then, though no commercial entities have carried this through to an industrial scale (Zeobond Group 2014). The University of Queensland's Global Change Institute is the world's first building to successfully use geopolymer based cement for structural purposes (Geopolymer Institute 2014); and the Wellcamp Airport in Toowoomba is the first airport in the world where geopolymer cement has been used (Welcamp 2014).

Replacing the high embodied energy Portland cement component of concrete with an appropriate lower embodied energy alternative is a simple way of reducing the embodied energy of concrete. Because concrete is such a universal building material, such energy saving may be significant (Lawson 2006).

Fly ash geopolymer can be used as binding material for partial replacement of cement in geopolymer concrete (Lohani et al. 2012). The opportunities for using fly ash in production of sustainable concrete are extensive and will continue to increase. Related to this, Louisiana Technology University is currently working to develop a 'green' type of concrete that uses geopolymers to reduce greenhouse gases by as much as 90 per cent compared to regular Portland cement (Building industry council 2014).

Replacing some of the cement content in concrete with sustainable construction materials such as fly ash is arguably the most efficient and economical means of reducing CO_2 emissions of concrete (Ash Development Association of Australia 2013). Key elements that could be considered to result in a more sustainable outcome when using such concrete are – less resource depletion; reduced emissions in production of the material or components (embodied energy); reduced water consumption; and waste avoidance and reduction (Geiger 2015).

Geopolymer represents a sustainable and economical binding material as it is produced from industrial by-products such as fly ash (Nath & Sarker 2014). Research has shown that fly ash based geopolymer concrete cured in ambient conditions can be modified for desirable workability, setting time, and compressive strength using ground granulated blast-furnace slag as a small part of the binder (Olivia & Nikraz 2012). Full replacement of Portland cement by geopolymer can result in a 97 per cent reduction in greenhouse gas emissions. However, where Portland cement has been replaced with geopolymer concrete mixes based on typical Australian usage, there is potential only for a 44 to 64 per cent reduction in greenhouse gas emissions, with associated reductions in financial costs (McLellan et al. 2011). For instance, the released carbon emissions for a one square metre '200 mm concrete slab on ground Floor' (Case Study 4: Civil Engineering Laboratory building, USQ) are 58.12 Kgs CO_2/m^2 . Use of geopolymer concrete can reduce this to 29.73 Kgs CO_2/m^2 , representing a potential 48.84 per cent (28.39 kg) reduction in the released carbon emissions, and reducing the total costs of cement production by up to 50 per cent (Calculation is illustrated in Table A.A.8, Appendix A).

In 2014, a project submitted to the Low Carbon Living Capital Research Centre (LCLCRC) aimed to gather field data from geopolymer real-life constructions to develop greater confidence in geopolymer use. Using field and laboratory data, a comprehensive handbook for geopolymer specification was developed and published through Standards Australia. Additionally, a pilot program developed lightweight aggregates based on fly ash to produce lightweight concrete, which reduces energy usage in buildings. Current technologies for producing lightweight aggregates using sintered fly ash involve carbon intensive processes. This project aims to develop low carbon processes based on geopolymerisation and alternative methods for producing aggregates from fly ash (LCLCRC 2015).

The project is supported by a range of partner organisations including the Ash Development Association of Australia (ADAA), the Australian Standard Associations (ASA), the University of New South Wales (UNSW), Swinburne University of Technology (SUT), and others. The project coordinators also have support from the main Australian geopolymer concrete suppliers, including Zeobond Pty Ltd and Wagners Concrete Pty Ltd, and other interested parties. The project is being funded by these various partner organisations, and this research has great potential in geopolymer concrete and high-volume applications of fly ash (Ash Development Association of Australia 2013).

An example of the use of geopolymer concrete in block wall construction is provided in the carbon emissions for a one square metre 'cavity concrete block wall' (Case Study 4: Civil Engineering Laboratory building, USQ). Emissions can be reduced from 37.73 Kgs CO_2/m^2 to 23.28 Kgs CO_2/m^2 by use of geopolymer cement, representing a potential 38.29 per cent (14.45 kg) reduction in released carbon emissions. The detailed calculation is presented in Table A.A.9 in Appendix A.

4.5.11 Emissions reduction in transportation

Transport activity is a major source of carbon emissions due to the use of fossil fuels. Transport produced 83.2 Mt CO₂-e or 15 per cent of Australia's net emissions in 2010. Emissions from this sector were 32 per cent higher in 2010 than in 1990. Road transport is the main source of transport emissions (Macintosh 2007; Carbon Neutral 2015). In respect to construction, environmental pollution relates to mining, logging and transportation of raw materials, and then to the manufacture and transportation of the finished products, and their installation on the construction site.

Waste and debris from demolished and dismantled buildings can be reused as an aggregate. This occurred in construction of the 2012 London Olympics Park where over 200 buildings were dismantled, and around 98.5 per cent of the debris was reclaimed and reused in production of the thousands of tonnes of concrete produced on site. Reduced use of fossil fuel was also achieved due to use of nearby waterways to transport materials and waste out of the park (Inventory of Carbon & Energy 2011; Aggregate Industries 2014). Calculations in Table A.A.10 (Appendix A) indicate that reduced transportation emissions by not carrying the waste to the landfill was 15.42 kg CO_2/m^2 for each square metre of 200 mm concrete slab laid.

4.5.12 Using sustainable types of transportation

The carbon emissions associated with construction are relatively small when compared to other aspects of construction operations. However, the use of sustainable modes of transport is still important. The energy consumption of different modes of transport is presented in Table 4.14 – thus, it is important to reduce road transport where possible. For example, the Tata Steel Group manages shipping and logistic operations. Their policies towards a shift to sustainable modes of transport for construction materials include – using water and rail in preference to road transport; road haulage weight optimisation; linking outward journeys with return journeys to minimise empty running; and improving the efficiency of the contracted and sub-contracted haulage fleet (TATA Steel 2015).

Mode	Energy Consumption	Energy Consumption
WIUUC	(MJtonne/km) United Kingdom	(MJtonne/km) Canada
Road	4.50	1.18
Rail	0.60	0.49
Ship	0.25	0.12

Table 4.14: Transportation energy consumption: United Kingdom and Canada

Source: Lawson (1996).

For reuse and recycling to become established in the Australian construction industry, several supporting initiatives will need to be enabled. Salvage markets and speciality suppliers of used building materials will have to increase in number and scope of offerings. Databases detailing the salvaged materials on offer will need to be established – providing life cycle inventory data, assembly and disassembly instructions, and warranty information on the building materials. Buyers and sellers need to know the full origin, use and impact of the materials or assemblies they are to exchange (Bales 2008).

Specifications in a building contract that demands use of recycled materials can facilitate increase in reuse. The following items are usually easy to locate and reuse – recycled steel reinforcements, recycled or plantation timber, recycled concrete and bricks. For example, there is an online initiative linking buyers and sellers of building products called Construction Connect in Sydney. Similarly, Eco Buy lists suppliers of second-hand construction and building materials. Buying recycled products increases the market for them, making it more viable for businesses to supply them (Hawkesbury City Council 2014).

4.6 Barriers to emission reduction in construction

The recovery process for deconstructing materials used in building can be time consuming and expensive. Additionally, many buildings were not constructed with future recovery of materials in mind. In this respect, recovered non-structural materials are more commonly used than structural components as certification is not required.

There are specific barriers to reuse of some construction elements. For example, reused steel must be recertified before use, and this is costly (UK Indemand 2014). Finding the appropriate steel section sizes and lengths can also be difficult and

expensive (Steel Construction Information 2014). There are also barriers to use of geopolymer concretes due to lack of standard specifications and unfamiliarity of their use (Wilson & Tagaza 2006).

Asbestos contamination is also a well-documented problem, and still presents a significant issue in waste derived from demolition and renovation works. High recovery rates for materials are achieved when materials are captured closer to the source, before there is opportunity for mixing with other wastes (Edge Environment Pty Ltd 2012). A summary classification of barriers to emission reduction is presented in Table 4.15

Table 4.15: Barriers to emission reduction

Market barriers

- Guaranteed quality and quantities of reused materials are difficult
- Reuse today is rare, there is a supply problem
- Limit and lack of market (many cities have limited markets, though these are increasing market in the US, Germany and the UK)

Design for Deconstruction

- Design for deconstruction in new buildings is often not considered important
- Existing buildings are not generally designed to be deconstructed

Technical barriers

- Lack of standardisation of components
- Reused steel generally must be recertified by mechanical testing to confirm its grade and this is costly
- Ensuring and warranting the performance of reused components
- Lack of detailed knowledge of the product's properties and in-use history
- Quality assurance of reused products
- Robustness of products in the deconstruction process (e.g. many lighter products do not survive the deconstruction process intact)
- Practicalities of economic deconstruction including deconstructing composite components
- Some new materials are subsidised, creating unfair competition with reused materials
- Increased use of non-reversible technology, systems, construction, chemical bonds, plastic sealants etc
- There are significant volumes of materials still being sent to landfill due to the lack of technology or equipment to sufficiently clean materials.
- Asbestos contamination is a well-documented problem
- New construction systems make recovery more difficult and less financially rewarding

Logistical and Transportation barriers

- Assured availability of supply
- Demolition programs are too short to enable contractors to deconstruct buildings
- Lack of sufficient storage space for recovered products
- Deconstruction as opposed to demolition has significant impacts on the health and safety

precautions required

Legislation and codification barriers

- Construction and demolition waste minimisation is not a priority for some councils and governments
- Inconsistent units of measurement in local waste data
- Waste management is a local council responsibility
- Lack of standard specifications for recycled products

Economic barriers

- The high cost of transport and storage of recycled components and materials
- Cost of storage, cataloguing, refurbished products, etc.
- Cost of testing to verify and guarantee properties
- Finding the appropriate section sizes and lengths can be difficult and expensive
- Additional cost of deconstruction over faster demolition

Liability barriers

- How to manage and apportion risk and liability associated with deconstruction and reuse
- Current standard specifications imply new materials should be used
- -The limit and lack of a grading system for reuse components
- Liability in certification of reused components or materials is not clear

Construction and Demolition Industry barriers

- Lack of communication and networking in the construction and demolition industry with waste minimisation organisations
- There is no formal umbrella group to distribute information
- There are significant volumes of materials still being sent to landfill due the inability to identify markets for the material as it is presented.
- Demolition is generally a low profit margin industry compared with construction

Source: Storey et al. (2005); Sattary & Thorpe (2011); Steel Construction Information (2014); UK Indemand (2014).

The Institute of Public Works Engineering Australasia have developed a specifications course designed to assist project managers and engineers responsible for public works to understand the specifications for materials such as recycled aggregates and other substitute materials, and to learn how to incorporate them into projects (Edge Environment Pty Ltd 2012). As the range of recyclable and reusable products and materials increases, there will be a greater need for such courses to provide awareness of materials and, more importantly, knowledge of how to use them successfully in projects.

4.7 Summary

This chapter has reviewed the significance of embodied energy and relevant carbon emissions in the construction process, and identified the optimum methods for their measurement. Discussion also centred on how construction carbon emissions may be minimised. This sets the context for the next chapter which takes as its focus Bioclimatic Design Principles and their application to the six case studies within this research.

CHAPTER FIVE BIOCLIMATIC DESIGN PRINCIPLES, GREEN BUILDING RATING TOOLS AND THE RESEARCH MODEL

5.1 Overview

Bioclimatic design principles (BDP) have already been introduced in Section 2.5 of Chapter Two. The purpose of this chapter is to provide more detail of the BDP criteria and their basic application to the six case studies in this research. There is also consideration of how BDPs are integrated into a range of green building rating systems. As will be seen, voluntary application of measures to reduce the carbon emissions of construction by the various stakeholders is patchy at best. Given this, it may be that legislation compelling the use of BDPs and similar measures through the building life cycle may be necessary.

This chapter is divided into nine sections. Section 5.1 provides an overview to the chapter. Section 5.2 discusses how BDPs can be applied in building design. Section 5.3 identifies how carbon emissions can be reduced through use of BDPs as exemplified in respect to aspects of the six case studies considered in this research. Section 5.4 considers bioclimatic design principles as applied in current best practice, and their current positioning with the LEED, BREEAM and Green Star green building rating systems. Section 5.5 identifies measurable criteria derived from BDPs that can be used to quantify the degree of carbon emission reduction that may be achieved through use of BDPs. Section 5.6 considers the carbon emissions achieved through use of BDPs in other research and under laboratory conditions. Section 5.7 discusses the limitations of green tool rating systems. Section 5.8 considers the role of Building Information Modelling (BIM) and how green tool rating systems may be integrated into its use. The final Section 5.9 provides a summary of this chapter's content.

5.2 Using bioclimatic design principles in building design

The term 'bioclimatic' refers to a process where savings in energy are achieved through the use of bioclimatic design principles (BDP) in building. As the energy efficiency of buildings increases, the relative contribution of embodied energy to total energy consumption becomes increasingly important, as does its reduction through bioclimatic design principles or other method. Energy saving (carbon emissions reduction) may be achieved through attention to BDPs during design. Appropriate bioclimatic design can reduce energy consumption in a building by five to six (Jones 2003). Other benefits of such energy reduction include improved health and productivity of workers, and reduction in costs of building (Birkeland 2002).

The Energy Design Partnership (EDP) company (2012) proposed use of bioclimatic design principles to improve and regulate environmental conditions in a building. As well as their use during the construction of the building, bioclimatic design principles are also taken into account during the design phase of the building in order to optimise control or use of the sun, the prevailing winds, and the ambient temperature and humidity. The Energy Design Partnership believes that exploitation of solar energy can be achieved in several ways – including through appropriate design of the building envelope (to maximise absorption of solar energy during winter, and minimise it during summer); through suitable orientation of spaces and openings in the building (a southern orientation is considered as the most appropriate); through the optimum sizing of the openings; through use of a layout of the interior spaces of the building based on thermal requirements; and finally by the adoption of passive applications that can collect sunlight and thus be considered as a 'natural' heating system (EDP 2012).

As seen in the Energy Designs Partnership example above, appropriate bioclimatic design can achieve thermal protection of a building by the suitable placement of openings to prevent the escape of heat; by use of appropriate insulation of the building envelope; and by strategic arrangement of internal spaces. Additionally, the provision of shading has as its goal the protection of the building from overheating during summer with strategically placed internal or external, vertical or horizontal blinds. Such systems and passive cooling techniques are a method of bioclimatic design that aims to control a building's microclimate. Another technique emerging from bioclimatic design principles is the careful use of natural lighting in a direct or indirect way to optimise conditions of comfort within the building for the sake of its occupants.

In the final analysis, the crucial principle of bioclimatic design is to achieve the least possible energy consumption concurrently with provision of optimum thermal and visual comfort for the users of a building (EDP 2012). The 'resources' of bioclimatic design may be considered as the natural flows of energy in and around a building – created through the interplay of the sun, wind, precipitation, vegetation, temperature and humidity in the air and in the ground (Architecture 2015).

This present research is focused on construction carbon emissions reduction. This can be achieved through use of bioclimatic design principles to identify measurable criteria that have potential to reduce carbon emissions generated by building construction. There are two main aims in bioclimatic construction – first, to ensure that the constructed building is able to function satisfactorily within current and future climatic conditions; and, second, that the environmental impact of existing buildings is reduced through reduction in their energy use and greenhouse gas emissions (Clarke & Pullen 2008).

The following is a summary of the bioclimatic design principles that have been used in the model proposed in this present research. They focus on reduced and smarter use of sustainable materials to minimise carbon equivalent emissions.

- Minimise energy consumption in mining, processing, equipment use, preassembly and assembly in manufacturing. Criteria measured are reduced energy in mining, processing, and construction materials.
- Minimise transportation at all stages of the building process. Criteria measured are reduced energy as a result of preassembly and reduced materials transportation.
- Minimise use of resources, achieving waste reduction by facilitating reuse and recycling. Criteria measured are reduced energy by recycling and reusing of building materials and building elements.
- Maximise use of renewable energy. Criteria measured are replaced and saved energy in mining and construction (preassembly, professional worker transportation, site processing, materials transportation).

5.3 Reduction of carbon emissions by application of bioclimatic design principles to the six case studies

The following guidelines have been identified through analysis of bioclimatic design principles to measure the potential carbon emissions that can be reduced in the preconstruction and construction stages of building (lifecycle stages 1 to 3). The criteria focus on three main areas that can measure potential carbon reduction: first, carbon emission from energy consumed in *extraction and production* of building materials and elements; second, in *implementation*; and finally, in *transportation*. At this stage, the research model and the calculations have been applied only to the major building elements (floor, wall and roof) of Australian construction systems; and only consider stages one, two and three of the building lifecycle (Table 5.1): extraction, production, and construction.

Table 5.1: Building lifecycle stages

Stage one	Stage two	Stage three	Stage four	Stage five
Extraction	Production	Construction	Operation	Demolition
Source: Author				

Source: Author

Measurable indicators from bioclimatic design principles that can be used to decrease the embodied energy and the associated carbon emissions of building construction – from mining and processing of natural resources to manufacturing, transport and product delivery – are delineated in Table 5.2 below, and also in Tables A.B.1 and A.B.2 in Appendix B.

The following methods and techniques based on bioclimatic design principles can reduce construction carbon emissions. They are available, but are not being consistently and properly used and applied in existing construction practices. This research proposes that if these practices were adopted, this would result in substantial reduction of construction carbon emissions. These reductions could be achieved through consideration of the bioclimatic criteria in Table 5.2; by legislation granting credits for use of environmental assessment tools (LEED, BREEAM, Green Star) to enable reuse of structural elements; by expanding and creating a warehouse of parts and reuse markets; and by expanding deconstruction techniques, machinery and facilities (Bales 2008; Steel Construction Information 2014).

Stage of	Stage 1 and 2	Stage 3 Construction		
construction process	Pre-Construction			
Measurable carbon emissions (embodied energy) that can be reduced in extraction and production of Building Materials	Saved and reduced embodied energy (relevant carbon emissions) by using recycled, reprocessed, reassembled components, materials and elements	 Saved and reduced carbon emissions (embodied energy) by: Reusing buildings, spaces and building elements Using re-treated, repaired and recycled materials Using materials with recycled content 		
Measurable carbon emissions that can be reduced in Implementation	- Reduced carbon emissions in production processes	 Saved and reduced carbon emissions in construction processes: Replaced materials to reduce carbon emissions Replaced renewable energy in construction processes Reduced carbon emissions by reducing materials use 		
Measurable carbon emissions (embodied energy) that can be reduced in Transportation Replaced renewable energy and reduced energy in transportation		construction processes by:Reusing and recycling materialsRegionalizing and localizing suppliers		

Table 5.2: Measurable indicators - potential carbon emissions reduction in construction processes

Source: Author

The following paragraphs discuss the application of these techniques to the six case studies considered in this research. Table 5.3 presents results in three columns in respect to the case studies – the possible reduced carbon emissions achieved through use of BDPs; the standard/Basic (expected) carbon emissions without application of BDPs; and the percentage reduction achieved through use of BDPs. These are referenced in Table 5.3. by letters (a) to (o), and build on examples discussed in the previous chapter. Detailed calculations for these results (a to o) are presented in Appendix A.

(a) Potential emission reduction by use of steel from average recycled content

Carbon emission for steel from primary resources is 3.33kg CO₂/kg (Lawson 1996), but that of steel from average recycled content is 1.96 kg CO₂/kg (Greenspec 2015). Steel from average recycled content: Steel mesh +Edge beams from average recycled

content = $5.148 \text{ Kg/m}^2 \text{ x}$ (embodied energy of steel from primary resources 34 MJ/Kg) (Lawson 1996, p. 13) – (embodied energy of the steel from average recycled content 20.10 MJ/Kg) (GreenSpec 2015) = 71.55MJ/m^2 . By using steel from recycled content in the mesh of the concrete slab of Case Study 5 (London Olympics buildings), the basic carbon emissions of $17.14 \text{ kg } \text{CO}_2/\text{m}^2$ can be reduced to 10.09 kg CO_2/m^2 , representing a 58.8 per cent reduction in generated carbon emission from just the concrete ground slab (see Table 5.3).

(b) Potential emission reduction by use of recycled materials in brick production

Research demonstrates a potential 40 per cent energy saving in brick manufacturing by using 67 per cent recycled container glass brick grog (BDA 2014; Tyrell and Goode 2014). If this technique was applied in Case Study 2 (ACF Green Home – a timber framed brick veneer wall system), there would be a potential 40 per cent energy savings in brick manufacturing. The relevant calculations show that the released carbon emissions could be reduced from 36.04 kg to 21.63 kg, a potential 40 per cent reduction (see Table 5.3).

(c) Potential emission reduction by use of fly ash brick

Fly ash brick gains strength and durability from the chemical reaction of fly ash with water. However, 85 per cent less energy is used in fly ash production than in fired clay brick (Volz & Stovner 2010; Structure Magazine 2014). For example, the carbon emission for a one square metre clay brick veneer wall system is 36.06 kg CO_2/m^2 (Case Study 3). Carbon emissions could be reduced to 6 kg CO_2/m^2 by using fly ash brick. This represents a potential 85 per cent reduction in released carbon emissions in brick manufacturing by using fly ash brick (see Table 5.3). Reduced energy 368 MJ/m² x 85% = 312.8 MJ/m².

(d) Potential emission reduction by use of recycled concrete aggregates

If a concrete mix uses from 30 to 80 per cent of coarse recycled aggregate, mechanical properties of the concrete are unaffected (Uche 2008; Kwan, et al. 2012; PCA 2014). In this case, the embodied energy of the aggregate is 0.083 MJ/Kg (GreenSpec 2015). If this technique was applied in Case Study 2 (ACF Green Home – a 110 mm Concrete slab on ground Floor), the following could be achieved. The released carbon emissions could be reduced from 47.13 Kg CO_2/m^2 to between 45.84

and 43.68 Kg CO_2/m^2 , a potential reduction of 2.73 to 7.32 per cent (1.29 - 3.45 Kg CO_2/m^2) in released carbon emissions from a 110-mm concrete ground floor slab (see Table 5.3).

(e) Emission reduction by using unwanted gas pipelines for structural elements

An example of the reuse of structural steel is that the roof trusses of the London Olympic Stadium were made out of unwanted gas pipelines (Craven 2012; Learning Legacy 2014). In Case Study 5, this use of unwanted gas pipelines in the steel framed, fabric roof of the London Olympic Buildings reduced carbon emissions by 18.02 per cent – usual carbon emissions for this process at 27.63 kg CO_2/m^2 was decreased to 22.65 kg CO_2/m^2 (Steel Construction Information 2014) (Table 5.3).

(f) Potential emission reduction by reuse of brick

Reuse of deconstructed bricks, specifically in non-exposed locations, can achieve an emission reduction of 28.85 kg CO_2/m^2 as demonstrated in Case Study 2, the ACF Green Home. Reuse of brick in the timber-framed clay brick veneer walls reduced carbon emissions by 52.48 per cent – usual carbon emission for this process at 54.97 kg Co_2/m^2 was decreased to 26.12 kg CO_2/m^2 (see Table 5.3).

(g) Potential emission reduction by recycling and reusing concrete roof tiles

Concrete roof tiles can be used towards achieving LEED credits in several new construction or major renovation categories. For example, they can be crushed and recycled, or reused as landscaping fill (LEED 2014). Reuse of concrete roof tiles in the timber frame, concrete tile roof of Case Study 2 demonstrates reduced carbon emissions of 0.65 per cent – usual carbon emission for this process at 23.52 kg CO_2/m^2 was decreased to 21.95 kg CO_2/m^2 (see Table 5.3).

(h) Potential emission reduction by decreasing material use in design

The London Olympics stadium (Case Study 5) weighs only 4,500 tonnes, the lightest Olympic Stadium ever built. This was achieved through design that aimed for reduced materials use. Calculating the reduction of carbon emissions achieved in the London Olympic Stadium is as follows – the basic carbon emissions level of 39.3 Kgs CO_2/m^2 was reduced to 8.02 Kgs CO_2/m^2 . There was thus a 79.6 per cent

reduction in released carbon emissions from the London Olympic stadium (Table 5.3).

(i) Potential emission reduction by replacing Portland cement with E-Crete

According to the International Energy Agency, the manufacture of cement produces about 0.9 kilograms of CO_2 for every kilogram of cement produced. In respect to Portland cement, the CSIRO has found that for every tonne of Portland cement manufactured, one tonne of carbon dioxide is produced. As noted around 5 per cent of global CO_2 emissions result from cement manufacture, making it one of the most polluting activities undertaken by mankind (Zeobond Group 2014).

A new geopolymer cement product called E-Crete forms at room temperature, requires no kiln, and uses fly ash as the main component. Life cycle analysis studies show that E-Crete produces 80–90 per cent less carbon dioxide than traditional Portland cement. Australia is now among the world leaders in research and commercialisation of such cement (Smith et al. 2009).

For example, in Case Study 2, the energy required to construct a one square metre area of a 110-mm concrete slab with Portland cement is 47.13 kg. If this is replaced by E-Crete, the released carbon emissions for one square metre of a 110-mm concrete slab can be reduced to 40.91 kg. If there was full replacement of Portland cement with this geopolymer product in floor construction, there is a potential 47.31 per cent reduction in released carbon emissions (Zeobond Group 2014) (see Table 5.3).

(j) Potential emission reduction by replacing Portland cement with geopolymer

Significant reduction in carbon emissions can be achieved by replacement of Portland cement by geopolymer cements. For example, the carbon emissions from one square metre of a '125 mm elevated concrete floor' of the Velodrome Building for the 2012 London Olympics (Case Study 5) is 48.70 Kgs CO_2 /m^2 – by replacing 40 per cent of Portland Cement with geopolymer, this can be reduced to 39.49 Kgs CO_2/m^2 , representing a potential 18.9 per cent reduction in released carbon emissions (Table 5.3) (calculations are illustrated in Table A.A.6, Appendix A). Alternatively, if Portland cement were fully replaced with geopolymer based cement, the released

carbon emissions for a one square metre a '125 mm elevated concrete floor' (Case Study 5) would reduce from 48.7 Kgs CO_2/m^2 25.66 Kgs CO_2/m^2 , representing a potential 47.31 per cent reduction in released carbon emissions (Table 5.3) (calculations are illustrated in Table A.A.7 in Appendix A).

(k) Potential emission reduction by replacing Portland cement with geopolymer in concrete blocks

The carbon emissions for a one square metre cored concrete block wall (Case Study 4 - Civil Engineering Laboratory building, USQ) is 37.73 Kgs CO₂/m² which can be reduced to 23.28 Kgs CO₂/m², representing a potential 38.29 per cent (14.45 kg) reduction in released construction carbon emissions (see Table 5.3).

I) Potential emission reduction in transportation by rail or water

Sustainability management reports show that 63 per cent (by weight) of construction materials were transported to the London Olympic Park by rail or water (JLL 2012), with consequent reduction in carbon emissions. For instance, consider the reduced carbon emission of transportation by reuse of one square metre of a '200 mm concrete slab floor aggregate' in Case Study 5: The Olympic Velodrome building. The carbon emissions of transportation if required materials were carried by road (truck) would be $13.62 \text{ Kgs } \text{CO}_2/\text{m}^2$. However, when recycled aggregates were used, the carbon emissions were only $1.29 \text{ Kgs } \text{CO}_2/\text{m}^2$. This represents a potential reduction of 90.52 per cent (12.33 Kgs CO_2/m^2) when recycled concrete aggregate is used (detailed calculations are illustrated in Table A.A.12, Appendix A). Similarly, for reuse of one square metre of 'Concrete Block wall's materials' (Case Study 5), there is a potential 90.57 per cent reduction in the released carbon emissions (calculations are illustrated in Table A.A.13, Appendix A) (Table 5.3).

(m) Potential emission reduction in transportation by localizing suppliers

Using locally produced building materials shortens transport distances, thus reducing air pollution produced by vehicles (Structure Magazine 2014). For example, if the construction materials in Case Study Six (Multi Sports Building USQ) were supplied from a local instead of distant supplier, the potential reduction in carbon emission for one square metre of concrete block wall would be 3.91 kgCO₂/m², an 8.6 per cent reduction in the wall-generated carbon emissions (see Table 5.3). Even products

manufactured near the source of their raw materials reduce the transportation energy in the products.

(n) Potential emission reduction in transportation by decreasing material use in design

Reduced materials use in design also decreases the need for transportation, thus reducing carbon emissions. For example, the London Olympics roof (Case Study 5) used a minimum of steel due to its design, thus reducing carbon emissions to 0.37 Kg CO_2/m^2 , an 0.94 per cent reduction in the roof generated carbon emissions (calculations are presented in Table A.A.11, Appendix A) (Table 5.3).

(o) Potential emission reduction by replacing energy in transportation

Construction materials can be carried by different types of transport. The energy efficiency of different means of transport is significant for construction materials (e.g. 4.5 MJtonne/km for road transport, compared to 0.60 MJtonne/km for rail, and 0.25 MJtonne/km for water) (Lawson 1996). For instance, the reduced carbon emissions in transportation (carried by water) gained by reusing one square metre of 200 mm concrete slab floor aggregates (Case Study 5 – Olympics Velodrome Building, London) is 12.33 Kgs CO_2/m^2 compared to carbon emissions generated by truck of 13.62 Kgs CO_2/m^2 , representing a potential 90.52 per cent reduction in released carbon emissions (Table 5.3).

Case Studies (CS	Potential carbon emission reduction	Reduced S kgCO ₂ /m ²	Standard/Basic kgCO ₂ /m ²	Reduction in carbon emissions (%)
Materials production				
CS5 – London Olympic buildings (a)	Steel from average recycled content for the 200-mm concrete slab floor	7.05	17.14	58.8%
CS2 – ACF Green Home (b)	Using recycled materials in brick for the timber-framed brick wall	14.58	36.04	40%
CS3 – Display Project Home (c)	Using fly ash for clay brick veneer wall system	30.06	36.06	85%
CS2 – ACF Green Home (d)	Using recycled concrete aggregates for concrete slab floor	1.29- 3.45	47.13	2.73-7.32%
• •	Using unwanted gas pipelines for structure of the roof	4.98	27.63	18.02%
CS2 – ACF Green Home (f)	Reusing brick for the non- exposed locations in wall	28.85	54.97	52.48%
CS2 – ACF Green Home (g)	Reusing concrete roof tiles	0.15	23.52	0.65%
	Decreasing material use in design for London stadium	28.16	39.3	79.6%
Implementation				
CS2 – ACF Green Home (i)	E-Crete fully replacing Portland cement with geopolymer in 110 mm con. slab	20.30	47.13	47.31%
CC5 – London Olympic buildings (j)	Replacing 40% Portland cement with geopolymer in 125 mm con. slab	9.21	48.70	18.9%
CS5 – London Olympic buildings (j)	Full replacement of Portland cement with geopolymer in 125 mm con. slab	23.04	48.70	47.31%
CS4 – Civil Engineering Laboratory (k)	Use of geopolymer product in cavity concrete block wall	14.45	37.73	38.29%
Transportation				
CS5 – Olympics Velodrome (l)	Aggregate transportation for concrete slab floor	12.33	13.62	90.52%
CS5 –Olympics Velodrome (1)	Using low carbon transport for concrete block wall materials	10	11.04	90.57%
. ,	Localizing suppliers of concrete block wall materials	3.91	45.6	8.6%
CS5 – London	Reducing steel use in the roof by design so reduces transport	0.37	39.3	0.94%
CS5 – London Olympic buildings (o)	Replacing renewable energy in transportation, water instead of truck	12.33	13.62	90.52

 Table 5.3: Summary – Reduced carbon emissions, standard/basic carbon emissions, and percentage reduction in carbon emissions in the six case studies

Source: Table provided by Author. Content summarised from this chapter (a-o) (for detailed information and calculations, see Appendices A and B).

In this section, as exemplified in Table 5.3, bioclimatic design principles have been applied to the construction systems in the six case studies from Australia and the UK. These BDPs include:

- Using recycled aggregates instead of extracting new aggregate from mining
- Using steel from recycled content instead of raw materials
- Using recycled construction materials and elements
- Replacing Portland cement with geopolymer based cement
- Using transportation that generates less carbon emissions (water or rail)
- Reducing transportation by reuse/recycling, and localisation of production

Table 5.4 summarises a number of bioclimatic design principles.

Column one, 'Bioclimatic design parameters', represents the BDPs applied to the case studies referred to in this chapter.

Column two, 'Current conditions, Implemented' are BDPs in current practice identified from the literature review. This column represents summarised data from Table A.D.1 in Appendix D where the numbered references may be found.

Column three, 'Conditions in this research', represent the criteria required to achieve the potential construction carbon emissions referred to in this chapter.

Bioclimatic Design Parameters	Current conditions, Implemented	Conditions in this research
Concrete from recycled aggregates	In Australia, there are a number of manufactured and recycled aggregates readily available in certain localities. ¹	100% recycled aggregate for non-structural purposes; 80 % recycled aggregate for structural purposes ⁶
Concrete block from recycled aggregates	24% recycled content of an aggregate concrete block; ⁸	Aggregate for concrete block fully from recycled aggregate ¹³
Brick from recycled aggregates	Current level of recycled material content in brick is 11%; ^{14,41}	Reuse recycled aggregate for brick, 67% ¹⁹
Steel from average recycled content	Primary typically 10-15% of scrap steel, Secondary 100% scrap based production ^{25, 34}	Steel from fully post-consumer recycled content
Reuse recycled and post-consumer structural and non-structural steel	Scaffolding, formwork, sheet piles, etc., London Olympic Stadium ^{32, 34}	Use 40% recycled and post-consumer steel elements
Reduce material use in steel structural design 10-20%	Some of the current green projects have reduced materials use in design by10-20% ²³	Reduced materials use in structural design 10-20%
Reuse recycled timber and post- consumer FSC timber	FSC works in 80 countries, 24,000 FSC chain of custody certificates are active in 107 countries ^{23,}	60% of all timber products re-used, post- consumer recycled timber; FSC certified timber
Roof tile from recycled tile	In some countries, materials such as concrete roof tiles, are removed separated and recycled ^{44, 45}	50% roof tiles from recycled aggregate ²¹
Thermal insulation from recycled content	Thermal insulation is fully recyclable, i.e. wool content ³¹	Thermal insulation from fully recycled waste ²⁵
Portland cement replaced with geopolymer based cement	Geopolymers have been used in structural, non- structural applications e.g. University GCI Qld, Wellcamp Airport Qld ^{46, 47, 48}	Geopolymer based cement fully replaces Portland cement, arranged for non-structural, structural
Reduce transportation by reusing and recycled materials	National Waste Policy Australia advise to reduce waste, re-use to reduce environmental impacts ³⁵	Reuse has been considered in material production and building elements as well
Transportation by water or rail not truck, Reduce transportation by localizing material supply.	15% of bricks are transported to the distributor's yard or jobsite by rail and 85% by truck ^{19, 30}	Localizing has been considered in detail

Table 5.4: Bioclimatic conditions – current and from this research

Source: This Table and data provided by author. References and detailed information for this table is presented in Appendix D, Table A.D.1.

5.4 Bioclimatic design principles in best practice and green tools

This section discusses the positioning and usage of BDPs in respect to current best construction practice, and then as they are currently positioned within the LEED, BREEAM, and Green Star green building tools.

5.4.1 Current best practice in use of bioclimatic design principles

The following comments are made in reference to the BDP parameters in Tables 5.4, 5.5 and 5.6. Construction materials have a limited life cycle before they become waste. Their reuse in the form of concrete from recycled aggregate extends the lifespan of the product. The construction industry realises the need to use available aggregate rather than searching for the perfect aggregate to make an ideal concrete suitable for all concrete applications. The importance of recycling aggregate has been recognised by the construction industry. Indeed, to date, hundreds of tons of aggregate concrete have been recycled and used for road-base and pavement. However, the use of recycled aggregate in concrete has become even more common practice in recent times.

In reference to 'concrete from recycled aggregate', in Australia, the Commonwealth Scientific and Industrial Research Organisation (CSIRO) initiated one of the most significant steps in promoting the use of recycled aggregate in new concrete through publication of *Guidance on the preparation of non-structural concrete made from recycled concrete aggregate* and *Guide to the use of recycled concrete and masonry materials* were issued in 1998 and 2002 respectively. These guidelines recommend two classes of recycled aggregate (Class 1 and Class 2) for non-structural concrete applications. Despite the CSIRO guidelines, there is an urgent need to establish technical and performance standards for recycled aggregate for new concrete production (Tam 2009).

A number of manufactured and recycled aggregates are readily available on the Sydney and Melbourne market. In other construction applications such as pavement, road base and sub-base, there is limited information on the performance of each material, as assessment appears to be based on field trials, especially those by road authorities. Clean waste recycled concrete aggregate is being used at least 95 per cent by weight in Australia (CCAA 2012a).

In reference to 'concrete block from recycled aggregate': based on a report from Concrete Block Association (CBA), the current average recycled content of an aggregate concrete blocks is only 24 per cent (CBA 2013).

In reference to 'brick from recycled aggregates': recycled and secondary sources are increasingly important in the manufacture of clay bricks – the current level of recycled material content in brick is 11 per cent (Brick Industry Association [Virginia] 2009). Brick is made from abundant natural resources (clay and shale), and is readily recycled for use in the manufacturing process or other uses. Brick manufacturers address sustainability by locating plants in close proximity to mines; and by incorporating waste products and recycled materials into the brick (BDA 2009).

In reference to 'steel from average recycled content': steel is produced by one of two production routes – the primary or basic oxygen steelmaking route which is based primarily on the reduction of iron ore and incorporates typically 10 to 15 per cent of scrap steel; and the secondary or electric arc furnace route which is 100 per cent scrap based production (Steel Construction Information 2014).

In reference to 'reuse recycled and post-consumer steel in structural and nonstructural' applications: steel structures and steel construction products are reusable. This potential is illustrated by the large number of temporary work systems that use steel components, including scaffolding, formwork, sheet piles, etc. Provided that attention is paid to eventual deconstruction at the design stage, there is no reason why nearly all of the steel building stock should not be regarded as a vast warehouse of parts for future use in new applications (Steel Construction Information 2014).

In reference to 'reduce material use in steel structural design': at present the reuse of building materials and products to reduce demand for virgin materials can be achieved, but there is no defined measure (US Green Building Council 2005).

In reference to 'reuse recycled timber and post-consumer Forest Stewardship Council (FSC) timber': in 2012, around 165 million hectares were certified to FSC's

Principles and Criteria in 80 countries, and around 24,000 FSC Chain of Custody certificates were active in 107 countries (Potts et al. 2014).

In reference to 'roof tiles from recycled tiles': in some countries, there have been recycling rates of 65 to 80 per cent. Construction materials such as concrete roof tiles and timber are recommended to be removed separately as much as possible and sorted at the source to facilitate recycling (Tam, Gao & Tam 2005)

In reference to 'thermal insulation from recycled content': thermal insulation is recyclable, and some manufacturers recover and recycle this product. For example, some thermal insulation such as mineral wool content can be fully recycled (Ecospecifier 2016).

In reference to 'Portland cement replaced with geopolymer based cement': carbon emissions are expected to increase by 100 per cent from the current level in the next few years. Geopolymer cements are available in some areas, and have been used for structural and non-structural purposes. In Australia, geopolymer cement was used in construction of the University of Queensland's Global Change Institute (GCI) (Geopolymer Institute 2014); and also in construction of Toowoomba's Wellcamp Airport (Welcamp 2014).

In reference to 'reduce transportation by reusing and recycling materials' and, 'transportation by water or rail not truck ... localizing': the National Waste Policy advises that the generation of waste should be avoided, but when produced, waste treatment, disposal, recovery and reuse must be undertaken in a safe and environmentally-sound manner (Department of the Environment and Energy 2012).

5.4.2 Bioclimatic design principles and the LEED green building tool

The Leadership in Energy and Environmental Design (LEED) for New Construction is a green building certification program/tool established by the US Green Building Council (USGBC) in 1993. This rating tool recognises best-in-class building strategies and practices. It is claimed that LEED rates not only the materials used in construction of buildings, but also the effect those materials have on energy consumption, human health and the environment (USGBC 2016). To achieve LEED certification, building projects must satisfy prerequisites and earn points to obtain different levels of certification. There are four levels of LEED certification: 26–32 points for certification, 33–38 points for silver status, 39–51 points for gold status, and 52–69 points for platinum status (Azhar et al. 2011).

The calculation of recycled content begins in LEED-NC by determining the recycled content value of each building material. This is the sum of the percentage of post-consumer recycled content by weight plus one-half of the percentage of pre-consumer recycled content by weight multiplied by the total cost of the material (BDA 2009). Some of the credits that LEED grants for reusing and recycling is given in Table 5.5.

 Table 5.5: LEED credits for reuse, waste management, recycled content and use of regional materials in construction

Credit	Materials and resources	Points
Credit 1.1	Building Reuse, Maintain 55%, 75%, 95% of Existing Walls, Floors, and Roof	up to 3
Credit 2	Construction Waste Management, Divert 50% or 75%	up to 2
Credit 4	Recycled Content, 10% (1) or 20% (2) (post-consumer plus ¹ / ₂ pre-consumer)	up to 2
Credit 5	Regional Materials, 10% or 20%	up to 2

Source: Project checklist - LEED - New construction (NC) v3 (Concrete Thinking 2014)

For example, in regard to reuse of recycled aggregate in concrete, the National Ready Mixed Concrete Association (NRMCA) provides specific guidelines as to use of returned leftover concrete. Its recommendations include the use of leftover concrete aggregate 'as received all-in' (coarse + fine) in non-structural applications up to 30 per cent by total weight of aggregate. This recommendation presumes that there is some sorting of the leftover concrete to use only leftover concrete 20 MPa and above. Up to 100 per cent replacement of coarse aggregate is allowed only for non-structural applications (Chisholm 2011). For structural applications, the American Society for Testing Materials (ASTM) generally allows up to 10 per cent by total weight of aggregate (equivalent to 20 to 25 per cent by weight of coarse aggregate); and 100 per cent recycled coarse aggregate replacement for concrete strengths up to 20 MPa (Chisholm 2011).

LEED grants a range of credits for local building reuse, construction waste management, resource reuse, use of recycled content, and regional materials. The use

of recycled aggregate in concrete block is awarded up to two points; and in brick production up to 4.5 points (BDA 2009; Obla, Kim & Lobo 2010). LEED also grants up to one point for use of FSC certified wood (Forest Stewardship Council 2010).

Detail of credits granted in LEED is presented in Table A.B.3 in Appendix B. In respect to use of bioclimatic design principles, LEED credits awarded are summarised in Tables 5.6 and 5.7.

5.4.3 Bioclimatic design principles and the BREEAM green building tool

BREEAM – the Building Research Establishment Environmental Assessment Method – was first published in 1990 by the Building Research Establishment (BRE) in the United Kingdom. It is claimed to the world's most established and widely used environmental assessment method for buildings, with over 116,000 buildings certified, and over 714,000 buildings registered. Recent studies have shown that BREEAM has helped reduce CO_2 output by over 4.5 million tonnes since its inception (Aubree 2009).

BREEAM covers a range of building types including offices, homes, industrial units, retail units, and schools. Other building types can be assessed using the Bespoke BREEAM (a custom-made option). When a building is assessed, points are awarded for each criterion, and the points are added to a total score. The overall building performance is awarded a rating of Pass, Good, Very Good, Excellent and Outstanding based on the score (Fowler & Rauch 2006). BREEAM International schemes also use a star rating system of 1 to 5 corresponding to the above rating categories (Aubree 2009). Buildings already certified or under assessment are located in twelve countries in Europe, as well as in the US, Algeria, Dubai, Mauritius, Philippines, Qatar, Lebanon, Morocco and Malaysia (Aubree 2009).

BREEAM contains a range of items that aim to reduce construction carbon emissions through use of bioclimatic design principles. Highlights are as follows. In respect to reusing 'recycled aggregate': where there is a maximum permitted level of 50 per cent recycled aggregate, one point is awarded when the percentage of recycled aggregate used is greater than or equal to 35 per cent. Where there is no maximum

regulatory level, the 50 per cent requirement must be achieved in order to gain this credit (BREEAM 2014a). In respect to 'concrete block from recycled aggregate': one point is awarded where at least 25 per cent of the aggregate used consists of secondary and/or recycled aggregate (Chisholm 2011). In respect to 'Portland cement replaced with geopolymer based cement': one point is awarded where cement and aggregate used is responsibly sourced (BREEAM 2014a).

In respect to 'steel from average recycled content': in the UK, almost 90 per cent of these steel products are recycled through an electric furnace process. In this process, producers of structural steel are able to achieve up to 97.5 per cent recycled content for beams and plates, 65 per cent for reinforcing bars, and 66 per cent for steel deck (Kang & Kren 2007).

In respect to 'reuse recycled timber and post-consumer FSC timber': up to three points are awarded where materials being assessed (including timber) are part of a pre-or post-consumer waste stream (Chisholm 2011).

In respect to 'thermal insulation from recycled content': one point is awarded where at least 80 per cent of the thermal insulation used in the assessed building elements is responsibly sourced (BREEAM 2014).

In respect to 'reduce transportation by reusing and recycling materials': one credit is awarded where at least 25 per cent of the aggregate used is obtained from a waste processing site within a 30km radius of the site (Chisholm 2011).

A summary of the credits that BREEAM grants for achieving a reduction in construction carbon emissions in the rating process is presented in Tables 5.6 and 5.7, and in Appendix D in Tables A.D.1 and A.D.2.

5.4.4 Bioclimatic design principles and the Green Star green building tool

The Green Star tool is an internationally recognised sustainability rating system launched by the Green Building Council of Australia (GBCA) in 2003. Green Star covers from individual buildings to entire communities, and is transforming the way the built environment is designed, constructed and operated in Australia. The Green Star tool is Australia's only national, voluntary rating system for buildings and communities (GBCA 2016).

The Green Star rating system is based on the US LEED system. It represents a comprehensive approach for evaluating the environmental performance of Australian buildings based on a number of categories (Iyer-Raniga & Wasiluk 2007). The Green Star rating scale provides a tool for rating buildings and fit outs, and scores are based on how the building achieves best practice or above sustainability outcomes. Buildings assessed using the Green Star tool can achieve a rating from 1 to 6 Green Stars – with stars rating respectively as Minimum Practice, Average Practice, Good Practice, Best Practice, Australian Excellence, and World Leadership (GBCA 2016; 2017).

Bioclimatic design principles to reduce construction carbon emissions are considered in the Green Star tool, and the following commentary relates to the associated credits. In reference to reusing 'recycled aggregate': Green Star grants one point when 20 per cent of all aggregate used for structural purposes is recycled aggregate class one (i.e. with a maximum specified strength limit of 40 MPa), and no natural aggregates are used in non-structural items (GBCA 2008).

In reference to 'steel from average recycled content': Green Star recognises the reduction in carbon emissions and resource depletion associated with use of recycled steel (GBCA 2008). In reference to 'reuse recycled and post-consumer steel in structural and non-structural' elements': Green Star grants up to 2 points where 90 per cent of all steel by mass either has post-consumer recycled content greater than 50 per cent, or is reused (GBCA 2008). In reference to 'reduce material use in steel structure': Green Star grants one point where 20 per cent less steel has been used than in conventional steel framing, without changing the load path to other structural components (GBCA 2008).

In reference to 'reuse recycled timber and post-consumer FSC timber': Green Star grants up to 2 points where 95 per cent of all timber products used in building and construction works have been sourced from any combination of the following: reused

timber, post-consumer recycled timber, or Forest Stewardship Council (FSC) Certified Timber (GBCA 2008).

In reference to 'roof tiles from recycled tile or recycled content': Green Star grants one point where at least 2 per cent of the project's total value is represented by reused products or materials. Additionally, one point is given for concrete where no natural aggregate has been used for non-structural purposes, for example in roof tiles (GCBA 2008). In reference to 'Portland cement replaced with geopolymer': Green Star awards two points where Portland cement content is reduced by 40 per cent in concrete block production (CCAA 2012b). Green Star also awards up to two points where a project has reduced use of Portland cement (GBCA 2008).

In reference to 'reduce transportation by reusing and recycling materials': Green Star credits reusing and recycling of up to 40 per cent of materials, but only advises localising, and using water and rail instead of road (GBCA 2008).

A summary of Green Star credits for achieving carbon emissions reduction in the rating process is presented in Tables 5.6 and 5.7, and detailed information is provided in Appendix D, Tables A.D.1 and A.D.2.

Bioclimatic conditions, Parameters	Australian Tool Green Star (GBCA)	US Green Tool LEED	UK Green Tool BREEAM
Concrete from recycled aggregates	Green Star, one point, 20% of aggregate for structural purpose; no natural aggregate used in non-structural purposes ²	LEED, recycled content, 10-20% of aggregate up to 3 points; ^{2, 24} ; 20-30% of aggregate for structural 100% non-structural purposes, US ^{18,36}	BREEAM, 25-50% RA; no restriction in 16 MPa and 40 MPa; 20% Designated concrete 20-40 MPa ^{2, 36}
Concrete block from recycled aggregate	Green Star, 40% RA; no natural aggregates in non-structural ^{23,33}	ASTM, structural 20-25% coarse aggregate; 100% up to 20 MPa $^{18,\;36}$	BREEAM, no restriction in 16 MPa and 40 for Concrete block ³⁶
Brick from recycled aggregates	Green Star, no direct credit, Mat-3, 80% reused material ^{2,9, 16}	LEED, recycled content in brick 10-20%, MR 4, 2 points, 2 $\frac{1}{2}$ points ¹⁴	BREEAM; all waste reused; recycled content is 11% ¹⁴
Steel from average recycled content	Green Star, Mat-6; maximum 60% post- consumer recycled content ²³	LEED, 65-97.5% post-consumer recycled content ^{23, 16}	BREEAM, Mat-6;60% recycled content ³⁸ ;97.5% beams, plates; 65% bars; 66% steel deck ¹⁶
Reuse recycled and post- consumer steel in structural & non-structural	95% of the joinery; 50% of the structural framing, roofing, designed to be disassembled ⁵	LEED, 1-2 points to 75-100% reuse of existing walls, floors and roof $^{\rm 24,3}$	BREEAM, Mat-6; maximum 60% recycled content ²³
Reduce material use in steel structural design	Green Star, Mat-6, grade reduced materials in design,10-20%, ²³ Mat-10, one point for 20% reduction	LEED, eliminating the need for materials in the planning and design phases ^{10, 7}	BREEAM, grade reduced materials in design ²¹ avoiding over-design, material reuse ³⁹
Reuse recycled timber and post-consumer FSC timber	Green Star 95% of all timber products re- used, post-consumer; FSC certified timber 22, 23	LEED, timber products re-used, post-consumer; 50% FSC certified timber, up to 1 point ^{32, 29, 24}	BREEAM; up to three points where timber is part of a pre-or post-consumer waste stream ³⁶
Roof tiles from recycled tiles	Green Star, Mat-5 one point, where no natural aggregates are used in non-structural uses ²³	LEED credits; produced from postconsumer recycled content, from the waste, up to 3.5 points ^{20,21}	BREEAM; M03, roof tiles can be extracted from the waste stream ³⁶
Thermal insulation from recycled content	Green Star, no direct credit, but 80% recycled content advised ^{27,}	LEED, MR4, 20% or more recycled thermal insulation, one point ^{12, 7}	80% thermal insulation must be responsibly sourced 1 point ³⁷
Portland cement replaced with geopolymer based cement	Green Star; Maximum 60% In situ concrete 40% precast and 30% for stressed concrete; 30% for 1 point and 40% for 2 points ^{23, 26}	LEED Concrete consists of at least 30% fly ash; 50% recycled content or reclaimed aggregate; 90% recycled content or reclaimed aggregate ^{23, 12,7}	One point awarded where geopolymer cement used and supply chain process and must be responsibly sourced ⁴⁰
Reduce transportation by reusing and recycling materials	Green tools credit the reusing and recycling up to 40% of materials, not directly credited 2 ^{, 15, 35}	Green tools credit the reusing and recycling up to 40% of materials, not directly credited $2^{,15}$	One credit where obtained from waste processing site(s) within a 30km radius of the site ³⁷
Transportation by water or rail not truck, Reduce transportation by localizing	Green Star advise localizing, using water and rail instead of road ^{2,15}	LEED, Regional Materials, up to 4 points ¹⁴ ; tools advise localizing, using water and rail instead of road ^{2,15}	Regional materials, localizing, using water and rail instead of road ^{2,15}

Table 5.6: Bioclimatic conditions of the research considered in the green tools (Green Star, LEED and BREEAM)

References, specifications and detailed information of this table is presented in Table A.D.2 (Appendix A)

5.5 Measurable criteria based on BDPs to reduce construction carbon emissions

The bioclimatic principles identified in this research are expressed as measurable criteria that can be applied in construction projects to reduce potential construction carbon emissions. The column labelled 'Conditions in this research' in Table 5.7 in this chapter, and in Table A.D.1 in Appendix D, represent the bioclimatic criteria that produce the highest possible carbon emission reductions when appropriately applied.

A research model has been proposed to measure embodied energy in the preconstruction and construction phases of building that takes into account decreased and replaced renewable energy in preconstruction and construction processes; saved energy in transportation by localisation; and reduced energy from reusing and recycling of materials. The detailed model format is illustrated in Appendix B.

The three areas examined in this study with reference to reduction of carbon emissions (CO₂-e) are - energy consumed during extraction/production of construction materials and building elements; energy consumed during implementation; and energy consumed during transportation.

The measurable criteria summarised below and in Tables 5.6 and 5.7 are derived from bioclimatic design principles and have been applied to the construction systems of the six case studies in this research.

Bioclimatic principles applied in this research to the six case studies	Application
Reusing recycled aggregates	This includes replacing concrete with 80 per cent
in materials production	recycled aggregate. and 100 per cent for non-
instead of extracting new	structural purposes (Uche 2008); and brick with 67
aggregate from mining	per cent recycled aggregate (BDA 2014; Tyrell &
	Goode 2014).
Using steel from recycled	This includes the use of steel mesh, edge beams, and
content instead of steel from	steel sheets, aiming towards 100 per cent
raw mining	replacement from recycled content (Greenspec 2015;
	Steel Construction Information 2014).
Reusing recycled	This includes reusing post-consumer recycled timber
construction materials and	or certified timber from the Forest Stewardship
elements	Council (FSC) (Design Coalition 2013; GBCA
	2008,); use of insulation from recycled materials
	(Greenspec 2015); use of concrete tiles from
	recycled roof tiles (LEED 2014); and reuse of
	structural elements (Karven 2012).
Replacing Portland cement	This includes full replacement of Portland cement
with geopolymer based	with cement substitute, 80 per cent for concrete for
cement	structural purposes, and 100 per cent for non-
	structural purposes (McLellan 2011; Nath & Sarker
	2014).
Using types of transportation	This refers to use of ship and rail instead of trucks,
that generate less carbon	i.e. use of sustainable modes of transportation
emissions	(Learning Legacy 2014).
Reducing transportation	This is done by reusing recycled aggregate, recycled
	materials, localizing and similar approaches.

5.6 Bioclimatic principles considered in other research and under laboratory conditions

Following is a summary of the bioclimatic design principles applied in research elsewhere and the laboratory, but which are more stringent than have been considered in this study.

Concrete from recycled aggregate: The CSIRO guide gives contamination limits for various classes of RCA. The binder content for Grade 1 RC concrete with 30 per cent partial replacement with coarse Class 1A RCA is comparable to that required for concrete containing 100 per cent natural aggregate. For Grade 2 RC mixes containing up to 100 per cent coarse Class 1A RCA, extra binder loading may be required to achieve the specified compressive strength (CCAA 2015).

Brick and concrete block from recycled aggregate: Using recycled aggregate as the replacement for natural aggregates of up to 100 percent, concrete paving blocks with a compressive strength of not less than 49 MPa can be produced without the incorporation of fly ash, while paving blocks for footway uses with a lower compressive strength of 30 MPa and masonry bricks can be produced with the incorporation of fly ash (Poon, Kou & Lam 2002).

National Green Building Standard 4RE 604.1: Brickwork can help meet requirements of many certification rating systems in the areas of development density, storm water management, the heat island effect, improved energy performance, building reuse, waste management, materials reuse, recycled content and regional materials (BDA 2009).

Reuse recycled and post-consumer steel from average recycled content in structural and non-structural applications: In the production of structural shapes and bars, 95-100 per cent old steel can be used to make new products. In this process, producers of structural steel are able to achieve high percentages of recycled content (Kang & Kren 2007). Most steel construction material and elements are highly reusable such as for sheet and bearing piles; and structural members, including

hollow sections and light gauge products such as purlins and rails (Steel Construction Information 2014) (Craven 2012; Learning Legacy 2014).

Reduce material use in steel structural design: In practice, the most noteworthy cases using an integrated design process or linear design process have achieved a considerable reduction in material use (Ecospecifier 2016). For example, the London Olympics stadium was constructed using only a tenth of the steel required to build Beijing's 'Bird's Nest' stadium (Craven 2012).

Reuse recycled timber and post-consumer FSC timber: This includes the complete re-use of timber products post-consumer, reusing recycled products, or the use of FSC-certified timber. FSC in Australia surpasses 1 million hectares of certified forests. with Forico, a Tasmanian forestry management company, awarded full FSC certification (FSC 2015).

Roof tiles from recycled tiles: Demolition and debris from land clearing can be recycled and reused. For example, roof tiles are reusable, with concrete roof tiles being less prone to waste. Concrete roof tiles can be crushed and recycled or reused as landscaping fill (LEED 2014).

Thermal insulation from recycled content: Thermal insulation can contain high levels of post-consumer recycled content, being ultra-low to zero in content of volatile organic compound (VOC) products, as well not being associated with health concerns. For example, some thermal insulation such as mineral wool batts contain 100 per cent recycled blast furnace slag (Ecospecifier 2016).

Portland cement replaced with Geopolymer based cement: The outcomes of the current research show that geopolymer based cement which is a relatively new binder can be a sustainable and economical binding material, as it is produced from industrial by-products such as fly ash. Geopolymer cements can replace 100 per cent of the Portland cement in concrete. here is increasing interest in geopolymer based cement due to its low level of carbon emissions compared to Portland cement (Nath & Sarker 2014).

Reduce transportation by reusing and recycling materials, localizing, and use sustainable modes of transport: In the future, construction design must ensure that there is minimum wastage, maximum recycling, and (thus) reduction in transportation.

A summary of the items detailed in this section is given in Table 5.7.

Column one, 'Bioclimatic principles/criteria' are identified from the present research into bioclimatic design principles.

Column 2, 'Current conditions, implemented', are design principles already in current practice (full references are in the legend at the base of Table A.D.3 in Appendix D).

Column 3, 'Conditions with green tools', detail the credits in the LEED, BREEAM, and Green Star rating tools that relate to the bioclimatic criteria being used in this research (i.e. in Column 1).

Column 4, 'Conditions in this research', refers to the bioclimatic criteria as applied in the case studies in this research.

Bioclimatic principles/criteria	Current conditions, Implemented	Conditions with Green tools (Green Star., LEED, BREEAM)	Conditions in this research
Concrete from recycled aggregates	In Australia, there are a number of manufactured and recycled aggregates readily available in certain localities. ¹	G.S. and LEED 1-3 points 20-30% RA for structural purposes; BRE 25- 50 % in 20-40 MPa - no restriction, 100% non-structural ^{2, 18, 36}	Fully RA for non-structural purpose; 100% RA for non-structural; 80 % RA for structural purpose ⁶
Concrete block from recycled aggregates	24% recycled content of an aggregate concrete block ⁸	G.S., BRE, 40%; US 25% RA structural; 100%, or no natural aggregates in non-structural ^{18,23,36}	Aggregate for concrete block fully from recycled aggregate ¹³
Brick from recycled aggregates	Current level of recycled material content in brick is 11% 14 ^{.41}	G.S., 30%; ^{16, 23} ; LEED 20%; BRE 11% ISO, up to 10 points for 10% Recycled aggregate ^{14,16,36}	Reuse recycled aggregate for brick, 67% ¹⁹
Steel from average recycled content	Primary typically 10-15% of scrap steel Secondary 100% scrap based production ^{25,} ³⁴	G.S. Mat-6, 60%; LEED 65-97.5%; BRE, Mat-6, 60%; - 97.5% beams, plates; 65% bars; 66% steel deck post- consumer recycled content ^{23,16,38}	Steel from fully post-consumer recycled contents
Reuse recycled and post- consumer structural and non- structural steel	Scaffolding, formwork, sheet piles, etc., London Olympic Stadium ^{32, 34}	G.S., 95% Joinery, 50% structural framing, roofing; LEED 75-100% existing wall, floor, roof; BRE, Mat-6, 60% recycled content ^{3,5,23,24}	Use 40% recycled and post-consumer steel elements
Reduce material use in steel structural design 10-20%	Some of the current green projects have reduced materials use in design 10-20% ²³	G.S., Mat-6, 10-20% one point; LEED, eliminating need for materials in the design stage; BRE reduced, avoiding over-design ^{23,21,10,7,32}	Reduced materials use in structural design 10-20%
Reuse recycled timber and post-consumer FSC timber	FSC works in 80 countries, 24,000 FSC chair of custody certificates are active in 107 countries. ^{23,}	G.S. 95% re-used, post-consumer; FSC certified timber; up to 3 points; LEED, 50% FSC; BRE, 3 points, post-consumer waste stream ^{22, 23, 32,24,29}	60% of all timber products re-used, post-consumer recycled timber; FSC certified timber
Roof tile from recycled tile	In some countries materials such as concrete roof tiles, removed separated and recycled ^{44, 45}	G.S. Mat-5, 1 point, no natural aggregates are used; LEED, from the waste, up to3.5 points, BRE, M03, from the waste stream ^{20,21,23,36}	50% Roof tile from recycled aggregate
Thermal insulation from recycled content	Thermal insulation is fully recyclable, i.e. wool content ³¹	G.S. 80% advised; LEED MR4 20%, ¹ / ₂ point, BRE 80%, 1 point, responsibly sourced ^{12.7,27,37}	Thermal insulation from fully recycled waste ²⁵
Portland cement replaced with geopolymer based cement	Geopolymers have been used in structural, non-structural, Zeobond group, University GCI in Qld, Wellcamp Airport, Qld ^{46,47,48}	G.S. 60% In situ concrete; 40% precast 30% stressed concrete; LEED, 30% structural; no limit others, BRE, responsibly sourced cement ^{23,26,7}	Geopolymer based cement, fully replaced with Portland cement, arranged for non-structural, structural
Reduce transportation by reusing and recycled materials	National Waste Policy Australia advise to reduce waste, re-use to reduce environmental impacts ³⁵	Green tools credit the reusing and recycling up to 40% of materials, not directly credited; obtained from30km radius of the site ^{2,15,35,37}	Reusing has been considered in material production and building elements
Transportation by water or rail not truck, Reduce transportation by localizing	15% of brick are transported to the distributor's yard or jobsite by rail and 85% by truck ^{19, 30}	LEED, regional materials, up to 2 points; ¹⁴ tools advise localizing, using water and rail instead of road ^{2,15}	Localizing has been considered

Table 5.7: Disalimetia conditions - aurrent: from bast	prostice with groop tools (Croop St	or IEED and DDEEAM); and from this research model
- raple .)./. D IOCHIMALIC CONDITIONS – CUITERL. HOIR DESL	Diactice with green tools (Green St	ar, LEED and BREEAM); and from this research model

Source This Table and data provided by Author. References and detailed information of this table is presented in Table A.D.1 (Appendix D)

5.7 Limitations of green tool rating systems

Following investigation of the bioclimatic conditions within the green tools, it is noted that their focus is on energy use and the environment. All contain numerous requirements and credits intended to reduce building operational energy use. However, what is often lacking in these green rating systems is a means by which to promote and measure the avoidance of negative consequences. For example, only one of these tools (LEED) currently contains methods to measure the avoidance of construction waste. All measure the diversion of waste from landfills, but only the National Association of Home Builders (NAHB) green tool (not considered in this present research) recognises that some materials have little or no on-site waste to begin with. In addition, the efficient use of materials is not properly recognised in the green tools. Materials such as brickwork perform multiple functions and construction can thus avoid the use of other materials, such as paints, sound insulation etc. (BDA 2009). In short, LEED, BREEAM and Green Star can still be further improved.

Another issue is that at this point in time, green building rating tools are simply not being consistently factored into building design. Added to this, even when a construction project is assessed against a green building tool such as LEED, BREEEAM or Green Star, those tools do not, in fact, adequately integrate BDPs into the criteria they rate. This can be seen in reference to Table 5.8 which compares the relative use of green tools in current practice, Green Star, LEED and BREEAM, and in the model proposed in this research. As can been seen from Table 5.8, the integration of bioclimatic design principles is consistently higher in all categories in the research model as compared to current practice and the green building rating systems being considered.

	Research model				
Bioclimatic conditions	Current practice	Green Star	LEED	BREEAM	Codes/Standards
Concrete from recycled aggregates, structural purposes	Poor	20%	30%	40%	80%
Concrete block from recycled aggregate, non-structural	24%	40%	25%	40%	100%
Brick from recycled aggregates	11% UK	-	10-20%	11%	67%
Steel from average recycled content	10-15%	60%	65-97%	65-66%	100%
Reuse recycled and post- consumer non-structural steel	10%<	-	75%	60%	60%
Reuse recycled and post- consumer structural steel	-	-	-	-	40%
Reduce material use in steel design	Poor	10-20%	-	-	10-20%
Reuse recycled timber and post- consumer FSC timber	Poor	95% NS	50%	-	60%
Roof tile from recycled content	Poor	-	20%+	-	50%
Thermal insulation from recycled content	Poor	80%	20%+	80% RS	100%
Portland cement replaced with geopolymer cement, non- structural purposes	Poor	60%	50%	-	100%
Portland cement replaced with geopolymer cement, structural purposes	Poor	40%	30%	-	80%

Table 5.8: Relative use of bioclimatic criteria in current practice, Green Tools and	for this Research
	Research model

Source: Table and data provided by Author (derived from data in Chapter Five)

Poor = Less than 25% availability | Fair = 25-50% availability | Good = 50-75 availability | Excellent = 75-100% availability, | NS = Non-structural | RS = Responsible Sourced

5.8 Building Information Modelling (BIM) and green design

Building Information Modelling (BIM) software provides a three-dimensional digital representation of a building or construction project (Eastman et al. 2011). BIM has applications in the engineering, architecture and construction industries, particularly as it provides a basis for life cycle analysis of a building or construction project, including energy usage analysis at various (conceptual) points of the building life cycle. This analysis of a building's energy consumption at the conceptual design stage allows for decisions to be made about the most suitable design that will provide an energy efficient building. BIM thus allows for greater sustainability and low energy performance to be more easily factored into any construction project (Jalaei & Jrade 2014).

BIM can estimate embodied energy and equivalent carbon emissions data. This information can be used to assess and calculate potential construction carbon emissions reduction in Australian construction systems at all points in the building life cycle (Eastman et al. 2011). BIM plugins for life cycle analysis tools such as Tally and IMPACT are already available (EPD-Tally 2008; IMPACT 2016). There is also work currently being conducted to link BIM and energy analysis tools with green building certification systems. This will allow building designers to identify the most energy efficient construction alternatives, and thus to calculate the potential green tool points they might gain for a given design using LEED, BREEAM, Green Star, or other green rating system (Jalaei & Jrade 2014).

5.9 Summary

This chapter has identified a range of criteria derived from bioclimatic design principles which can be used to reduce the carbon emissions from construction projects. As has been seen, the current use of BDPs and green rating tools in construction projects is inconsistent, and the green tools themselves also fail to integrate BDPs adequately into their rating criteria. Additionally, the bioclimatic design criteria in the research model have been demonstrated to potentially achieve higher levels of carbon emission reduction than in any of the rating tools considered, or even in current best practice. The levels of carbon emission reduction may improve even further as Building Information Modelling with integrated life cycle analysis becomes more widely applied in construction design and building projects.

CHAPTER SIX RESEARCH METHODOLOGY AND RESEARCH DESIGN 6.1 Overview

It is generally accepted that the construction, demolition, reconstruction and restoration of buildings result in intensive energy consumption and generated carbon emissions with considerable environmental impact. It is thus imperative to reduce the energy consumption and carbon emissions of the construction process. There are existing techniques to do this, but these are inconsistently applied and lacking in depth of criteria for application.

There are no recognised benchmarks defining acceptable levels of embodied energy and relevant carbon emissions of the construction process. There is also a lack of knowledge and research with a focus on reducing the carbon emissions of construction through the application of bioclimatic design principles. This present research contributes knowledge to these areas, and proposes a green tool based on consideration of bioclimatic design principles whose application has the potential to reduce the carbon emissions of the construction process. The purpose of this chapter is to discuss the type of research and process used to achieve these aims.

This chapter is divided into seven sections. Section 6.1 provides an overview to this chapter. Section 6.2 discusses the research type and case study method. Section 6.3 considers the procedure (methodology) used to achieve the research aims. Section 6.4 identifies the sources providing the embodied energy and carbon emissions data analysed in this research. Section 6.5 delineates the limitations of this study. Section 6.6 identifies how the results from the study may be generalisable to other construction contexts. Section 6.7 provides a summary of this chapter.

6.2 Research type and the case study method

In any discussion of research methods, there is always debate regarding the scholarly nature, contributions, merits and limitations of quantitative as compared to qualitative research (Gan 2006). This present research is based on quantitative methods that use objective measurements to analyse the numerical data collected in the research. In respect to this, the aim of quantitative research is to gather numerical data and generalise it to explain a particular phenomenon (Giesbrecht 1996).

Quantitative research requires the use of structured and objective data, where the response options have been predetermined. The objective data for this research is gathered from a range of sources relating to the six case studies examined in this research, and to Australian construction systems (detailed in Section 6.3).

Six case studies were selected as a number that provide for a stronger research design, greater validity of the findings, and for more confidence in results that are generalisable to other contexts. In this respect, multiple case studies also allow the researcher to verify that findings are not just the result of the characteristics of the research setting (Gan 2006).

This research investigates the potential construction carbon emissions that can be reduced by application of bioclimatic design principles. The bioclimatic conditions depend on where that building and its construction site is located. Accordingly, the six cases studies were selected from a range of different locations in order to provide different construction contexts for application of the research model, enhancing its validity.

6.3 Research methodology

This study has been conducted through a range of stages. Stage one involved identifying and detailing the embodied energy and carbon emissions inherent within the construction process, and how they might be measured (Chapter Four). Stage two identified specific measurable bioclimatic criteria within bioclimatic design principles that could be applied in the green model/tool developed for this research (Chapter Five).

Stage three involved application of this model to specific elements of the floor, wall and roof construction systems used within the six case studies, and analysis of the potential reductions in carbon emissions that could be achieved (Chapter Seven). Stage four involved application of the model to emissions and embodied energy data available for elements of general floor, wall and roof construction systems in Australia, and analysis of the potential reductions in carbon emissions that could be achieved (Chapters Seven).

6.4 Sources of embodied energy and carbon emission data used in this research

The Australian construction data used in this research has been obtained from Lawson's publications in 1996 and 2006. The analysis and detail of Australian floor, wall and roof construction systems supplied by Lawson (1996), and the embodied energy of building materials data supplied in Lawson (2006), have been applied within the research model, this to demonstrate how construction carbon emissions may have been reduced in the selected Australian case studies.

One international case study was also considered in this research, namely the velodrome building constructed for the London Olympics in 2012. Extensive data from this construction was detailed in various sources (e.g. Rodway 2010; Inventory of Carbon & Energy 2011; Bull 2012; Smith 2012). A sample of the developed model format is illustrated in Appendix B. A summary of the six case studies is provided in Table 6.1.

Other supporting data concerning the embodied energy and carbon emissions of specific elements of the construction process were obtained from a variety of sources. These include the Australian Your Home technical manual (Milne & Reardon 2014); the Building Research Establishment Environmental Assessment Method (BREEAM 2014b); Ecospecifier (2015; 2016); the Environmental Design Guide (EDG 2014); the Green Building Council of Australia (2008; 2014a; 2014b; 2016; 2017); GreenSpec (2015); the Inventory of Carbon and Energy (2011); and the US Green Building Council's Leadership in Energy and Environmental Design (LEED 2015; 2016).

Ecospecifier is a database of independently vetted eco-preferable products and materials including product descriptions. It is not a rating tool. It was developed initially by the Centre for Design at RMIT, and is now managed by Natural Integrated Living. It provides an understanding of the upstream and downstream implications of decisions in an economic, legal and ecological sense. It helps the user to identify eco-preferable products and materials, and to understand associated environmental and health issues that need to be considered in the use of a product (Iyer-Raniga & Wasiluk 2007).

		Construction Systems			
C	ase studies in this research	Floors	Walls	Roofs	
Source: Trip Advisor (2014)	 Friendly Beaches Lodge, 1991; accommodation for guests completing a guided three-day bushwalk Architect: Latona Masterman Freycinet Peninsula, Tasmania, Australia 	Timber frame floor	Single skin timber walls	Timber frame, steel sheet roof	
Source: Environmental Design Guide (EDG 2014)	 2. ACF Green Home, 1992. This display home was constructed for VDPH in accordance with environmental guidelines prepared for the Australian Conservation Foundation (ACF) Architect: Taylor Oppenheim Architects Roxburgh Park, Victoria, Australia 	110 mm Concrete slab on ground floor; Timber- framed upper floor	Timber- framed brick veneer walls	Timber frame, concrete tile roof	
Source: Lawson (1996)	 3. Display Project Home, 1994. This Canberra Display Project House was sponsored by Energy Research Development Corporation (ERDC) to demonstrate the application of energy-saving design measures. Architect: Jen-Vue Homes Ginninderra, Australian Capital Territory 	110 mm Concrete slab floor	Timber- framed brick veneer walls	Timber frame, steel sheet roof	
Source: This author	 4. Civil Engineering Laboratory, USQ, 2013; This is a one-level 350 m² building commissioned by the University of Southern Queensland (USQ) Nairn Construction; Architect: Wilson Architects Springfield Central, 4300, Brisbane, Australia 	200 mm Concrete slab on ground floor	Cored Concrete block walls	Steel frame, steel sheet roof	
Source: London Olympics (2012)	 5. The London Olympic Velodrome Building. The design brief asked for a lightweight construction. All parties in the construction supply chain co-operated to deliver the project to minimise excess material usage. Principal architects: Jonathan Watts, George Oates, Hopkins, Olympic Park London 	Concrete slab floor Concrete upper floor	Cored Concrete block walls; Steel frame timber wall	Steel frame, fabric roof	
Source: This author	 6. Multi Sports Building, USQ, 2013. This two-story 302 m² building was commissioned by USQ which as a multi sports building. Nairn Construction; Architect: Reid Design Springfield Central, 4300, Brisbane, Australia 	Concrete slab floor Concrete upper floor	Cored Concrete block walls	Steel frame, steel sheet roof commercial	

Table 6.1: Case Studies – Construction systems of the main elements (floors, walls and roofs)

The Inventory of Carbon and Energy (2011) is a research database located at the University of Bath in the UK. It provides an inventory of embodied energy and carbon emissions for building materials in the UK. Other specific data was also collected from various suppliers and manufacturers of construction materials in the UK and Australia (e.g. Steel Construction Information 2014).

Some of the original data and information about the case studies was also obtained directly from the designers – for example, data and information about two of the case studies at USQ was obtained directly from their building manager. Finally, the latest findings and data about the currently accepted and used percentages for recycled and reused construction materials was obtained from the World Federation of Engineering Organizations (2011).

6.5 Limitations of this study

As noted in Section 1.4 of Chapter One, this study is limited to stages one to three of the building lifecycle. These stages of the building life cycle are summarised in Figure 6.1.

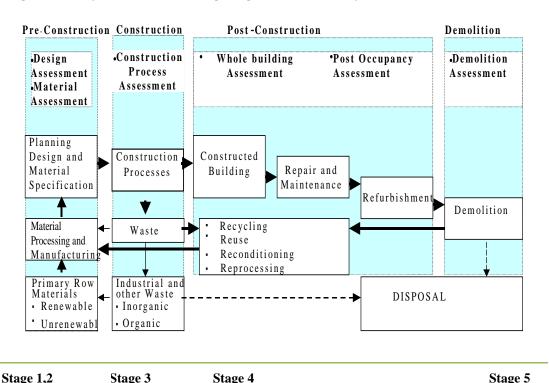




Figure 6.1: Life cycle model of building. Stages 1 to 3 are within this study. Source: Derived from Lawson (1996) and UNEP SBCI (2009)

6.6 Generalising the outcomes from this study

The major outcome from this study is identification of a model to reduce the carbon emissions of construction during the first three stages of the building life cycle. This model has been applied to the six case studies within this research. The findings are considered as generalisable to other Australian construction projects where the model is appropriately applied.

6.7 Summary

This chapter has outlined and justified the research type and methodology used for this study, and identified the sources of the embodied energy and emissions data analysed within the research model. The limitations of this research have also been described. Results from the application of the research tool/model developed for this study are described in Chapters Seven.

CHAPTER SEVEN RESULTS AND ANALYSIS OF APPLYING THE RESEARCH MODEL TO CASE STUDIES AND GENERAL AUSTRALIAN CONSTRUCTION SYSTEMS

7.1 Overview

The purpose of this chapter is to present the results and analysis of this research project. The bioclimatic criteria of the research model are first applied to the floor, wall, roof and then whole construction systems of the six case studies considered in this research. The research model criteria are then applied to elements of general Australian floor, wall and roof construction systems. The carbon reductions achieved, and the associated emissions generated, from application of the research model are then compared with results obtained from similar standard building system elements, implementation (completion) of building projects, and application of the Green Star rating tool. Results are presented in four ways for each construction system studied – as tables of numerical data for the reductions in emissions achieved, and the carbon emissions generated; the emissions generated are then displayed in a comparative bar graph; the final table available for each construction system considered presents the carbon emission reductions achieved as comparative percentages for each type of building element. An overall analysis of each section's results is also presented.

The chapter is divided into seven sections. Section 7.1 provides the background to this chapter. Section 7.2 details the six case studies selected for this research. Section 7.3 presents the data and analysis of results obtained following application of the research model to elements of floor, wall and roof construction systems in the case studies. Section 7.4 presents the data and analysis of results obtained following application of the roof systems. Section 5 summarises the content of this chapter.

7.2 Selected case studies

The model developed reviews six case studies, five from Australia and one from the United Kingdom. The Australian case studies use the general construction systems in Australia as identified by Lawson (1996). These can include any project from any classification (residential, public, and commercial). For example, the first three case studies are taken from a paper written by Lawson (1996) – all detail and information for these are provided, together with embodied energy and implemented embodied energy (Lawson 1996). The fourth and sixth case studies focus on buildings recently completed on the Springfield campus of the University of Southern Queensland (USQ). All drawings and detailed information were accessible. The Olympic Velodrome Building from the London Olympics in 2012 is the focus of the fifth case study – these Olympics achieved high sustainability levels from a range of different environmental tools (e.g. CEEQUAL, ISCA, and BREEAM). In case study five, the data was obtained from four main sources – Rodway (2010); Inventory of Carbon & Energy (2011); Bull (2012); and Smith (2012).

Table 7.1 presents the results from application of the bioclimatic criteria within the research model to the six case studies that could potentially result in significant carbon emissions reduction.

This section details information about the floor, wall and roof construction systems used in the six case studies. Tabulated data of their embodied energies and carbon emissions are presented in the following sections, with detailed calculations presented in Appendix C.

Bioclimatic criteria	1. Friendly Beaches Lodge, 1991	2. ACF Green Home, 1992	3. Display Project Home, 1994	4. Civil Engineering Laboratory, USQ 2013	5. Olympic Velodrome Building, London 2012	-
Concrete from recycled aggregates	80 % RA for fixing posts in the ground 1 ^{, 6} ,	80 % RA for concrete slab on ground $^{1,\ 6,}$	80 % RA for concrete slab on ground ^{1, 6,}	80 % RA for concrete slab on ground, structural ^{1, 6,}	80 % RA for concrete slab on ground, structural ^{1, 6,} 100% RA for non-structural	80 % RA for concrete slab on ground, structural ^{1, 6,}
Concrete block from recycled aggregate	N/A	N/A	N/A	Concrete block wall from full RA ¹³	Concrete block wall from full RA ¹³	Concrete block wall from full RA ¹³
Brick from recycled aggregate	Brick from 67% RA for posts Use recycled bricks 60% ¹⁹	Brick wall from 67% RA $^{\rm 19}$	Brick wall from 67% RA ¹⁹	N/A	N/A	N/A
Steel from average recycled content	Steel sheets of roof from recycled content 100% ^{25, 34}	100% recycled content in	Use steel mesh produced with 100% recycled content, floor and steel sheets of roof ^{25, 34}	Use steel mesh produced with 100% recycled content, floor and steel sheets of roof ^{25, 34}	Use steel mesh produced with 100% recycled content, floor and steel sheets of roof ^{25, 34}	Use steel mesh produced with 100% recycled content, floor and steel sheets of roof ^{25, 34}
Reuse recycled and post- consumer structural and non-structural steel	N/A	N/A	N/A	Use 40% recycled steel in trusses ²⁴	Use 40% recycled steel in trusses ²⁴	Use 40% recycled steel in trusses ²⁴
Reduce material (steel) use in design	N/A	N/A	N/A	Reduced 20% steel use in design ²³	Reduced 20% steel use in design ²³	Reduced 20% steel use in design ²³
Reuse recycled timber and post-consumer FSC timber	Use 60%, recycled timber or FSC certified timber for wall and roof ²³	Use 60%, recycled timber or FSC certified timber for wall and roof ²³	Use 60%, recycled timber or FSC certified timber for wall and roof 23	N/A	Use 60%, recycled timber or FSC certified timber for wall and roof 23	N/A
Roof tile from recycled tile	N/A	Use 13% recycled tile, tiles with 45% with recycled content ²¹	N/A	N/A	N/A	N/A
Thermal insulation from recycled content	Thermal insulation 100% from recycled content in the wall and roof ²⁵	Thermal insulation 100% from recycled content in the wall and roof ²⁵	Thermal insulation 100% from recycled content in the wall and roof 25	Thermal insulation 100% from recycled content in the wall and roof ²⁵	N/A	Thermal insulation 100% from recycled contents in the wall and roof ²⁵
Geopolymer cement replacement for Portland cement	100% replacing PC with GC for fixing timber posts ²⁶	100% replacing PC with GC in concrete slab on ground floor 26	100% replacing PC with GC in concrete slab on ground floor 26	100% replacing PC with GC in concrete slab on ground floor, concrete block wall ²⁶	100% replacing PC with GC in concrete slab, floor, first floor, concrete block wall ²⁶	100% replacing PC with GC in concrete slab on ground floor, concrete block wall ²⁶
Reduce transportation by reusing and recycled materials	Transportation reduced by reuse of recycled materials; 32, 35	Transportation reduced by reuse of recycled materials; ^{32,} ³⁵	Transportation reduced by reuse of recycled materials; 32, 35	Transportation reduced by Transportation reduced by reuse of recycled materials; ^{32,} ³⁵	Transportation reduced by reuse of recycled materials; 32, 35 35	Transportation reduced by reuse of recycled materials; 32, 35
Transportation by water or rail not truck, Reduce transportation by localizing	Transportation reduced by using local supplier and materials ^{19, 30}	Transportation reduced by using local suppliers and materials ^{19, 30}	Transportation reduced by using local suppliers and materials ^{19, 30}	Transportation reduced by using local suppliers and materials ^{19, 30}	Transportation by water; reduced by using local suppliers and materials ^{19, 30}	Transportation reduced by using local suppliers and materials ^{19, 30}

Table 7.1: Research model (bioclimatic criteria) applied to the six case studies (data extracted from Tables 5.4 and 5.6)

Sources:: 1-(CCAA 2015; Gonzalez-Fonteboa 2005); 2-(GBCA 2008); 6-Chapter Seven; 13-(Portland Cement Australia 2014; Uche 2008; 19-(BDA 2014; Tyrell & Goode 2014); 21-(LEED 2014); 23-(GBCA 2008; US Green Building Council 2011); 24-(US Green Building Council 2005); 25-(Greenspec 2015; Steel Construction Information 2014); 26-(Ash Development Association of Australia 2013); 30-(Benn, Dunphy & Griffiths 2014; Learning Legacy 2014); 32-(Allwood et al. 2012; UK Indemand 2014, 2015); 34-(Inhabitat 2014; Steel Construction Information 2014), 35- (DEE 2012)) RA = Recycled Aggregate, PC = Portland cement, GC = Geopolymer Cement.

This Table and data provided by Author.

7.2.1 Case study one – Friendly Beaches Lodge

The Friendly Beaches Lodge is an environmentally well-known project that was designed by Latona Masterman Pty Ltd (Australia), and built in the Freycinet Peninsula of Tasmania in Australia in 1991. This is a private development on an isolated parcel of freehold costal woodland and heath within a national park. The architect sought to provide a basic standard of accommodation for guests completing a guided three-day bushwalk. Traditional domestic timber floor framing is comprised of hardwood beaters and dried hardwood joists. External decks are elevated and constructed from treated pine decking boards. Walls generally are single-skin timber from air-dried hardwoods and plates with kiln hardwood internal lining boards. The roof is timber framed and covered with single sheet steel (see Figure 7.1).

The embodied energy of the floor, wall and roof elements in this construction project were calculated by Lawson (1996). The floor construction system (timber floor) had an implemented embodied energy of 72 MJ/m² of floor area. The wall construction system (single skin timber wall) had an implemented embodied energy of 32 MJ/m² of wall area. The roof construction system (timber frame with single steel sheet covering) had an implemented embodied energy of 230 MJ/m² of roof area (Lawson 1996).

Using this basic data, the research model was applied to this case study, and calculations made of potential reductions in carbon emissions. Detailed calculations are presented in Appendix C, and a summary of potential and generated (i.e. actual) carbon emissions of construction are presented in Tables 7.2 and 7.3 respectively for the floor systems; in Tables 7.4 and 7.5 respectively for the wall construction systems; and Tables 7.6 and 7.7 respectively for the roof construction systems.

Figure 7.1: Friendly Beaches Lodge, Tasmania	Bioclimatic conditions of Case Study One Reuse, recycle, material resources, suppliers, transport			
	Recycled aggregates in material production	80% recycled aggregate assumed to be used for concrete Recycled aggregate assumed to be used for brick		
	Steel from recycled contents	Steel and steel mesh assumed to be used from average recycled content (Steel Construction Information 2014)		
Source: Trip Advisor (2014)		Reuse recycled bricks		
Location: Battery Point, Freycinet Peninsula National Park, Tasmania 7215	construction materials	Use recycled softwood Use recycled thermal insulation Use roof tiles from recycled tiles (LEED 2014)		
Floor construction system: Timber floor	Geopolymer, fly ash and cement substitute	Geopolymer cement replaces Portland cement		
Wall construction system: Single skin timber wall	Transportation reduction	Reduce transportation by (re)using recycled materials		
Roof construction system: Timber frame, steel sheet roof	Material resources and	Construction material resources are inside the park, the saved		
Principal architects: Latona Masterman Pty Ltd. Australia Construction completed 1991	suppliers	distance is 80km, supplier is 237 km and local supplier is 157km (Devonport, Tasmania)		

7.2.2 Case Study Two – ACF Green Home

The Australian Conservation Foundation (ACF) Green Home is a well-known project designed by Taylor Oppenheim Architects, and built in Roxburgh Park in Victoria in 1992. This display home was constructed for the Victorian Department of Planning and Housing in accordance with environmental guidelines prepared by the ACF. The objectives were to create a building for the home market which demonstrated various ways of conserving energy in the day-to-day running of a house, as well as the use of materials selected on the basis of minimum embodied energy.

The ground floor is a concrete slab. Fly ash was incorporated in the concrete mix as a partial cement substitute. The slab was poured over a waterproof membrane manufactured from 70 per cent recycled material. The reinforcing steel was made entirely from recycled materials. The upper floor is constructed in pine framing with a timber floor. External walls are constructed with planation pine timber framing and a clay brick veneer. The roofs are framed in Radiata pine, and concrete tiles are fixed over aluminium foil sarking.

The embodied energy of the floor, wall and roof elements in this construction project were calculated by Lawson (1996). The floor construction system (concrete slab ground floor, timber framed upper floor) had an implemented embodied energy of 537 MJ/m² of floor area. The wall construction system (timber framed brick veneer wall) had an implemented embodied energy of 595 MJ/m² of wall area. The roof construction system (timber frame, concrete tile roof) had an implemented embodied energy of 226 MJ/m² of roof area (Lawson 1996).

Using this basic data, the research model was applied to this case study, and calculations made of potential reductions in carbon emissions. Detailed calculations are presented in Appendix C, and a summary of potential and generated (i.e. actual) carbon emissions of construction are presented in Tables 7.2 and 7.3 respectively for the floor systems; in Tables 7.4 and 7.5 respectively for the wall construction systems; and Tables 7.6 and 7.7 respectively for the roof construction systems.

Figure 7.2: ACF Green Home, Roxburgh Park Victoria		Bioclimatic	conditions of Case Study Two
	ji:		e, materials resources, suppliers,
Cherry Carlos and Carl	8F	Ĉ.	transport
A AND AND AND AND AND AND AND AND AND AN		Recycled	80% recycled aggregate
	×	aggregate in	assumed to be used for concrete
	• • •	materials	Recycled aggregate assumed to
	iZ	production	be used for brick
	¥/te	Steel from	Steel and steel mesh assumed to
	A	recycled	be used from average recycled
	[]	content	content
		Reuse	Reuse recycled bricks
		construction	Use recycled softwood
Source: Environmental Design Guide (EDG 2014)		materials	Use recycled thermal insulation
			Use roof tiles from recycled tiles
		Geopolymer	Geopolymer cement replaces
Location: ACF Green Home, Roxburgh		fly ash	Portland cement
Park Victoria 3064			
Floor construction system: Concrete slab		Transportation	Reduce transportation by
floor, timber framed upper floor		reduction	(re)using recycled materials
Wall construction system: timber framed		Material	Construction materials resources
brick veneer walls		resources and	are local, then the saved distance
Roof construction system: timber Frame,		suppliers)	is 54.2 km (Melbourne Building
concrete tile roof			Supplies 2014), and local
Principal architects: Taylor Oppenheim			supplier is Boral concrete
Architects, Pty Ltd, Australia			Somerton (Boral 2014)
Construction completed 1992			

7.2.3 Case Study Three – Display Project Home

The Display Project House in Canberra was commissioned by the Energy Research and Development Corporation (ERDC) to demonstrate the application of energysaving design measures within a house design which successfully conforms to project home style. The home was designed by Jen-Vue Homes in Ginninderra in the Australian Capital Territory, and construction completed in 1993. The external envelope of the house deliberately used conventional materials and technologies, including a concrete ground slab, brick veneer external walls, and a metal deck roof.

The embodied energy of the floor, wall and roof elements in this construction project were calculated by Lawson (1996). The floor construction system (concrete slab) had an implemented embodied energy of 841 MJ/m^2 of floor area. The wall construction system (timber framed brick veneer) had an implemented embodied energy of 570 MJ/m^2 of wall area. The roof construction system (timber frame steel sheet roof) had an implemented embodied energy of 474 MJ/m^2 of roof area (Lawson 1996).

Using this basic data, the research model was applied to this case study, and calculations made of potential reductions in carbon emissions. Detailed calculations are presented in Appendix C, and a summary of potential and generated (i.e. actual) carbon emissions of construction are presented in Tables 7.2 and 7.3 respectively for the floor systems; in Tables 7.4 and 7.5 respectively for the wall construction systems; and Tables 7.6 and 7.7 respectively for the roof construction systems.

Figure 7.3: Display Project Home,	Bioclimatic conditions of Case Study Three			
Ginninderra, ACT	Reuse, recycle, materials resources, suppliers,			
		transport		
CARLINE CONTRACTOR	Recycled	80% recycled aggregate assumed to		
	aggregate in materials	be used for concrete		
	production	Recycled aggregate assumed to be used for brick		
	Steel from	100% steel and steel mesh assumed		
	recycled	to be used from average recycled		
	content	content		
	Reuse	Reuse recycled bricks		
Source: Lawson (1996)	construction	Use recycled hardwood bearers and		
	materials	joists Use recycled thermal insulation		
		Use recycled mermai misulation		
	Geopolymer	Geopolymer cement replaces		
Location: Ginninderra 2913 ACT	Geopolymer, fly ash	Geopolymer cement replaces Portland cement		
Location: Ginninderra, 2913 ACT Floor construction system: Concrete slab	Geopolymer, fly ash	Geopolymer cement replaces Portland cement		
Floor construction system: Concrete slab	fly ash	Portland cement		
· · · · · · · · · · · · · · · · · · ·	fly ash			
Floor construction system: Concrete slab Wall construction system: timber framed	fly ash Transportation	Portland cement Reduced transportation by reusing/recycling, and transportation by rail or water when		
Floor construction system: Concrete slab Wall construction system: timber framed brick veneer walls	fly ash Transportatior reduction	Portland cement Reduced transportation by reusing/recycling, and transportation by rail or water when required.		
Floor construction system: Concrete slab Wall construction system: timber framed brick veneer walls Roof construction system: timber frame	fly ash Transportation reduction Material	Portland cement Reduced transportation by reusing/recycling, and transportation by rail or water when required. Construction materials from		
Floor construction system: Concrete slab Wall construction system: timber framed brick veneer walls Roof construction system: timber frame steel sheet roof	fly ash Transportation reduction Material resources and	Portland cement Reduced transportation by reusing/recycling, and transportation by rail or water when required. Construction materials from interstate (Thylacine 2014) and		
Floor construction system: Concrete slab Wall construction system: timber framed brick veneer walls Roof construction system: timber frame steel sheet roof Principal architects: Jen-Vue Homes Pty Ltd, Australia	fly ash Transportation reduction Material	Portland cement Reduced transportation by reusing/recycling, and transportation by rail or water when required. Construction materials from interstate (Thylacine 2014) and local supplier is Skyline, the saved		
Floor construction system: Concrete slab Wall construction system: timber framed brick veneer walls Roof construction system: timber frame steel sheet roof	fly ash Transportation reduction Material resources and	Portland cement Reduced transportation by reusing/recycling, and transportation by rail or water when required. Construction materials from interstate (Thylacine 2014) and local supplier is Skyline, the saved distance is 25.2 for local, but the		
Floor construction system: Concrete slab Wall construction system: timber framed brick veneer walls Roof construction system: timber frame steel sheet roof Principal architects: Jen-Vue Homes Pty Ltd, Australia	fly ash Transportation reduction Material resources and	Portland cement Reduced transportation by reusing/recycling, and transportation by rail or water when required. Construction materials from interstate (Thylacine 2014) and local supplier is Skyline, the saved		

7.2.4 Case Study Four – Civil Engineering Laboratory, USQ

The Civil Engineering Laboratory building at the University of Southern Queensland's Springfield campus was designed by Wilson Architects in Brisbane, and was completed in 2013. The floor construction system uses a concrete slab on ground. The wall construction system uses cored concrete blocks. The roof construction system is steel framed with steel roof Colorbond sheeting.

Data for this building was obtained directly from the USQ campus services management section. Using this basic data, the research model was applied to this case study, and calculations made of potential reductions in carbon emissions. Detailed calculations are presented in Appendix C, and a summary of potential and generated (i.e. actual) carbon emissions of construction are presented in Tables 7.2 and 7.3 respectively for the floor systems; in Tables 7.4 and 7.5 respectively for the wall construction systems; and Tables 7.6 and 7.7 respectively for the roof construction systems.

Figure 7.4: Civil Engineering Laboratory	Bioclimatic o	conditions of Case Study Four		
USQ	Reuse, recycle, materials resources, suppliers transport			
	Recycled aggregates in material production	80% recycled aggregate assumed to be used for concrete Recycled aggregate assumed to be used for concrete block		
	Steel from recycled content	100% steel and steel mesh assumed to be used from average recycled content		
	Reduce material use in design	Reduced materials in structural design 20%		
Source: Author	Reuse construction materials	Reuse recycled trusses Use recycled thermal insulation or with recycled content		
Location: Civil Engineering Laboratory, Springfield Central 4300	Geopolymer, fly ash and cement substitute	Geopolymer cement replaces Portland cement		
Floor construction system: concrete slab Wall construction system: concrete block walls Roof construction system: steel frame, steel sheet Roof (Stramit Speed Deck; 0.48 BMT Colorbond steel sheet roof)	Transportation reduction by reuse, recycle, sustainable transportation mode	By reusing and recycling, transportation was reduced Transported when necessary by rail or water		
Principal architects: Wilson Architects, Brisbane Construction completed in 2013	Material resources and suppliers	Construction material resources are inside of state, saved distance is 44.9 km (Global 2014), for local supplier is 32.3km (BIG Mate 2014; Nuway 2014)		

7.2.5 Case Study Five – London Olympic Velodrome Building

This project was constructed on 246 hectares of previously heavily contaminated industrial land – thus, around 700,000 cubic metres of soil was cleaned and reclaimed. Additionally, around 98 per cent of construction materials were recycled from the site's demolished buildings, including a glue factory, a chemical works, and an oil refinery. Final implementation achieved 38 per cent lower carbon emissions than in the original design (CNN 2012; Smith, 2012).

Using construction data from a variety of sources (Rodway 2010; Inventory of Carbon & Energy 2011; Bull 2012; Smith 2012), the research model was applied to this case study, and calculations made of potential reductions in carbon emissions. Detailed calculations are presented in Appendix C, and a summary of potential and generated (i.e. actual) carbon emissions of construction are presented in Tables 7.2 and 7.3 respectively for the floor systems; in Tables 7.4 and 7.5 respectively for the

wall construction systems; and Tables 7.6 and 7.7 respectively for the roof construction systems.

Figure 7.5: Olympic Velodrome Building,	Bioclimatic	conditions of Case Study Five
London	Reuse, recycle,	materials resources, suppliers and transport
	Aggregates for concrete	80% recycled aggregate was used in the concrete (Ingenia 2014)
	Steel and steel mesh	100% steel and steel mesh was used from average recycled content (Steel Construction Information 2014)
	Reduce material use in design	Reduced materials in structural design 20%
Source: London Olympics (2012)	Reuse construction materials	Reuse of leftover gas pipes for construction of the Olympic stadium's ring beam (Karven
Location: Olympic Park, London		2012) Reuse softwood from local salvage/re-use centre (JLL 2012)
Floor construction system: Concrete slab floor, concrete upper floor	Geopolymer, fly ash and cement substitute	Geopolymer cement replaces Portland cement
Wall construction system: concrete block walls, steel frame timber wall	Transportation reduction by	By reusing and recycling, transportation was reduced
Roof construction system: steel frame, fabric roof (commercial)	reuse, recycle, sustainable transportation mode	Transported when necessary was by rail or water (London Olympics 2012)
Principal architects: Jonathan Watts, George Oates, Hopkins, Olympic Park London Construction completed in 2012	Material resources and suppliers	Construction material suppliers are outside London, thus distance is more than 100km (Aggregate Industries 2014)

7.2.6 Case Study Six – Multi Sports Building, USQ

The multi sports building at the University of Southern Queensland's Springfield campus was designed by Reid Design in Brisbane, and construction was completed in 2013. The floor construction uses a concrete ground slab and a concrete upper floor. The wall systems are cored concrete blocks. The roof construction is steel framed with a trussed, steel sheet roof.

Data for this building was obtained directly from the USQ campus services management section. Using this basic data, the research model was applied to this case study, and calculations made of potential reductions in carbon emissions. Detailed calculations are presented in Appendix C, and a summary of potential and generated (i.e. actual) carbon emissions of construction are presented in Tables 7.2

and 7.3 respectively for the floor systems; in Tables 7.4 and 7.5 respectively for the wall construction systems; and Tables 7.6 and 7.7 respectively for the roof construction systems.

Figure 7.6: Multi Sports Building,	Bioclimati	c conditions of case study six
Springfield	Reuse, recycle,	materials resources, suppliers and transport
	Recycled aggregates in material production	80% recycled aggregate assumed to be used for concrete 100% recycled aggregate assumed to be used for concrete block
	Steel from recycled ontent	Steel and steel mesh assumed to be used from average recycled content
Source: Author	Reduce material use in design	Reduced materials in structural design 20%
Location: Multi Sports Building, Springfield Central, 4300	Reuse construction materials	Reuse recycled trusses Use recycled thermal insulation or with recycled content
Floor construction system: concrete slab floor, concrete upper floor	Geopolymer, fly ash and cement substitute	Geopolymer cement replaces Portland cement
Wall construction system: concrete block	Transportation reduction by reuse, recycle, sustainable transportation mode	By reusing and recycling, transportation was reduced Transported when necessary by rail or water
Roof construction system: steel parallel cord trussed roofPrincipal architects: Reid Design Brisbane Construction completed in 2013	Material resources and suppliers	Construction material resources are within the state, saved distance is 44.9 km (Global 2014) and for local supplier is 32.3km (BIG Mate 2014)

7.3 Case studies – Potential carbon emission reductions in floor, wall and roof construction systems

This section identifies the carbon emissions related to the floor, wall and roof construction systems of the case studies during the extraction, materials production and construction processes (stages one to three of the building life cycle), both for each construction system, and then as a whole.

The **potential carbon emission reductions** that could be achieved by application of bioclimatic criteria are presented in Tables 7.2, 7.5 and 7.8 for floor, wall and roof respectively, and for the whole/combined construction systems of the case studies in Table 7.11. There are also percentage calculations of the (potential) carbon emission reductions for the floor, wall and roof construction systems presented in Tables 7.4, 7.7, 7.10 respectively, and for the whole/combined construction systems of the case studies in Table 7.13.

This contrasts with Tables 7.3, 7.6 and 7.9 which present the **generated carbon emissions** of the case studies for floor, wall and roof respectively, and for the whole/combined construction systems of the case studies in Table 7.12. There are also bar graphs that provide a graphical representation of the carbon emissions and results for each construction system of the case studies in Figures 7.7, 7.8 and 7.9 for floor, wall and roof respectively, and one for the whole/combined (floor, wall and roof) construction systems of the case studies in Figure 7.10.

These emission generation figures are obtained by subtracting the emission reduction figure for the item concerned from the standard/basic figure in column one of the corresponding table, the result being the generated carbon emission for the item concerned. Figures in each table are compared for Implementation, the Green Star tool, and the research model. Detailed calculations relating to these tables are presented in Appendix C.

The tables and figures presented in this section compare data from four sources:

• **Standard/Basic carbon emissions**: Carbon emissions to be expected with no application of green or bioclimatic criteria to the building process.

- **Implemented**: The carbon reductions/emissions calculated from implementation (i.e. completion) of the construction element or project concerned
- **Green Star**: The potential carbon reductions/emissions predicted if the criteria of the Green Star tool is applied to a construction system of a given case study.
- This research: The potential carbon reductions/emissions predicted if the bioclimatic criteria of the research model are applied to a construction system of a given case study

An analysis of the findings is presented in Section 7.3.5.

7.3.1 Case studies – Floor construction systems emissions reduction

Tables 7.2 and 7.3 present comparative carbon emission reduction and generation figures for the floor construction systems used in the case studies.

	Standa	rd/Basic								
Floor construction			Impleme	entation		Gree	n Star	This R	esearch	
systems of the case			Reduced or	Increased	Potential	reduction	Potential reduction			
studies	Embodied Carbon Energy Emissions MJ/m ² Kg/m ²	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		
1-Elevated Timber Floor (lowest level)	293	28.71	221	21.65		55.29	5.41	168.82	16.54	
2-Elevated Timber Floor (upper level)	147	14.40	-34	-3.33		86.26	8.45	88.92	8.71	
110 mm Concrete Slab on ground	645	63.21	108	10.58		209.74	20.55	347.30	34.03	
3- 110 mm Concrete Slab on ground	645	63.21	- 196	- 19.2		157.21	15.40	415.06	40.67	
4-200mm Concrete Slab on ground	908	88.98	-	-		262.35	25.71	492.39	48.25	
5-200mm Hollow Core Precast Concrete Slab	908	88.98	600.70	58.86		283.53	27.49	608.10	59.59	
125mm Elevated Concrete Slab temporary frame work	750	73.50	515.60	50.52		259.31	25.41	521.35	51.09	
6-110 mm Concrete Slab on ground	645	63.21	-	-		206.68	20.25	382.03	37.44	
125mm Elevated Concrete Slab temporary frame work	750	73.50	-	-		247.27	24.23	438.98	43.02	

 Table 7.2: Potential carbon emission (embodied energy) reductions for the floor construction systems of the case studies

Sources: 'Standard/Basic' column represents construction carbon emissions (embodied energy) from values given in Chapter Four; the 'Implementation', 'Green Star' and 'This research' columns are the potential construction carbon emission (embodied energy) reductions as calculated in Appendix C (Tables A.C.-1, 8, 9, 17, 24, 30, 32, 33, 42, 43, 44, 52, 53).

case studies								
Floor construction	Standar	rd/Basic	Implen	nented	Gree	n Star	This re	esearch
systems of the case studies of the research	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²						
1-Elevated Timber Floor (lowest level)	293	28.71	72	7.06	237.71	23.29	124.18	12.17
2- Elevated Timber Floor (upper level)	147	14.40	113	11.07	60.74	5.95	58.08	5.69
110 mm Concrete Slab on ground	645	63.21	537	52.62	435.26	42.65	297.70	29.17
3-110 mm Concrete Slab on ground	645	63.21	841	82.41	487.79	47.80	229.94	22.53
4-200mm Concrete Slab on ground	908	88.98	-	-	645.65	63.27	415.61	40.73
5-200mm Hollow Core Precast Concrete Slab	908	88.98	307.3	30.11	624.47	61.49	299.90	29.39
125mm Elevated Concrete Slab temporary frame work	750	73.50	234.4	22.97	490.69	48.08	228.65	22.40
6-110 mm Concrete Slab on ground	645	63.21	-	-	438.32	42.95	262.97	25.77
125mm Elevated Concrete Slab temporary frame work	750	73.50	-	-	502.73	49.26	311.02	30.48

Table 7.3: Carbon emissions (embodied energy) generated in the floor construction systems of the case studies

Source: 'Standard/Basic' column is from values given in Chapter Four; 'Implementation', 'Green Star' and 'This Research' columns are the generated construction carbon emissions (embodied energy) obtained from Table 7.2 (subtract reduction figures from standard/basic figures)

The bar graph in Figure 7.7 provides a comparative representation of the generated carbon emissions data for the floor systems of the case studies (as given in Table 7.3).

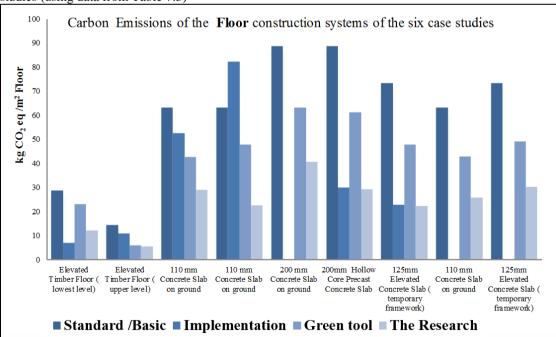


Figure 7.7: Bar graph of carbon emissions generated for the **floor** construction systems of the case studies (using data from Table 7.3)

Source: Generated carbon emissions data from Table 7.3

Table 7.4 provides a percentage representation of the potential carbon emission reductions for the case studies using the data from Table 7.2.

Floor construction systems of the case studies	Implemented	Green Star	This Research
studies	Reduction	Reduction	Reduction
1-Elevated Timber Floor (lowest level)	75.4%	18.8%	57.6%
2-Elevated Timber Floor (upper level)	Increase -23.1%	58.6%	60.4%
110 mm Concrete Slab on ground	16.7 %	32.5%	<mark>53.8%</mark>
3- 110 mm Concrete Slab on ground	Increase- 30.3%	24.3%	64.3%
4-200mm Concrete Slab on ground	-	28.8%	54.2%
5-200mm Hollow Core Precast Concrete Slab	66.1%	30.8%	66.9%
125mm Elevated Concrete Slab temporary frame work	68.7%	34.5%	<mark>69.5%</mark>
6-110 mm Concrete Slab on ground	-	32%	59.2%
125mm Elevated Concrete Slab temporary frame work	-	32.9%	58.5%

Table 7.4: Potential carbon emission (embodied energy) **reductions** for the **floor** construction systems of the case studies expressed as percentages (using data from Table 7.2)

Source: Data from Table 7.2 expressed in percentage form. Highlighting indicates reference to figures in the discussion in Section 7.3.5.

7.3.2 Case studies – Wall construction systems emissions reduction

Tables 7.5 and 7.6 present comparative carbon emission reduction and generation figures for the wall construction systems used in the case studies.

	Standa	rd/Basic	Potential Reduction											
Wall construction				Implem	entation		Gree	n Star		This R	esearch			
systems of the case				Reduced or	Increased		Potential	reduction		Potential reduction				
studies	Embodied	Carbon		Embodied	l Carbon		Embodied	Carbon		Embodied	Carbon			
studies	Energy	Emissions		Energy	Emissions		Energy	Emissions		Energy	Emissions			
	MJ/m ²	Kg/m ²		MJ/m ²	Kg/m ²		MJ/m ²	Kg/m ²		MJ/m ²	Kg/m ²			
1-Timber Frame, Single Skin Timber Wall	151	14.79		119	11.66		25.17	2.47		72.71	7.12			
2-Timber Frame, Clay Brick Veneer Wall	561	54.97		-34	- 3.33		21.77	2.13		256.48	25.13			
3-Timber Frame, Clay Brick Veneer Wall	561	54.97		- 9	- 0.88		23.44	2.29		257.47	25.23			
4-Cavity Concrete Block Wall	511	50.07		-	-		96.48	9.46		248.34	24.34			
5-Cavity Concrete Block Wall	511	50.07		336.81	33.01		106.77	10.46		336.81	33.01			
Steel Frame, timber w/board Wall	238	23.32		134.01	13.13		125.44	12.29		134.01	13.13			
6-Cavity Concrete Block Wall	511	50.07		-	-		96.48	9.45		248.34	24.34			

 Table 7.5: Potential carbon emission (embodied energy) reductions for the wall construction systems of the case studies

Sources: 'Standard/Basic' column represents construction carbon emissions (embodied energy) from values given in Chapter Four; the 'Implementation', 'Green Star' and 'This research' columns are the potential construction carbon emission (embodied energy) reductions as calculated in Appendix C (Tables A.C. – 3, 4, 12, 13, 19, 20, 25, 26, 34, 35, 36, 37, 46, 47, 48, 54, 55)

Table 7.6: Carbon emissions (embodied energy) generated in the wall construction systems of the case studies

Wall construction	Standa	rd/Basic	Implen	nented	Gree	en Star	This re	esearch
systems of the case studies	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²						
1-Timber Frame, Single Skin Timber Wall	151	14.79	32	3.1	125.83	12.33	78.29	7.67
2-Timber Frame, Clay Brick Veneer Wall	561	54.97	595	58.3	539.23	52.84	304.52	29.84
3-Timber Frame, Clay Brick Veneer Wall	561	54.97	570	55.9	537.56	52.68	303.53	29.74
4-Cavity Concrete Block Wall	511	50.07	-	-	414.52	40.62	262.66	25.74
5-Cavity Concrete Block Wall	511	50.07	174.19	17.07	404.23	39.61	174.19	17.07
Steel Frame, timber w/board Wall	238	23.32	103.99	10.19	112.56	11.03	103.99	10.19
6-Cavity Concrete Block Wall	511	50.07	-	-	414.52	40.62	262.66	25.74

Source: 'Standard/Basic' column is from values given in Chapter Four; 'Implementation', 'Green Star' and 'This Research' columns are the generated construction carbon emissions (embodied energy) obtained from Table 7.4 (subtract reduction figures from standard/basic figures)

The bar graph in Figure 7.8 provides a comparative representation of the generated carbon emissions data for the wall systems of the case studies (as given in Table 7.6).

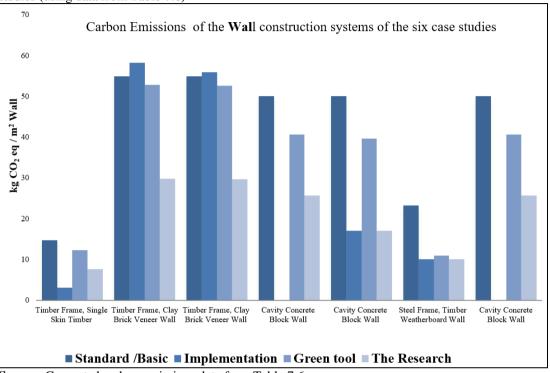


Figure 7.8: Bar graph of carbon emissions generated for the **wall** construction systems of the case studies (using data from Table 7.6)

Source: Generated carbon emissions data from Table 7.6

Table 7.7 provides a percentage representation of the potential carbon emission reductions for the case studies using the data from Table 7.2.

Table 7.7: Potential carbon emission (embodied energy) reductions for the wall construction systemsof the case studies expressed as percentages (using data from Table 7.5)

Wall construction systems of	Implemented	Green Star	This Research
the case studies	Reduction	Reduction	Reduction
1-Timber Frame, Single Skin Timber Wall	78.8%	17.7%	48.1%
2-Timber Frame, Clay Brick Veneer Wall	Increase - 6%	3.8%	<mark>45.7%</mark>
3-Timber Frame, Clay Brick Veneer Wall	Increase - 1.6%	4.1%	45.8%
4-Cavity Concrete Block Wall	-	18.8%	48.6%
5-Cavity Concrete Block Wall	65.9%	20.8%	<mark>65.9%</mark>
Steel Frame, timber w/board Wall	56.3%	52.7%	56.3%
6-Cavity Concrete Block Wall	-	18.8%	48.6 %

Source: Data from Table 7.5 expressed in percentage form. Yellow highlighting indicates reference to figures in the discussion in Section 7.3.5.

7.3.3 Case studies – Roof construction systems emissions reduction

Tables 7.8 and 7.9 present comparative carbon emission reduction and generation figures for the roof construction systems used in the case studies.

	Standa	rd/Basic				Potential	Reduction					
			Implem	entation		Green Star			This R	esearch		
Roof construction systems of the case			Reduced or	Reduced or Increased			reduction		Potential reduction			
studies	Embodied	Carbon	Embodied	Carbon		Embodied	Carbon		Embodied	Carbon		
	Energy MJ/m ²	Emissions Kg/m ²	Energy MJ/m ²	Emissions Kg/m ²		Energy MJ/m ²	Emissions Kg/m ²		Energy MJ/m ²	Emissions Kg/m ²		
1-Timber Frame, Steel Sheet Roof	330	32.34	100	9.80		114.48	11.22		144.59	14.17		
2-Timber Frame, Concrete Tile Roof	240	23.52	14	1.37		45.16	4.42		91.51	8.97		
3-Timber Frame, Steel Sheet Roof	330	32.34	-144	-14.11		114.48	11.22		144.59	14.17		
4-Steel Frame, Steel Sheet Roof	401	39.29	-	-		145.65	14.28		231.85	22.72		
5-Steel Frame, Fabric Roof (commercial)	282	27.63	182.82	17.91		84.49	8.28		144.72	14.18		
6-Steel parallel chord trussed sheet roof	401	39.29	-	-		145.65	14.27		231.85	22.72		

 Table 7.8: Potential carbon emission (embodied energy) reductions for the roof construction systems of the case studies

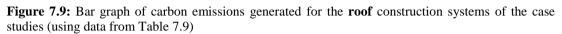
Sources: 'Standard/Basic' column represents construction carbon emissions (embodied energy) from values given in Chapter Four; the 'Implementation', 'Green Star' and 'This research' columns are the potential construction carbon emission (embodied energy) reductions as calculated in Appendix C (Tables A.C. – 5, 6, 14, 15, 21, 22, 27, 28, 39, 40, 48, 49, 56)

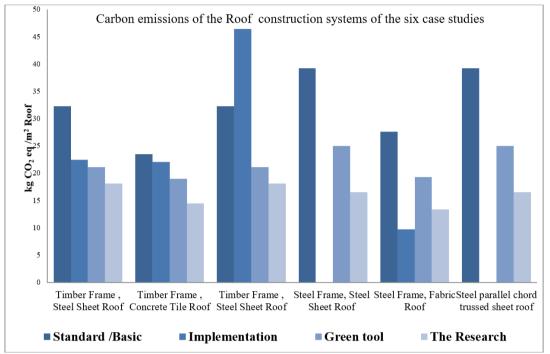
Table 7.9: Carbon emissions (embodied energy) generated in the roof construction systems of the case studies

Roof construction	Standa	rd/Basic	Implen	nented	Gree	en Star	This research			
systems of the case studies	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²								
1-Timber Frame, Steel Sheet Roof	330	32.34	230	22.54	215.52	21.12	185.41	18.17		
2-Timber Frame, Concrete Tile Roof	240	23.52	226	22.15	194.84	19.09	148.49	14.55		
3-Timber Frame, Steel Sheet Roof	330	32.34	474	46.45	215.52	21.12	185.41	18.17		
4-Steel Frame, Steel Sheet Roof	401	39.29	-	-	255.35	25.02	169.15	16.57		
5-Steel Frame, Fabric Roof (commercial)	282	27.63	99.18	9.72	197.51	19.35	137.28	13.45		
6-Steel parallel chord trussed sheet roof	401	39.29	-	-	255.35	25.02	169.15	16.57		

Sources: Standard/Basic' column is from values given in Chapter Four; 'Implementation', 'Green Star' and 'This Research' columns are the generated construction carbon emissions (embodied energy) obtained from Table 7.6 (subtract reduction figures from standard/basic figures)

The bar graph in Figure 7.9 provides a comparative representation of the generated carbon emissions data for the roof systems of the case studies (as given in Table 7.9).





Source: Generated carbon emissions data from Table 7.9

Table 7.10 provides a percentage representation of the potential carbon emission reductions for the case studies using the data from Table 7.8

 Table 7.10: Potential carbon emission (embodied energy) reductions for the roof construction systems of the case studies expressed as percentages (using data from Table 7.8)

Roof construction systems of	Implemented	Green tool	This Research			
the case studies	Reduction	Reduction	Reduction			
1-Timber Frame, Steel Sheet Roof	30.3%	34.6%	43.8%			
2-Timber Frame, Concrete Tile Roof	5.8%	18.7%	<mark>38.1%</mark>			
3-Timber Frame, Steel Sheet Roof	Increase - 43.6%	34.6%	43.8%			
4-Steel Frame, Steel Sheet Roof	-	36.3%	57.8%			
5-Steel Frame, Fabric Roof (commercial)	64.8%	29.9%	51.3%			
6-Steel parallel chord trussed sheet roof	-	36.3%	<mark>57.8%</mark>			

Source: Data from Table 7.8 expressed in percentage form. Yellow highlighting indicates reference to figures in the discussion in Section 7.3.5.

7.3.4 Case studies – Whole construction systems emissions reduction

The final summary table presented in this section is for the whole construction system of each case study which collates the figures for the floor, wall and roof construction systems presented in Tables 7.2 to 7.7. The comparative data for potential carbon emission reductions in the six case studies is presented in Table 7.8, and the comparative data for generated carbon emissions is presented in Table 7.9.

 Table 7.11: Potential construction carbon emission (embodied energy) reductions for the whole (floor, wall and roof) construction systems of the six case studies

	Standa	rd/Basic				Potential	Reduction				
				Implem	entation	Green Star			This R	esearch	
Case studies of the				Reduced or	Increased	Potentia	reduction		Potential reduction		
research	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²	
1. Friendly Beaches Lodge	774	75.85		440	43.12	194.94	19.10		386.12	37.84	
2. ACF Green Home	1623	159.05		122	11.95	276.67	27.11		783.86	76.81	
3. Display Project Home	1536	150.52		347	34	295.13	28.92		817.12	80.07	
4. Civil Engineering Lab.	1820	178.36		-	-	504.48	49.45		972.58	95.31	
5. Velodrome Building	2689	263.52		1769.9	173.4	856.54	83.94		1744.99	170.98	
6. Multi Sports Building	2307	226.08		-	-	696.08	68.21		1301.20	127.51	

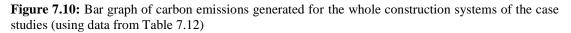
Sources: 'Standard/Basic' column represents construction carbon emissions (embodied energy) from values given in Chapter Four; the 'Implementation', 'Green Star' and 'This research' columns are the potential construction carbon emission (embodied energy) reductions as calculated in Appendix C (Tables A.C. – 7, 16, 23, 29, 40, 50, 57)

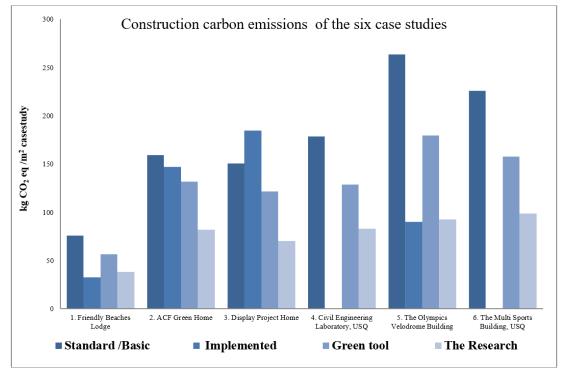
Table 7.12: Carbon emissions (embodied energy) generated in the whole (floor, wall and roof) construction systems of the case studies

Case studies of the research	Standard or Basic		Implemented			Green Star		This research	
	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²
1. Friendly Beaches Lodge	774	75.85	334	32.73		579.06	56.75	387.88	38.01
2. ACF Green Home	1623	159.05	1501	147.10		1346.33	131.94	839.14	82.23
3. Display Project Home	1536	150.52	1883	184.53		1240.87	121.60	718.88	70.45
4. Civil Engineering Lab.	1820	178.36	-	-		1315.52	128.92	847.42	83.04
5. Velodrome Building	2689	263.52	919.1	90.07		1832.46	179.58	944.01	92.51
6. Multi Sports Building	2307	226.08	-	-		1610.92	157.87	1005.80	98.57

Sources: 'Standard/Basic' column is from values given in Chapter Four; 'Implementation', 'Green Star' and 'This Research' columns are the generated construction carbon emissions (embodied energy) obtained from Table 7.8 (subtract reduction figures from standard/basic figures)

The bar graph in Figure 7.10 provides a comparative representation of the generated carbon emissions data for the whole construction systems of the case studies (as given in Table 7.12).





Source: Generated carbon emissions data from Table 7.12

Table 7.13 provides a percentage representation of the potential carbon emission reductions for the whole construction systems of the case studies (using the data from Table 7.11).

Table 7.13: Potential carbon emission (embodied energy) reductions for the whole constructionsystems of the case studies expressed as percentages (using data from Table 7.11)

Case studies of the research	Implemented	Green tool	This Research
	Reduction	Reduction	Reduction
1. Friendly Beaches Lodge	<mark>56.7%</mark>	25.2%	49.8%
2. ACF Green Home	7.5%	<mark>17%</mark>	<mark>48.3%</mark>
3. Display Project Home	- 22.6%	19.2%	53.2%
4. Civil Engineering Lab	-	30%	53.4%
5. The Velodrome Building	<mark>65.8%</mark>	<mark>31.9%</mark>	<mark>64.9%</mark>
6. The Multi Sports Building	-	30.2%	56.4%

Source: Data from Table 7.11 expressed in percentage form. Yellow highlighting indicates reference to figures in the discussion in Section 7.3.5.

7.3.5 Analysis of data from the floor, wall and roof systems of the case studies

In respect to the floor construction systems of the case studies, the bar graph of carbon emissions generated (Figure 7.7) indicates that emissions following application of the research model to the floor systems are consistently lower than for the other three scenarios (standard building practice, at implementation/completion of a floor construction project, and following application of the Green Star tool). Similar trends are seen when the bar graph of generated carbon emissions of the wall and roof construction systems are considered (Figures 7.8 and 7.9). The generated carbon emissions for wall and roof systems are generally lower following application of the bioclimatic criteria in the research model as compared to the standard building practice, on completion of a building, and following application of the Green Star tool. This is also the case for generated emissions for the whole construction systems of the case studies as shown in Figure 7.10.

This trend is also seen when carbon reductions are considered. Potential carbon emission reductions data for the floor, wall and roof construction systems of the case studies are presented in Tables 7.4, 7.7 and 7.10 respectively as percentage reductions. There is a similar presentation of percentage data for the combined/whole construction systems of the case studies in Table 7.13. Analysis of these figures indicates that, in all cases, the potential carbon emission reductions are generally higher with application of the research model as compared to the implemented and Green Star results.

In analysis of the data presented in the tables and figures in this section, as compared to the carbon emissions from standard building practice, there are generally considerable reductions in construction carbon emissions that can be achieved through use of environmentally-friendly building practices. The highest overall reduction was achieved in the whole construction system of the 2012 Olympics Velodrome building (Case Study 5), at 65.8 per cent (Table 7.13). This was at implementation of the building and presumably reflects the focus on sustainable material usage in the construction of the Velodrome.

Application of the criteria in the Green Star tool to the construction process (Table 7.13) again shows significant reductions across all buildings considered in the case

studies, with the highest at 31.9 percent, again for the Olympic Velodrome (Case Study 5). The figures for the Olympic Velodrome (Case Study 5) are about equal for the implemented and research model reductions (65.8 per cent and 64.9 percent respectively). This Velodrome building was, in fact, implemented by the London Olympic builders to achieve maximum emission reduction during construction, and it obviously has achieved this.

It is also noted that the potential carbon emission reduction for the Friendly Beaches Lodge (Case Study 1) as implemented (constructed) is higher than achieved through application of the research model (56.7 per cent compared to 49.8 percent – Table 7.13). This is presumably due to the environmental considerations applied at implementation of the project in this particular case study.

Overall, however, the research model using bioclimatic criteria clearly shows the greatest potential for reduction in construction carbon emissions across the six case studies as compared to standard construction carbon emissions and those achievable following application of the Green Star tool. The lowest carbon reduction was 48.3 per cent for the ACF Green Home (Case Study 2), and the highest for the Olympic Velodrome at 64.9 percent for their whole construction systems (Table 7.13). In fact, in many cases, reductions in construction carbon emissions could be approximately doubled by use of the criteria in the research model tool as compared with Green Star and current best practice.

In respect to application of the research model's bioclimatic criteria to the construction systems of the case studies, it is noted that:

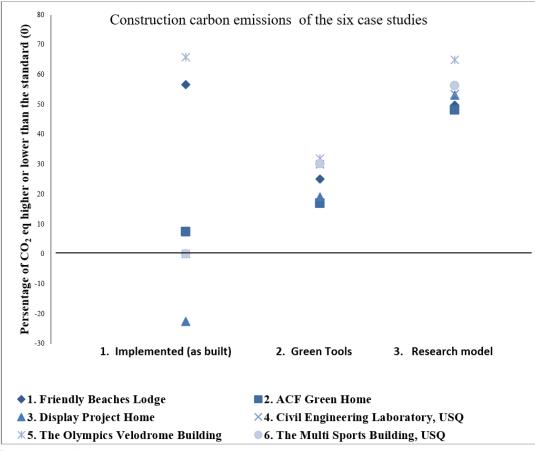
- For the floor construction systems (Table 7.4), the potential reductions in carbon emissions are between 53.8 and 69.5 per cent, the highest percentage being for the Olympics Velodrome Building's concrete slab floor (Case Study 5).
- For the wall construction systems (Table 7.7), the potential reductions in carbon emissions are between 45.7 and 65.9 per cent, the highest being for the Velodrome Building's concrete block wall (Case Study 5).
- For the roof systems (Table 7.10), the potential reductions in carbon emissions are between 38.1 and 57.8 per cent, the highest being in the Civil

Engineering Lab and the Multi Sports building roof construction systems (Case Studies 4 and 6).

• For the combined/whole construction systems (Table 7.13), the potential reductions in carbon emissions are between 48.3 and 64.9 per cent, the highest being for the Velodrome building (Case Study 5).

These results are displayed graphically in Figure 7.11 which compares the carbon emission reductions achieved in the case studies at implementation, and then through application of the Green Star tool and the research model tool. From these results, the conclusion can be made that application of the research model to the construction systems of the case studies can achieve potential reduction in carbon emissions of from 50 to 65 per cent.

Figure 7.11: Carbon emission reductions in the whole construction systems of the case studies achieved at Implementation, and then by application of the Green Star and the research model tools



Source: Data from Table 7.13

A summary table of the bioclimatic design principles used in the research model, and the percentage potential reductions in carbon emissions of the research compared to those from implantation and green tools is presented in Table 7.14.

Bioclimatic Design Principles (BDP)	Current conditions, Implemented	Conditions with Green tools G.S., LEED, BRE	Through Bioclimatic Principles Conditions in this research
Concrete from recycled aggregates	In Australia, there are a number of manufactured and recycled aggregates readily available in certain localities ¹	G.S. and LEED 1-3 points 20-30% RA for structural purpose; BRE 20% in 20-40 MPa - no restriction, 100% non-structural ^{2, 18, 36}	Fully RA for non-structural purposes; 100% RA for non-structural; 80 % RA for structural purpose ⁶
Concrete block from recycled aggregate	24% recycled content of an aggregate concrete block ⁸	G.S., BRE, 40%; US 25% RA structural; 100%, or no natural aggregates in non-structural ^{18,23,36}	Aggregate for concrete block fully from recycled aggregate ¹³
Brick from recycled aggregates	Current level of recycled material content in brick is 11% 14.41	G.S. 30% $^{16, 23}$; LEED 20%; BRE 11% ISO, up to 10 points for 10% Recycled aggregate 14,16,36	Reuse recycled aggregate for brick, 67% 19
Steel from average recycled content	Primary typically 10-15% of scrap steel Secondary 100% scrap based production ^{25, 34}	G.S. Mat-6, 60%; LEED 65-97.5%; BRE, Mat-6, 60%; - 97.5% beams, plates; 65% bars; 66% steel deck post- consumer recycled content ^{23,16,38}	Steel from fully post-consumer recycled content
Reuse recycled and post- consumer structural and non- structural steel	Scaffolding, formwork, sheet piles, etc., London Olympic Stadium ^{32, 34}	G.S., 95% Joinery, 50% structural framing, roofing; LEED 75-100% existing wall, floor, roof; BRE, Mat-6, 60% recycled content ^{3,5,23,24}	Use 40% recycled and post-consumer steel elements
Reduce material use in steel structural design 10-20%	Some of the current green projects have reduced materials use in design 10-20% ²³	G.S., Mat-6, 10-20% one point; LEED, eliminating need for materials in the design stage; BRE reduced, avoiding over-design ^{23,21,10,7,32}	Reduced materials use in structural design 10-20%
Reuse the recycled timber and post-consumer FSC timber	FSC works in 80 countries, 24000 FSC chain of custody certificates are active in 107 countrie. ^{23,}	G.S. 95% re-used, post-consumer; FSC certified timber; up to 3 points; LEED, 50% FSC; BRE, 3 points, post-consumer waste stream ^{22, 23, 32,24,29}	60% of all timber products re-used, post-consumer recycled timber; FSC certified timber
Roof tile from recycled tile	In some countries materials such as concrete roof tiles, are removed separated and recycled ^{44, 45}	G.S. Mat-5, 1 point, no natural aggregates are used; LEED, from the waste, up to3.5 points, BRE, M03, from the waste stream; ^{20,21,23,36}	50% Roof tile from recycled aggregate ²¹
Thermal insulation from recycled content	Thermal insulation is fully recyclable, i.e. wool content ³¹	G.S. 80% advised; LEED MR4 20%, ¹ / ₂ point, BRE 80%, 1 point, responsibly sourced ^{12,7,27,37}	Thermal insulation from fully recycled waste ²⁵
Portland cement replaced with Geopolymer based cement	Geopolymer has been used structural, non- structural, University GCI in Qld, Wellcamp Airport, Qld ^{46,47,48}	G.S. 60% In situ concrete; 40% precast 30% stressed concrete; LEED, 30% structural; no limit others, BRE, responsibly sourced cement ^{23,26,7}	Geopolymer based cement fully replaces Portland cement, arranged for non-structural, structural
Reduce transportation by reusing and recycled materials	National Waste Policy Australia advice to reduce waste, re-use to reduce environmental impacts ³⁵	Green tools credit the reusing and recycling of up to 40% of materials, not directly credited; obtained from30km radius of the site ^{2,15,35,37}	Reuse considered in material production and building elements
Transportation by water or rail not truck, reduce transportation by localizing	15% of bricks are transported to the distributor's yard or jobsite by rail and 85% by truck ^{19, 30}	LEED, Regional Materials, up to 2 points ¹⁴ Tools advise localizing, using water and rail instead of road 2 ¹⁵	Localizing has been considered
CONSTRUCTION CARBON EMISSIONS REDUCTION	CASE STUDIES: IMPLEMENTATION → BETWEEN -23% AND 57%	CASE STUDIES: GREEN TOOL → POTENTIAL BETWEEN 17 TO 32 %	CASE STUDIES: RESEARCH MODEL POTENTIAL BETWEEN 50 AND 65 %

Table 7.14: Bioclimatic conditions – current; from best practice with green tools (Green Star, LEED and BREEAM); from this research model (BDP)

References and detailed information of this table is presented in Table A.D.3 | RA = Recycled Aggregate, From Author

7.4 General Australian floor, wall and roof construction systems – Potential carbon emission reductions

In this section, the research model and Green Star criteria are applied to the general Australian construction systems of floor, wall and roof (i.e. construction systems unrelated to the case studies). The bioclimatic criteria applied are summarised in Table 7.15.

The **potential carbon emission reductions** achievable by application of bioclimatic criteria to the floor, wall and roof of general Australian construction systems are presented in Tables 7.16, 7.19 and 7.22 respectively. There are also percentage calculations of the potential carbon emission reductions for the floor, wall and roof construction systems presented in Tables 7.18, 7.21 and 7.24 respectively for floor, wall and roof systems.

This contrasts with Tables 7.17, 7.20 and 7.23 which present the **generated construction carbon emissions** for floor, wall and roof respectively. These figures are obtained by subtracting the emission reduction figure for the item concerned from the standard/basic figure in column one of the corresponding table, the result being the generated carbon emission for the item concerned. Figures in each table are compared for the Green Star tool and the research model. Detailed calculations relating to these tables are presented in Appendix C.

The tables and figures presented in this section compare data from three sources:

- **Standard/Basic carbon emissions**: Carbon emissions to be expected with no application of green or bioclimatic criteria to the building process.
- **Green Star**: The potential carbon reductions/emissions predicted if the criteria of the Green Star tool is applied to a given construction system.
- **This research**: The potential carbon reductions/emissions predicted if the bioclimatic criteria of the research model are applied

An analysis of the findings is presented in Section 7.4.4.

Table 7.15: Bioclimatic criteria examined in general Australian floor, wall and roof construction systems using the research model and the Green Star rating tool

Bioclimatic criteria		A.1 Floor construction systems	A.2. Wall construction systems	A.3. Roof construction systems		
Concrete from recycled aggregates	Study	80% RA for fixing posts in the ground ¹	80 % RA for concrete slab on ground 1	80 % RA for concrete slab on ground $^{\rm 1}$		
	Green Star	20% RA for fixing posts in the ground 2	20 % RA for fixing posts in the ground 2	20 % RA for fixing posts in the ground $^{\rm 2}$		
Concrete block and brick from recycled	Study	-	Concrete block wall from (67-100%) RA ³	-		
aggregate	Green Star	-	Concrete block wall from 20% RA ³	-		
Brick from recycled aggregate	Study	Brick from 67% RA for posts Use recycled bricks %60 ⁴	Brick wall from 67% RA ⁴	-		
	Green Star	-	-	-		
Steel from average recycled content	Study	Use steel produced with 100% recycled content ^{8,13}	Use steel produced with 100% recycled content ^{8,13}	Use steel produced with 100% recycled content ^{8,13}		
	Green Star	Use steel produced with 90% recycled content ^{6,7}	Use steel produced with 90% recycled content ^{6,7}	Use steel produced with 90% recycled content ^{6,7}		
Reuse recycled and post-consumer structural and non-	Study	Reuse 40% recycled steel in structural and non-structural elements ^{31,32}	Reuse 40% recycled steel in structural and non-structural elements ^{31,32}	Reuse 40% recycled steel in the structural and non-structural elements ^{31,32}		
structural steel	Green Star	-	-	-		
Reduce material (steel) use in design	Study	Reduced 20% steel use in design ^{12, 14}	Reduced 20% steel use in design ^{12, 14}	Reduced 20% steel use in design ^{12, 14}		
10-20%		Reduced 20% steel use in design ^{, 15,16, 5, 6, 12}	Reduced 20% steel use in design ^{, 15,16, 5, 6, 12}	Reduced 20% steel use in design ^{15,16, 5, 6, 12}		
Reuse recycled timber and post-consumer FSC certified timber	Study	Use 100%, recycled timber or FSC certified timber, reuse ^{6,}	Use 100%, recycled timber or FSC certified timber, reuse ⁶ , ¹⁷	Use 100%, recycled timber or FSC certified timber, reuse ^{6,}		
	Green Star	Use 100%, recycled timber or FSC certified timber, reuse ^{6,} 7, 12, 18, 19	Use 100%, recycled timber or FSC certified timber, reuse ^{6,} 7, 12, 18, 19	Use 100%, recycled timber or FSC certified timber, reuse ^{6, 7,} ^{12, 18, 19}		
Roof tile from recycled tiles	Study	-	-	Use 13% recycled tile, tiles with 45% recycled content ^{5, 20}		
	Green Star	-	-	-		
Thermal insulation from recycled content	Study	-	Thermal insulation 100% from recycled content ⁸	Thermal insulation 100% from recycled content ⁸		
	Green Star	-	-	-		
Replaced Portland cement with	Study	Replace 100% of Portland cement with geopolymer ^{12, 21}	Replace 100% of Portland cement with geopolymer ^{12, 21}	Replace 100% of Portland cement with geopolymer ^{12, 21}		
geopolymer cement	Green Star	Replace 60% of Portland cement with geopolymer ^{6,9,} ²²	Replace 60% of Portland cement with geopolymer ^{6,9,} ²²	Replace 60% of Portland cement with geopolymer ^{6,9,22}		

References, specifications and detailed information relating to this table are presented in Table A.D.4 (Appendix D). (RA = Recycled Aggregates)

7.4.1 Potential emission reductions in general Australian floor construction systems

Tables 7.16 and 7.17 present comparative carbon emission reduction and generation figures for general Australian floor construction systems.

 Table 7.16: Potential carbon emission (embodied energy) reductions for general Australian floor construction systems

	Stan	dard		Potential Reduction						
General Australian floor construction	/Basic			Green Star			This research			
systems	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		
a-Elevated Timber Floor (lowest level)	293	28.7		45.6	4.46		146.58	14.36		
b-Elevated Timber Floor (upper level)	147	14.4		84.60	8.29		84.60	8.29		
c-110 mm Concrete Slab on ground	645	63.21		194.70	19.08		291.46	28.56		
d-125mm Elevated Concrete Slab (temporary framework)	750	73.5		234.76	23.01		344.72	33.78		
e-110mm Elevated Concrete Slab (permanent framework)	665	65.17		218.14	21.37		292.3	28.64		
f- 200mm Precast Concrete Tee Beam/Infill flooring	602	59		238.46	23.36		273.50	26.80		
g-200mm Hollow Core Precast Concrete flooring	908	88.98		249.05	24.40		383.07	37.54		

Sources: 'Standard/Basic' column represents construction carbon emissions (embodied energy) from values given in Chapter Four; the 'Green Star' and 'This research' columns are the potential construction carbon emission (embodied energy) reductions as calculated in Appendix C (Tables A.C.58-A.C.69)

 Table 7.17: Carbon emissions (embodied energy) generated in the general Australian floor construction systems

General Australian floor construction	Standard /Basic			Green Star			This research	
systems	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²
a-Elevated Timber Floor (lowest level)	293	28.7		247.4	24.24		146.42	14.34
b-Elevated Timber Floor (upper level)	147	14.4		62.4	6.11		62.4	6.11
c-110 mm Concrete Slab on ground	645	63.21		450.30	44.12		353.54	34.64
d-125mm Elevated Concrete Slab (temporary framework)	750	73.5		515.24	50.49		405.28	39.71
e-110mm Elevated Concrete Slab (permanent framework)	665	65.17		446.86	43.79		373	36.55
f- 200mm Precast Concrete Tee Beam/Infill flooring	602	59		363.54	35.62		328.5	32.19
g-200mm Hollow Core Precast Concrete flooring	908	88.98		658.95	64.57		524.91	51.44

Sources: 'Standard/Basic' column is from values given in Chapter Four; the 'Green Star' and 'This Research' columns are the generated construction carbon emissions (embodied energy) obtained from Table 7.16 (subtract reduction figures from standard/basic figures)

The bar graph in Figure 7.12 provides a comparative representation of the generated carbon emissions data for general Australian floor systems (as given in Table 7.17).

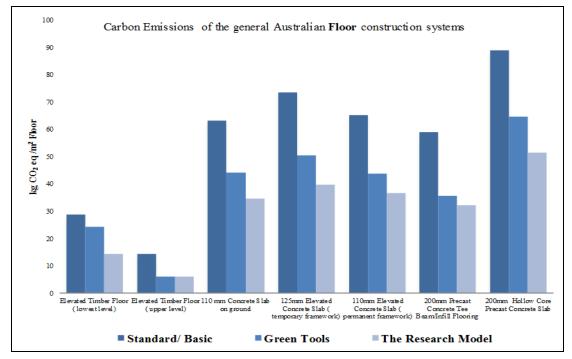


Figure 7.12: Bar graph of carbon emissions generated for general Australian floor construction systems (using data from Table 7.17)

Source: Generated carbon emissions data from Table 7.17

Table 7.18 provides a percentage representation of the potential carbon emission reductions that can be achieved in general Australian floor construction systems by application of the Green star and research model tools (using data from Table 7.16).

Table 7.18: Potential carbon emission reductions in general Australian floor construction system	S
expressed as percentages (using data from Table 7.16)	

	Green Star	This research
General Australian floor construction systems	Carbon Emissions	Carbon Emissions
	Kg/m ²	Kg/m ²
a-Elevated Timber Floor (lowest level)	<mark>15.56%</mark>	50.02%
b-Elevated Timber Floor (upper level)	<mark>57.55%</mark>	<mark>57.55%</mark>
c-110 mm Concrete Slab on ground	30.18%	45.17%
d-125mm Elevated Concrete Slab (temporary framework)	31.30%	45.96%
e-110mm Elevated Concrete Slab (permanent framework)	32.80%	43.95%
f- 200mm Precast Concrete Tee Beam/Infill flooring	39.61%	45.43%
g-200mm Hollow Core Precast Concrete flooring	27.42%	<mark>33.37%</mark>

Sources: Data from Table 7.16 expressed in percentage form. Yellow highlighting indicates reference to figures in the discussion in Section 7.4.4.

7.4.2 Potential emission reductions in general Australian wall construction systems

Tables 7.19 and 7.20 present comparative carbon emission reduction and generation figures for general Australian wall construction systems.

Table 7.19: Potential	carbon	emission	(embodied	energy)	reductions	for	general	Australian	wall
construction systems									
						Po	tential Re	duction	

	Standar	d /Basic	ic Potential Reductio			eduction			
General Australian wall construction					n Star		search		
systems	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²	
a-Timber Frame, Single Skin Timber Wall	151	14.8		40.36	3.95		41.36	4.05	
b-Timber Frame, Timber Weatherboard Wall	188	18.4		71.06	6.96		107.01	10.48	
c-Timber Frame, Reconstituted Timber Weatherboard Wall	377	36.9		287.73	28.19		320.03	31.36	
d-Timber Frame, Fiber Cement W/board Wall	169	16.6		35.53	3.48		70.60	6.91	
e-Timber Frame, Steel Clad Wall	336	32.9		114.46	11.21		157.32	15.41	
f-Steel Frame, Steel Clad Wall	425	41.7		143.45	14.05		234.53	22.98	
g-Timber Frame, Aluminium W/board Wall	403	39.5		266.10	26.07		310.03	30.38	
h-Timber Frame, Clay Brick Veneer Wall	561	63.8		19.80	1.94		191.60	18.77	
i-Steel Frame, Clay Brick Veneer Wall	650	63.7		78.72	7.71		154.99	15.18	
j-Timber Frame, Concrete Block Veneer Wall	361	35.4		76.69	7.51		131.95	12.93	
k-Steel Frame, Concrete Block Veneer Wall	453	44.4		121.41	11.89		228.58	22.40	
l-Steel Frame, timber weatherboard Wall	238	23.3		134.82	13.21		222.64	21.81	
m-Cavity Clay Brick Wall	860	84.3		29.15	2.85		340.07	33.32	
n-Cavity Concrete Block Wall	465	45.6		145.15	14.22		256.18	25.10	
o-Single Skin Stabilised Rammed Earth Wall	405	39.7		95.76	9.38		273.72	26.82	
p-Single Skin Aerated Concrete Block(AAC)wa	440	43.1		40.55	3.97		74.10	7.26	
q-Single Skin Cored Concrete Block Wall	317	31.1		56.30	5.51		103.71	10.16	
r-Steel Frame, Compressed Fibre Cement Clad Wall	385	37.7		158.70	15.55		282.34	27.67	
s-Hollow-Core Precast Concrete Wall	729	71.4		187.60	18.38		298.76	28.2	
t-Tilt-up Precast Concrete Wall	818	80.1		224.02	21.95		356.95	34.98	
u-Porcelain-Enamelled Steel Curtain Wall	865	84.8		480.92	47.11		523.09	51.26	
v-Glass Curtain Wall	770	75.5		451.42	44.23		492.09	48.22	
w-Steel Faced Sandwich Panel Wall	1087	106.5		197.05	19.31		218.24	21.38	
x-Aluminium Curtain Wall	935	91.6		722.19	70.77		802.44	78.63	

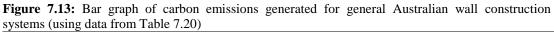
Sources: 'Standard/Basic' column represents construction carbon emissions (embodied energy) from values given in Chapter Four; the 'Green Star' and 'This research' columns are the potential construction carbon emission (embodied energy) reductions as calculated in Appendix C (Tables A.C.71-A.C.118)

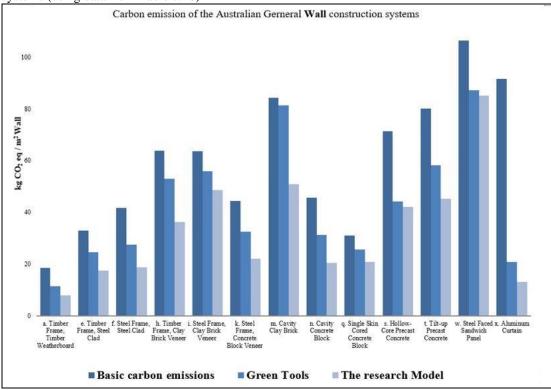
	Standar	rd /Basic
General Australian Wall construction systems	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²
Timber Frame, Single Skin Timber Wall	151	14.8
Timber Frame, Timber Weatherboard Wall	188	18.4
Гіmber Frame, Reconstituted Timber Veatherboard Wall	377	36.9
Timber Frame, Fiber Cement W/board Vall	169	16.6
Timber Frame, Steel Clad Wall	336	32.9
Steel Frame, Steel Clad Wall	425	41.7
'imber Frame, Aluminium W/board /all	403	39.5
Timber Frame, Clay Brick Veneer Wall	561	63.8
teel Frame, Clay Brick Veneer Wall	650	63.7
imber Frame, Concrete Block Veneer Vall	361	35.4
Steel Frame, Concrete Block Veneer Wall	453	44.4
teel Frame, timber weatherboard Wall	238	23.3
avity Clay Brick Wall	860	84.3
avity Concrete Block Wall	465	45.6
Single Skin Stabilised Rammed Earth Vall	405	39.7
Single Skin Aerated Concrete Block(AAC)wall	440	43.1
Single Skin Cored Concrete Block Wall	317	31.1
eel Frame, Compressed Fibre Cement ad Wall	385	37.7
ollow-Core Precast Concrete Wall	729	71.4
lt-up Precast Concrete Wall	818	80.1
orcelain-Enamelled Steel Curtain Wall	865	84.8
lass Curtain Wall	770	75.5
Steel Faced Sandwich Panel Wall	1087	106.5
Aluminium Curtain Wall	935	91.6

 Table 7.20: Carbon emissions (embodied energy) generated in general Australian wall construction systems

Sources: 'Standard/Basic' column is from values given in Chapter Four; the 'Green Star' and 'This Research' columns are the generated construction carbon emissions (embodied energy) obtained from Table 7.20 (subtract reduction figures from standard/basic figures)

The bar graph in Figure 7.13 provides a comparative representation of the generated carbon emissions data for general Australian wall construction systems (as given in Table 7.17).





Source: Generated carbon emissions using data from Table 7.20

Table 7.21 provides a percentage representation of the potential carbon emission reductions that can be achieved in general Australian wall construction systems by application of the Green star and research model tools (using data from Table 7.19).

	Green Star	This research
General Australian wall construction systems	Carbon Emissions Kg/m ²	Carbon Emissions Kg/m ²
a-Timber Frame, Single Skin Timber Wall	26.72%	27.39%
b-Timber Frame, Timber Weatherboard Wall	37.79%	56.92%
c-Timber Frame, Reconstituted Timber Weatherboard Wall	76.32%	84.88%
d-Timber Frame, Fiber Cement W/board Wall	21.02%	41.77%
e-Timber Frame, Steel Clad Wall	34.06%	46.82 %
f-Steel Frame, Steel Clad Wall	33.75%	55.18%
g-Timber Frame, Aluminium W/board Wall	66.02%	76.39%
h-Timber Frame, Clay Brick Veneer Wall	3.52%	34.15%
i-Steel Frame, Clay Brick Veneer Wall	12.11%	23.84%
j-Timber Frame, Concrete Block Veneer Wall	21.24%	36.55%
k-Steel Frame, Concrete Block Veneer Wall	26.80%	50.45%
1-Steel Frame, timber weatherboard Wall	56.64%	<mark>93.54%</mark>
m-Cavity Clay Brick Wall	3.38%	39.54%
n-Cavity Concrete Block Wall	31.23%	55.09%
o-Single Skin Stabilised Rammed Earth Wall	23.64%	67.58%
p-Single Skin Aerated Concrete Block(AAC)wall	9.21%	<mark>16.84%</mark>
q-Single Skin Cored Concrete Block Wall	17.76%	32.71%
r-Steel Frame, Compressed Fibre Cement Clad Wall	41.22%	73.33%
s-Hollow-Core Precast Concrete Wall	25.73%	40.98%
t-Tilt-up Precast Concrete Wall	27.38%	43.63%
u-Porcelain-Enamelled Steel Curtain Wall	55.59%	60.74%
v-Glass Curtain Wall	58.62%	63.90%
w-Steel Faced Sandwich Panel Wall	18.12%	20.07%
x-Aluminium Curtain Wall	72.23%	85.82%

 Table 7.21: Potential carbon emission reductions in general Australian wall construction systems

 expressed as percentages (using data from Table 7.19)

Sources: Data from Table 7.19 expressed in percentage form. Yellow highlighting indicates reference to figures in the discussion in Section 7.4.4.

7.4.3 Potential emission reductions in general Australian roof construction systems

Tables 7.22 and 7.23 present comparative carbon emission reduction and generation figures for general Australian roof construction systems.

Table 7.22: Potential	carbon	emission	(embodied	energy)	r	eductions	for	general	Australian	roof
construction systems										
					- 1					

	Standard /Basic		Potential Reduction				
General Australian roof construction systems			Green Star			This research	
	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²
a-Timber Frame, Timber Shingle Roof	151	14.8	48.45	4.74		68.57	6.71
b-Timber Frame, Fiber Cement Shingle Roof	291	28.5	40.85	4.00		74.10	7.26
c-Timber Frame, Steel Sheet Roof	330	32.3	109.47	10.72		137.32	13.46
d-Steel Frame, Steel Sheet Roof	483	47.3	178.57	17.49		232.29	31.68
e-Timber Frame, Concrete Tile Roof	240	23.5	45.16	4.42		74.10	7.26
f-Steel Frame, Concrete Tile Roof	450	44.1	97.64	9.56		191.49	18.76
g-Timber Frame, Terracotta Tile Roof	271	26.6	45.16	4.42		78.59	7.70
h-Timber Frame, Synthetic Rubber Membrane Roof	386	37.8	45.16	4.42		60.57	5.93
i-Concrete Slab, Synthetic Rubber Membrane Roof	1050	102.9	258.71	25.35		393.11	38.52
j-Steel Frame, Fibre Cement Sheet Roof	337	33	55.44	5.43		149.55	14.65
k-Steel Frame, Steel Sheet Roof (commercial)	401	39.3	145.65	14.27		230.20	22.56

Sources: 'Standard/Basic' column represents construction carbon emissions (embodied energy) from values given in Chapter Four; the 'Green Star' and 'This research' columns are the potential construction carbon emission (embodied energy) reductions as calculated in Appendix C (Tables A.C.119 – A.C.140).

General Australian roof construction systems	Standard /Basic		Green Star			This research		
	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²		Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²	
a-Timber Frame, Timber Shingle Roof	151	14.8	102.55	10.04		82.43	8.08	
b-Timber Frame, Fiber Cement Shingle Roof	291	28.5	250.15	24.51		216.9	21.25	
c-Timber Frame, Steel Sheet Roof	330	32.3	220.53	21.61		192.68	18.88	
d-Steel Frame, Steel Sheet Roof	483	47.3	339.75	33.29		250.71	24.56	
e-Timber Frame, Concrete Tile Roof	240	23.5	194.84	19.09		165.90	16.25	
f-Steel Frame, Concrete Tile Roof	450	44.1	385.68	37.79		291.89	28.60	
g-Timber Frame, Terracotta Tile Roof	271	26.6	225.84	22.13		192.41	18.85	
h-Timber Frame, Synthetic Rubber Membrane Roof	386	37.8	340.84	33.40		325.46	31.89	
i-Concrete Slab, Synthetic Rubber Membrane Roof	1050	102.9	791.29	77.54		656.89	64.37	
j-Steel Frame, Fibre Cement Sheet Roof	337	33	281.56	27.59		187.45	18.37	
k-Steel Frame, Steel Sheet Roof (commercial)	401	39.3	255.35	25.02		170.80	16.73	

Table 7.23: Carbon emissions (embodied energy) generated in general Australian roof construction systems

Sources: 'Standard/Basic' column is from values given in Chapter Four; the 'Green Star' and 'This Research' columns are the generated construction carbon emissions (embodied energy) obtained from Table 7.24 (subtract reduction figures from standard/basic figures)

The bar graph in Figure 7.14 provides a comparative representation of the generated carbon emissions data for general Australian roof systems (as given in Table 7.23).

Carbon emissions of the Austalian General Roof construction systems 120 100 kg CO₂ eq / m² Roof 80 60 40 20 b. Timber c. Timber d. Steel Frame, Fiber Frame, Steel Frame, Steel Cement Sheet Roof Sheet Roof e. Timber Frame , f. Steel Frame, g. Timber Frame, h. Timber Frame, i. Concrete Slab, Synthetic Rubber j. Steel k Frame, Fibre Fran k. Steel Stee name, ncrete Tile Co Roof Timb ncrete Tile Roof Terracotta Tile Roof Synthetic Rubber Cement Sheet Sheet Roof ngle Roof Roof f Shi com Membrane Roof R Standard /Basic The Research Model Green tool

Figure 7.14: Bar graph of carbon emissions generated for general Australian roof construction systems (using data from Table 7.23)

Source: Generated carbon emissions using data from Table 7.23

Table 7.24 provides a percentage representation of the potential carbon emission reductions that can be achieved in general floor construction systems by application of the Green star and research model tools (using data from Table 7.22).

 Table 7.24: Potential carbon emission reductions in general Australian roof construction systems expressed as percentages (using data from Table 7.22)

General Australian roof construction systems	Green Star Carbon emissions	This Research Carbon emissions		
	KgCo ₂ /m ² eq.	KgCo ₂ /m ² eq.		
a-Timber Frame, Timber Shingle Roof	32.08%	45.41%		
b-Timber Frame, Fiber Cement Shingle Roof	14.03%	25.46%		
c-Timber Frame, Steel Sheet Roof	33.17%	41.61%		
d-Steel Frame, Steel Sheet Roof	<mark>36.97%</mark>	48.09%		
e-Timber Frame, Concrete Tile Roof	18.81%	30.87%		
f-Steel Frame, Concrete Tile Roof	21.69%	42.55%		
g-Timber Frame, Terracotta Tile Roof	16.66%	29.00%		
h-Timber Frame, Synthetic Rubber Membrane	<mark>11.69%</mark>	<mark>15.69%</mark>		
i-Concrete Slab, Synthetic Rubber Membrane	24.63%	37.43%		
j-Steel Frame, Fibre Cement Sheet Roof	16.45%	44.37%		
k-Steel Frame, Steel Sheet Roof (commercial)	36.32%	<mark>57.40%</mark>		

Sources: Data from Table 7.22 expressed in percentage form. Yellow highlighting indicates reference to figures in the discussion in Section 7.4.4.

7.4.4 Analysis of data from general Australian floor, wall and roof systems

In respect to general Australian floor construction systems, the bar graph (Figure 7.12) of carbon emissions generated indicates that, following application of the research model to the floor systems, generated carbon emissions are consistently lower in comparison to standard building practice and use of the Green Star tool.

This trend is also seen when percentage carbon reductions are considered for floor systems as in Table 7.18. The potential carbon emission reductions achieved by application of the Green Star tool ranged from 15.56 to 57.55 per cent. In comparison, the potential carbon emission reductions achieved by application of the bioclimatic criteria of the research tool were higher for all floor systems, ranging from 33.37 to 57.55 per cent. Overall, the research model criteria clearly show the greater potential reduction in carbon emissions for Australian floor construction systems.

In respect to general Australian wall construction systems, the bar graph (Figure 7.13) of carbon emissions generated indicates again that the research model consistently produces the lowest emissions. This is confirmed in consideration of percentage emission reductions as shown in Table 7.21, where Green Star emission reductions range from 3.52 to 76.23 per cent, in comparison to application of the research model where the reductions range from 16.84 to 93.54 per cent, and again potential emission reductions are higher for all Australian wall construction systems.

Finally, in the case of general Australian roof construction systems, the bar graph (Figure 7.14) confirms that the carbon emissions generated after application of the research model tool are consistently lower than in the other scenarios (standard/basic building practice and the Green Star tool). This trend is confirmed in reference to the percentage emission reductions in Table 7.24. Reductions for use of the Green Star tool range from 11.69 to 36.97 per cent, in comparison to the research model tool where the range is from 15.60 to 57.40 per cent, and again potential emission reductions are higher for all Australian roof construction systems.

Overall, application of the research model criteria to an Australian floor, wall or roof construction system consistently produces the potential for the lowest carbon

generation, and thus the highest reductions in carbon emissions when compared to standard building practice (standard/basic) or application of the Green Star tool. This is the case for all items considered within general Australian floor, wall and roof construction systems.

7.5 Summary

This chapter has presented and analysed the results of applying the research model's bioclimatic criteria, first, to elements of the floor, wall and roof construction systems of six selected case studies; and, second, to elements of general Australian floor, wall and roof construction systems. The results have been presented for all systems in numerical, graphical and percentage form, and compared to emissions expected in standard building systems, implemented building systems, and from application of the Australian Green Star rating tool.

Analysis of results from all construction systems clearly shows that appropriate application of the bioclimatic criteria of the research model will generally result in reduction of carbon emissions of around 50 to 65 per cent (Table 7.13) in the Case Studies, and 57 to 93 per cent (Tables 7.18, 7.21 and 7.24) in general Australian construction systems, levels which are consistently higher in achievement than current best practice or through use of a green rating tool.

CHAPTER EIGHT CONCLUSIONS BIOCLIMATIC DESIGN PRINCIPLES IN CONSTRUCTION

8.1 Overview

The Australian building sector is reported to be one of the largest contributors to Australian greenhouse gas emissions (McKinsey 2008), and thus has the greatest potential for a significant reduction of greenhouse gases as compared to other major emitting sectors (IPCC 2011). This is now of immediate importance given that the Australian Federal Government has agreed to reduce greenhouse gas emissions 26 to 28 per cent by 2030 (Hasham, Bourke & Cox 2015). The application of bioclimatic design principles within the building life cycle has been explored in this research as one way to achieve this.

This final chapter is divided into six sections. Section 8.1 provides the context for this chapter. Section 8.2 presents a discussion on the significance of this study. Section 8.3 details recommendations for the Australian construction sector following on from this research. Section 8.4 makes recommendations for further research. Section 8.5 discusses the limitations of this research project. Finally, Section 8.6 offers some concluding remarks and brings this thesis to a close.

8.2 Significance of this study

The use of green rating tools such as the Australian Green Star tool to assist in reduction of the carbon emissions from buildings is well known. However, from personal experience of using this tool, I can attest to the fact that the Green Star tool can be applied to only 5 to 10 per cent of a given building under limited conditions. This is because green tools do not assess and apply the range of criteria inherent in bioclimatic design principles and the research model. With the Green Star tool, it may thus not be possible to include evaluation of all the sustainability features present in a given construction project. The sustainability credits offered to the construction industry for use of a green tool rating system for a given project are also limited

The particular significance of this present research lies in the fact that the green tool developed for this project is based on generic bioclimatic sustainability criteria that

can be applied to single cases or all areas of the construction industry and its activities. This research has produced a bioclimatic green tool that can be applied to reducing carbon emissions from any single building element in an Australian construction system independently of their building class or typology. Furthermore, the effectiveness of the developed model tool has been demonstrated in this research.

For whole construction systems, the maximum reductions achieved using the Green Star tool were from 17 to 32 per cent, as compared to the higher reductions achieved in the research model tool of 48 to 65 per cent (Table 7.13). When the research tool is applied to building elements of the floor, wall and roof of general Australian construction systems, reduction in carbon emissions ranged from 57 to 93 per cent (Tables 7.18, 7.21 and 7.24). However, a more significant finding is that application of the research tool to these elements of general construction systems consistently achieved significantly higher reductions in carbon emissions than in current building practice or through application of a currently-used green rating system (i.e. Green Star tool) to building elements (Tables 7.18, 7.21 and 7.24).

The significance of this study thus lies in the fact that it clearly demonstrates that consideration of bioclimatic principles in construction projects has potential to significantly reduce the environmental impact of the construction process. Reduction of construction carbon emissions is becoming of vital importance if an ecologically healthy environment based on a program of sustainability and sustainable development is to be achieved in Australia and elsewhere.

8.3 Recommendations for the Australian construction sector based on this research

Consideration of bioclimatic design principles in the construction industry must be of high priority in order to reduce carbon emissions resulting from the building construction process. Research needs to be funded and commenced on how these principles can best be implemented, as has been done in the United Kingdom (Allwood et al. 2012; UK Indemand 2014) and Germany (World Federation of Engineering Organizations 2011). It is also important to establish criteria that would allow for grant of credits where use of environmental assessment tools is incorporated into the building design process.

Reuse and recycling of construction and demolition materials also needs to be facilitated and mandated through legislation. Related to this, there also needs to be the creation and expansion of a warehouse of parts, reuse markets, and construction guidelines, as well as the expansion of deconstruction techniques, machinery and facilities (Bales 2008; Steel Construction Information 2014). This would increase the use of recycled construction materials, and reduce the impact of transportation. If such were established in the Australian context, this would significantly reduce embodied energy and carbon emissions in the building sector, and assist the Federal Government in their aim to reduce the total carbon emissions generated by Australian society.

8.4 Recommendations for further research

The green model developed for this research considers only the main elements of the buildings in the case studies and general Australian construction systems (i.e. floors, walls and roofs), and then only within the first three stages of the building lifecycle. Extension of this research to include calculation of embodied energies and potential carbon emission reductions for all building elements in construction (e.g. finishing, stairs, windows, doors) needs to be performed. Additionally, this future research should encompass the entire building lifecycle.

The use of 3D digital modelling in BIM (Eastman et al. 2011), with other software such as IMPACT (eToolLCD 2015) and Tally (EPD-Tally 2008), are able to collate and analyse data through applications such as AutoCAD or Revit (Eastman et al. 2011). Such applications have been used in environmental assessment, materials selection, and calculation of embodied energies and potential carbon emission reduction levels. Furthermore, such software can be used for sustainability assessment at any point during the building life cycle. Overall, use of such software facilitates a more integrated materials selection, design and construction process management that results in better quality and more sustainable buildings with lower carbon emissions, and even has potential to reduce the project duration (Drogemuller 2009; Jalaei & Jrade 2014).

Extension of this research can thus most easily be achieved through use of software tools such as these. This will remove the limitations of the current research model,

and facilitate the application of bioclimatic design principles to any Australian construction project.

8.5 Limitations of this research

As noted, the model in this present study has been applied only to the main building elements in the first three stages of the building lifecycle. In the next stage of this research, Building Information Modelling (BIM) or other software will be used. This will allow for calculation of embodied energy and relevant construction carbon emissions throughout the building lifecycle, and for all elements of the building concerned. It will then be possible for the research model to be applied to any case study with any classification in any location in Australia.

The Process Energy Requirement (PER) method was used to calculate embodied energies in this research. An alternative calculation technique for embodied energies is the Input-Output method which is based on the sum of all energy inputs into a product system through all stages of the life cycle (Lawson 2006). However, calculations using the Input-Output method produce figures for embodied energy that are two to three times higher than the PER method. Such discrepancies will be solved through the use of Building Information Modelling and other software.

Typical embodied energy units are measured using MJ/kg (megajoules of energy needed to make a kilogram of product), and these have to be converted to equivalent kilograms of carbon emissions. However, such conversion is not straightforward because different types of energy (oil, wind, solar, etc.) emit different amounts of carbon dioxide, thus the actual amount of carbon dioxide emitted when a product is made will depend on the type of energy used in the manufacturing process. To facilitate this conversion, the standard Australian Government equation (1 MJ = 0.098 kgCO_2) has been used to convert embodied energy to equivalent carbon emissions.

This study proposes geopolymer cement as a replacement for Portland cement for structural and non-structural building purposes. Geopolymer cement was chosen as the cement for reference in this thesis rather than other green cements for two reasons. First, while there are other options available, geopolymer cement is currently by far the most common and widely used green cement in Australian construction, and its use is increasing. Second, geopolymer cement emerged in the literature review as the most appropriate green cement to consider from the viewpoint of reducing carbon emissions of construction.

In respect to this, when used as a replacement for Portland cement, geopolymer cement produces a range of potentially high reductions in carbon emissions (75 to 90 per cent). This is because GC can be slag-based, rock-based or fly-ash-based. Geopolymer cements made from fly ash or granulated blast furnace slag require less sodium silicate solution in order to be activated. They consequently have a lower environmental impact than geopolymer concrete made from metakaolin rock (i.e. rock-based geopolymer cement). However, the type of geopolymer cement that might be used to replace Portland cement in building construction ultimately depends on the particular type available in the area concerned (Habert, d'Espinose de Lacaillerie & Roussel 2011). In turn, this will affect the outcomes where the research model is used, and this must be taken into account when the research model is applied.

8.6 Concluding Remarks

Our world is changing, and our construction industry needs to adapt to these changes. The Australian building sector has the largest potential for achieving a significant reduction in greenhouse gas emissions. This could be through the simple application of bioclimatic design and construction principles.

The outcomes of this research demonstrate that use of bioclimatic criteria can achieve reductions in carbon emissions from 48 to 65 per cent for whole building systems (Table 7.13), and from 57 to 93 per cent when applied to building elements of general Australian construction systems (Tables, 7.18, 7.21 and 7.24). However, a more significant finding is that application of the research tool to elements of general Australian construction systems consistently achieved significantly higher reductions in carbon emissions than in current building practice, or through application of a currently-used green rating system (i.e. Green Star tool) to building elements. The future of the green construction industry should thus include consideration of bioclimatic design principles.

The UK government has funded the UK-Indemand plan to achieve an 80 per cent reduction in construction carbon emissions by 2050. This is considered as an achievable target providing that future design and construction of buildings take into account bioclimatic principles and criteria (Allwood et al. 2012). If the Australian construction sector is to follow this lead, then some form of Australian Indemand scheme has to be funded and established. The outcomes of this research based on bioclimatic design support this proposal. Such a scheme would enable the government to achieve significant reductions in greenhouse gas emissions, and thus to reduce the impact of the building sector on the Australian environment.

Current green tool rating systems are voluntary, do not apply the range of bioclimatic criteria inherent in the research model, and can be used only in 5 to 10 per cent of buildings. Full development of the research model will allow for its application to all building elements throughout the building lifecycle, and to any construction project of any classification in any location in Australia.

One of the main objectives of this study is to assist the Australian Federal Government to meet the agreed targets from the 2015 Paris conference. Reducing the carbon emissions of the building sector is one of the most cost-effective ways of doing this. The application of green criteria and bioclimatic principles in building design and construction is currently not mandatory for the Australian construction sector, and thus sustainable practice is not routinely followed in this country. This must change if the Australian Federal Government are serious about meeting their carbon emission reduction targets of 26 to 28 per cent by 2030.

In concluding this thesis, I would like to mention a quote attributed to the famous physicist, Albert Einstein:

Problems cannot be solved at the same level of awareness that created them (Albert Einstein)

For the last century, humankind has had an increasingly negative impact on the resources and environment of this planet through unsustainable population growth and development, seemingly without great awareness of the problems we are now facing. Urgent measures are now required to address these environmental and other problems.

Awareness of bioclimatic principles in building design to reduce carbon emissions may provide a small step along the way to achieving sustainable construction as part of the solution to our global problems.

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PAPERS AND BOOK CHAPTERS FROM THIS RESEARCH

Papers published as a consequence of this research have received much attention – for example, Sattary and Thorpe (2016) has received the highest read rating for the University of Southern Queensland (USQ) papers on the ResearchGate website.

The following papers and book chapters have been published as a result of research relating to this thesis.

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Sustainable Construction

APPENDICES

Potential Carbon Emissions Reduction (PCER) in Australian Construction Systems through the Use of Bioclimatic Design Principles

A Thesis submitted by

Sattar Sattary

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APPENDIX D

DATA RELATING TO CHAPTER FIVE

APPENDIX A

DATA RELATING TO CHAPTERS TWO, THREE AND FOUR

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The Canadian common Building	Standard/Basic	Embodied Energy
Materials	MJ/kg	MJ/m ³
Aggregate	0.10	150
Straw bale	0.24	31
Soil-cement	0.42	819
Stone (local)	0.79	2030
Concrete block	0.94	2350
Concrete (30 Mpa)	1.3	3180
Concrete precast	2.0	2780
Lumber	2.5	1380
Brick	2.5	5170
Cellulose insulation	3.3	112
Gypsum wallboard	6.1	5890
Particle board	8.0	4400
Aluminium (recycled)	8.1	21870
Steel (recycled)	8.9	37210
Shingles (asphalt)	9.0	4930
Plywood	10.4	5720
Mineral wool insulation	14.6	139
Glass	15.9	37550
Fiberglass insulation	30.3	970
Steel	32.0	251200
Zinc	51.0	371280
Brass	62.0	519560
PVC	70.0	93620
Copper	70.6	631164
Paint	93.3	117500
Linoleum	116	150930
Polystyrene insulation	117	3770
Carpet (synthetic)	148	84900
Aluminium	227	515700

Table A.A.1: Embodied energy of common Canadian building materials)

Source: Canadian Architects (2015)

Australian Building Materials	Standard/Basic Embodied Energy MJ/kg	Standard/ Basic Carbon Emissions per Kg/MJ
Kiln dried sawn softwood	3.4	0.333
Kiln dried sawn hardwood	2.0	0.196
Air dried sawn hardwood	0.5	0.049
Hardboard	24.2	2.372
Particleboard	8.0	0.784
MDF	11.3	1.107
Plywood	10.4	1.019
Glue-laminated timber	11.0	1.078
Laminated veneer lumber	11.0	1.078
Plastics – general	90.0	8.820
PVC	80.0	7.840
Synthetic rubber	110.0	10.780
Acrylic paint	61.5	6.027
Stabilized earth	0.7	0.069
Imported dimension granite	13.9	1.362
Local dimension granite	5.9	0.578
Gypsum plaster	2.9	0.284
Plasterboard	4.4	0.431
Fiber cement	4.8	0.470
Cement	5.6, 5.4 ¹	$0.549, 0.82^{1}$
In situ concrete	1.9	0.186
Precast steam-cured concrete	2.0	0.196
Precast tilt-up concrete	1.9	0.186
Clay bricks	2.5	0.245
Concrete blocks	1.5	0.147
AAC	3.6	0.353
Glass	12.7, 12.8 ¹	$1.245, 1.5^{1}$
Aluminium	170	16.660
Copper	100	9.800
Galvanized steel	38	3.724
Steel	341	AU 3.33, AU 2 ¹

Table A.A.2: Embodied energy and carbon emissions of common Australian building materials

Source: Superscript data – 1: from Lawson (1996); remaining figures are from Lawson (2006); and Sattary and Cole (2012)

Common Building Materials	Standard/Basic Embodied Energy MJ/kg	Standard/ Basic Carbon Emissions per Kg/MJ
Aggregate	0.083	0.0048
Concrete (1:1.5:3)	1.11	0.159
Bricks (common)	3	0.24
Concrete block (Medium density)	0.67	0.073
Aerated block	3.5	0.3
Limestone block	0.85	
Stone	-	0.1^{1}
Marble	2	0.116
Cement mortar (1:3)	1.33	0.208
Cement	-	1.0^{1}
Steel (general, av. recycled content)	20.1	1.37
Steel	-	2.7
Stainless steel	56.7	6.15
Timber (general, excludes sequestration)	8.5	0.46
Timber		0.30 ¹
Glue laminated timber	12	0.87
Cellulose insulation (loose fill)	0.94–3.3	
Cork insulation	26	
Glass fibre insulation (glass wool)	28	1.35
Flax insulation	39.5	1.55
Rockwool (slab)	16.8	1.05
Expanded Polystyrene insulation	88.6	2.55
Polyurethane insulation (rigid foam)	101.5	3.48
Plastic	-	1.9 ¹
Wool (recycled) insulation	20.9	1.7
Straw bale	0.91	0.1^{1}
	37	2.7
Mineral fibre roofing tile		
Slate	0.1–1.0	0.006-0.058
Clay tile	6.5	0.45
Aluminium (general & incl 33% recycled)	155	8.24
Aluminium	-	11.51
Bitumen (general)	51	0.38-0.43
Medium-density fibreboard	11	0.72
Plywood	15	1.07
Plasterboard	6.75	0.38
Gypsum plaster	1.8	0.12
Glass	15	0.85
Fiber glass	-	8.11
PVC (general)	77.2	2.41
Vinyl flooring	65.64	2.92
Terrazzo tiles	1.4	0.12
Ceramic tiles	12	0.74
Wool carpet	106	5.53
Wallpaper	36.4	1.93
Vitrified clay pipe (DN 500)	7.9	0.52
Iron (general)	25	1.91
Copper (average incl. 37% recycled)	42	2.6
Brass	-	4.5 ¹
Lead (incl 61% recycled)	25.21	1.57
Lead	-	3.21
Zinc		2.91
Ceramic sanitary ware	29	1.51
Paint - Water-borne	59	2.12
Paint - Solvent-borne	97	3.13
Photovoltaic (PV) Cells Type	Energy MJ per m ²	Carbon kg CO ₂ per m ²
Monocrystalline (average)	4750	242
Polycrystalline (average)	4730	242
· · · · ·		
Thin film (average)	1305	67

Table A.A.3: Embodied energy in common building materials

Source: Superscript data – 1: Wilson (2015); remaining figures are from the Inventory of Carbon & Energy (2011); and the Institution of Civil Engineers (Bull 2012).

Building Materials in AU, UK and CA	Standard/Basic Embodied Energy MJ/kg	Standard/ Basic Carbon Emissions per Kg/MJ	Standard/Basic Embodied Energy MJ/kg	Standard/ Basic Carbon Emissions per Kg/MJ	
	From Raw materials, V	irgin natural resources	ources From recycled materials and recycled		
Aggregate	AU, CA 0.1 UK 0.083	CA 0.009 ² UK 0.0048 ¹			
Kiln dried sawn softwood	3.4	0.333			
Kiln dried sawn hardwood	2.0	0.196			
Air dried sawn hardwood	0.5	0.049			
Hardboard	24.2	2.372			
Paper	36.4		23.4		
Particleboard	8.0	0.784			
MDF	11.3	1.107			
Plywood	10.4	1.019			
Glue-laminated timber	11.0	1.078			
Laminated veneer lumbe	11.0	1.078			
PVC	US 65, AU 80.0	7.840	US 29, AU		
Synthetic rubber	110.0	10.780			
Acrylic paint	61.5	6.027			
Stabilized earth	0.7	0.069			
Imported dimension granite	13.9	1.362			
Local dimension granite	5.9	0.578			
Gypsum plaster	2.9	0.284			
Plasterboard	4.4	0.431			
Fiber cement	4.8*	0.470			
Cement	5.6	0.549			
In situ concrete	1.9	0.186			
Precast steam-cured concrete	2.0	0.196			
Precast tilt-up concrete	1.9	0.186			
Clay bricks	AU 2.5, UK 3	AU 0.245, UK 0.24			
Concrete block	AU 1.5, UK 0.67	AU 0.147, UK 0.073			
AAC	3.6	0.353			
	AU12.7, UK15, AU 15.6 ³		12.5 ³		
Plastics – general	AU 90, AU 98 ³	8.820	AU 12, AU12 ³		
Polyethylene	US 98, AU 103	0.020	US 56, AU -		
Polyester	53.7		05 50, A0 -		
Polypropylene expanded					
Aluminium	US 196, AU 170, AU 191 ³	AU 16.660, UK 11.5 ⁴	US 27, AU 8.1, AU8.1 ³ CA 8.1, UK 155	UK8.25 (33%recycled)	
Copper	AU100	AU9.800	UK 42 (average incl. 37% recycled)	UK 2.6 (average incl. 37% recycled)	
Steel	AU 32 ³ , US40, CA32	UK2.7 ⁴	AU 10.1 ³ , US 18, CA8.9	CA0.872	
Steel (general - average recycled content)	AU 32 ³ , US40, CA32		UK 20.7	UK 1.37	
Steel (section - average recycled content)	AU 32 ³ , US40, CA32		UK 21.5	UK 1.42	
Steel (pipe-average recycled content)	AU 32 ³ , US40, CA32		UK 19.8	UK 1.37	
Galvanized Steel	AU38	3.724	AU 10.1		
Stainless Steel	UK 56.7	UK 6.15			

|--|

Sources: Superscript data – 1: Greenspec (2015); 2: Canadian Architects (2015); 3: O'Halloran, Fisher and Rab (2008); 4: Institution of Civil Engineers (Bull 2012).

Remaining Australian data from Lawson (1996; 2006), and O'Halloran, Fisher and Rab (2008); US data from Jong and Rigdon (1998); and Canadian data from Canadian Architects (2015).

LEED NC	US Green Building Council	Concrete Roof Tile	Points
Category	Requirements		
Local Heat I	sland Effects LEED for Homes		
SS 3	Material with a solar reflectance (SRI)	Roof Tile offers product with SRI >	1
	> 29	29	
Energy Perfo	ormance		
EA 1	Improve the overall energy performance of a home by meeting or exceeding the performance of an ENERGY STAR labelled home	Roof Tiles with SRI > 29 help to reduce cooling loads in homes	Up to 4
Environment	ally Preferable Products		
MR 2	Local production. Use products that were extracted, processed and manufactured within 500 miles of the home	Roof tile manufacturers can provide information to identify production facilities within 500 miles of a project.	1/2
Environment	ally Preferable Products		

Table A.A.5: LEED Points for concrete roof tiles

Source: Hanson Roof Tiles (LEED 2014)

Table A.A.5: LEED credits for reuse of roof tiles

Use recycled roof tiles, 92 MJ/m² x 13% (LEED 2014) = 11.96 MJ/m² Use recycled roof tiles (Herbudiman & Saptaji 2013) from 45% recycled content Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg (Greenspec 2015) x (44 concrete – 6.16 cement) Kg/m² (Lawson 1996, p.134) x 45% = 0.083 x 37.84 kg/m2 x 50% (Herbudiman & Saptaji 2014) =1.57 MJ/m² Therefore, total released carbon from concrete roof tile (Lawson 1996, p. 127) is 240 MJ/m² x 0.098 kg CO₂ = 23.52 Kg CO₂/m² The reduced carbon emission from use of recycled concrete roofs: 1.57 MJ/m² x 0.098 kg CO₂ = 0.15 Kg CO₂/m²

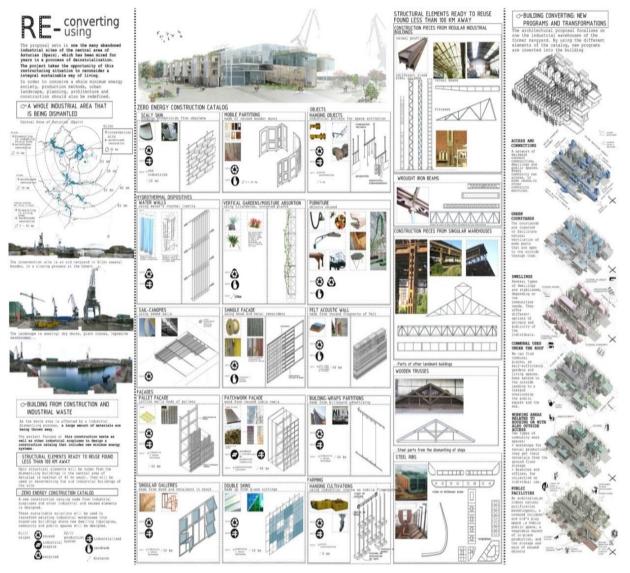


Figure A.A.1: Reuse strategy: Catalogue of construction systems made of reused materials

Source: Holcim (2011).

Table A.A.6: Replacement 40% Portland cement with geopolymer cement: carbon emissions for a one square metre of 125 mm elevated concrete floor

300kg/m² concrete (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) = 42 kg replaced cement/ m² in concrete; therefore the reduced embodied energy will be:

42 kg Cement/m² x 5.6 MJ/kg (Lawson 1996, p. 13) x 40% = 94.08 MJ/m²

Generated carbon emission 1 MJ = 0.098 kg CO₂ (CSIRO 2014)

Therefore, the total reduced carbon emission of 125 mm elevated concrete floor will be: $94.08MJ/m^2 \times 0.098 \text{ kg CO}_2 = 9.21 \text{ Kg CO}_2/m^2$

Total carbon emission of 125 mm elevated concrete floor will be: 497 MJ/m² x 0.098 kg $CO_2 = 48.7$ Kg CO_2 /m².

Table A.A.7: Full replacement of Portland cement with geopolymer cement: carbon emissions for one square metre of 125 mm elevated concrete floor

300kg/m² concrete (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) = 42 kg replaced cement/ m² in concrete; therefore the reduced embodied energy will be:

42 kg Cement/m² x 5.6 MJ/kg (Lawson 1996, p. 13) = 235.2 MJ/m²

Generated carbon emission $1 \text{ MJ} = 0.098 \text{ kg CO}_2$ (CSIRO 2014)

Therefore, total reduced carbon emission of 125 mm elevated concrete will be: $235.2MJ/m^2 \times 0.098 \text{ kg CO}_2 = 23.04 \text{ Kg CO}_2 /m^2$

The total carbon emission of 125 mm elevated concrete floor will be: 497 MJ/m² x 0.098 kg $CO_2 = 48.7 \text{ KgCo}_2/\text{m}^2$.

Table A.A.8: Full replacement of Portland cement with geopolymer concrete: carbon

 emissions for a one square metre 200 mm concrete slab on ground floor

381 kg/m² (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/ m^2 in concrete

51.73 kg Cement/m² x 5.6 MJ/kg (Lawson 1996, p.13) = 289.74 MJ/m² Reduced Embodied Energy

289.74 MJ/ m² Reduced Embodied Energy

594 MJ/ m^2 Total Embodied Energy of the 200mm Concrete Slab (Lawson 1996, p. 125)

Embodied energy 1 MJ = 0.098 kg CO_2) Generated carbon emission (CSIRO 2014)

The total carbon emission of 200 mm concrete slab floor will be: $594MJ/m^2 x = 0.098 \text{ kg CO}_2 = 58.12 \text{ Kg CO}_2/m^2$

Therefore, total reduced carbon emission of 200 mm concrete slab floor will be: $289.74 \text{ MJ/m}^2 \times 0.098 \text{ kg CO}_2 = 28.39 \text{ Kg CO}_2/\text{m}^2 - \text{shows } 48.84\%$ reduction in the generated carbon emissions of 200mm concrete slab on ground floor

Table A.A.9: Reduced carbon emissions in concrete block with full replacement by geopolymer cement

Geopolymer based cement = 89Kgs/tonne (CBA 2013) / 1000 x 275 = 24.47 Kg/ m² reduced Portland cement in concrete block

Reduced cement 24.47 Kg/ m² x 5.6 MJ/kg (Lawson 1996, p. 13) = 137.03 MJ/ m² reduced embodied energy

Embodied energy 1 MJ = 0.098 kg CO₂ Generated carbon emission (CSIRO 2014)

Embodied Energy of the concrete Block with Portland cement 385 MJ/m²

Reduced carbon emissions $137.03 \text{ MJ}/\text{m}^2$

Generated carbon emissions of the concrete block with Portland cement is 385 MJ/m^2 (Lawson 1996, p. 129) x 0.098 kg CO₂ = 37.73 Kgs CO₂/m²

Reduced carbon emissions by replacing Portland cement with geopolymer cement is 137.03 MJ/ $m^2 x 0.098 \text{ kg CO}_2 = 14.45 \text{ Kgs CO}_2/m^2$

That shows 38.29 per cent reduction in carbon emissions.

Table A.A.10: Reduced transportation emissions for each square metre of 200 mm concrete slab from recycled aggregate

Reuse aggregate (275 concrete – 24.47 cement) kg.m²/1000 T/m² x 100 km x 4.5 – $\{(0.6 + 0.25) / 2\}$ MJtonne/km (Lawson 1996, p. 12) = 102.09 MJ/m²

Generated carbon emission $1 \text{ MJ} = 0.098 \text{ kg CO}_2$ (CSIRO 2014)

Reduced carbon emission is: 102.09 MJ/ $m^2 x 0.098 \text{ kg CO}_2 = 10.00 \text{ Kgs CO}_2/m^2$

The Standard/Basic carbon emission by truck is:

Reuse aggregate (275 concrete – 24.47 cement) kg/m² /1000 T/m² x 100 km x 4.5 MJ/ton/km (Lawson p. 12) = 112.73 MJ/ m²

139.01 MJ/ $m^2 x 0.098 \text{ kg CO}_2 = 11.04 \text{ Kgs CO}_2/m^2$

Table A.A.11: Emission reduction in transportation by decreasing steel use in design(London Olympics stadium roof, Case Study 5)

9.33 kg/m² steel (Lawson 1996, p. 135) /1000 T/m² x 100 km x 4.5 MJtonne/km (Lawson 1996, p. 12) x 90% = 3.77 MJ/m² decreased embodied Energy

Generated carbon emission 1 MJ = 0.098 kg CO₂ (CSIRO 2014)

 $3.77 \text{ MJ/m}^2 \text{ x } 0.098 \text{ kg } \text{CO}_2 = 0.37 \text{ Kgs } \text{CO}_2/\text{m}^2$

Embodied Energy of the roof is 282 MJ/ m² (Lawson 1996, p. 129)

Generated carbon emissions from the roof is 401 MJ/ $m^2\,x$ 0.098 kg CO_2 = 39.3 Kgs CO_2/m^2

Table A.A.12: Reduced carbon emissions in transportation from reuse of one squaremetre of 200 mm concrete slab floor's aggregates (Case Study 5)

Reduced embodied energy in transportation

 $(297 + 5.148 + 84) = 386.14 \text{ kg/m}^2$

386.14 kg/m²/1000 T/m² x 100 km x {4.5 – (0.6 +0.25) /2} MJ/ton/km (Lawson 1996, p. 12) = 125.87 MJ/ m²

Generated carbon emission $1 \text{ MJ} = 0.098 \text{ kg CO}_2$ (CSIRO 2014)

The reduced carbon emission is:

125.87 MJ/ $m^2 x 0.098 \text{ kg CO}_2 = 12.33 \text{ Kgs CO}_2/m^2$

The Standard/Basic carbon emission by truck is:

386.14 kg/m² /1000 T/m² x 100 km x 4.5 MJ/ton/km (Lawson 1996, p. 12) = 139.01 MJ/ m²

139.01 MJ/ $m^2 x 0.098 \text{ kg CO}_2 = 13.62 \text{ Kgs CO}_2/m^2$

Table A.A.13: Reduced carbon emissions in transportation (carried by ship or rail) from reuse of one square metre of concrete block wall materials

Reduced embodied energy in transportation:

Reuse aggregate (275 concrete – 24.47 cement) kg.m²/1000 T/m² x 100 km x 4.5 – $\{(0.6 + 0.25) / 2\}$ MJtonne/km (Lawson 1996, p. 12) = 102.09 MJ/m²

Generated carbon emission $1 \text{ MJ} = 0.098 \text{ kg CO}_2$ (CSIRO 2014)

Reduced carbon emission is: 102.09 MJ/ $m^2 x 0.098 \text{ kg CO}_2 = 10.00 \text{ Kgs CO}_2/m^2$

The Standard/Basic carbon emission by truck is:

Reuse aggregate (275 concrete – 24.47 cement) kg/m² /1000 T/m² x 100 km x 4.5 MJ/ton/km (Lawson 1996, p. 12) = 112.73 MJ/ m²

139.01 MJ/ m² x 0.098 kg CO₂ = 11.04 Kgs CO₂/m²

APPENDIX B

DATA RELATING TO CHAPTER FIVE

Table A.B.1: Te	chnical guide – F	Potential embodied energy	reductions in building	life cycle

Building Life	Stage I, II	Stage III	Stage IV	Stage V
Cycle Stages	Pre- Construction	Construction	Post-Construction	Demolition
Bioclimatic criteria	Produce, reprocess, assemble and re-assemble	Construct, retrofit and reuse	Repair, maintain, refurbish and retrofit	Demolish, deconstruct and recycle
Reduce, save and replace energy use in extraction and Production of Building materials	Reduce, save and replace energy use in building by using renewable materials - Use organic materials - Reprocess materials and elements - Use recycled materials	Reduce, save and replace energy use in buildings by: Reusing building materials Using organic materials Retreating materials Repairing materials Using recycled materials Using materials with recycled content Recycling waste materials	Reduce, save and replace energy use in building by: - Reusing building materials - Reconditioning buildings - Retrofitting and repairing (reusing, retreating, repairing, recycling materials) - Recycling construction waste	 Reduce, save and replace energy use in building by using easily- demolished systems Using deconstructible systems Use fully recyclable materials
Reduce, save and replace energy use in Implementation	reduce energy use in	 Save and reduce energy use in construction processes, reusing Replaced renewable energy in production processes, reusing 	 Save and reduce energy use in repair, maintenance, refurbishment, retrofitting Replace renewable energy in repair, maintenance, refurbishment and retrofitting 	 Save and reduce energy use in demolishing, deconstructing and recycling Replace renewable energy in demolishing, deconstructing and recycling
Reduce, save and replace energy use in Transportation	 Save and reduce energy use in transportation of materials and elements Replace renewable energy in transportation of materials and elements 	 Save and reduce energy use in transportation of construction processes by using locally resourced materials, local professionals Replace renewable energy in transportation by using materials carried with renewable energy 	 Save and reduce energy use in transportation of repair, maintenance, refurbishment and retrofitting Replace renewable energy in transportation for repair, maintenance, refurbishment and retrofitting 	 Save and reduce energy use in transportation for demolishing, deconstructing and recycling Replace renewable energy in transportation for demolishing, deconstructing and recycling

Building Life	Stage I, II	Stage III	Stage IV	Stage V
Cycle Stages	Pre- Construction	Construction	Post-Construction	Demolition
Bioclimatic criteria	Produce, reprocess, assemble and reassemble	Construct, retrofit and reuse	Repair, maintain, refurbish and retrofit	Demolish, recycle and deconstruct
Measurable energy that can be reduced and saved in extraction and Production of Building materials	embodied energy by	 Saved and reduced embodied energy by: Reusing buildings Reusing materials and elements Retreating & repairing materials Using recycled material Using material with recycled content Using fully recycled materials Ising recycled materials 	Saved and reduced embodied energy by: - Reusing buildings - Reusing material - Reconditioning, repairing and retrofitting (reusing, retreat, repair, recycled material)	Saved and reduced embodied energy by: - Using de- constructible elements and building materials - Using recyclable materials
Measurable energy that can be replaced and saved in Implementation	 Saved and reduced energy use in production processes Replaced renewable energy in production processes 	Saved and reduced energy use in construction processes by; - Reusing building, spaces, elements, materials - Replaced renewable energy in construction processes	Saved and reduced energy use in repair, maintenance, refurbishment and retrofitting processes - Replaced renewable energy in repair, maintenance	 Saved and reduced energy use in demolition processes Replaced renewable energy in demolition processes
Measurable energy that can be replaced and saved in Transportation	 Saved and reduced energy use in transportation, and production processes Replaced renewable energy in transportation of materials 	 Saved and reduced energy use in transportation and construction processes Reused buildings, spaces, elements, materials Replaced renewable energy in transportation and construction processes Reused buildings, spaces, elements, materials 	 Saved and reduced energy use in transportation of production processes Reused building, spaces, elements, materials Replaced renewable energy in transportation 	 Saved and reduced energy use in transportation for demolition processes Replaced renewable energy in transportation

 Table A.B.2: Measurable indicators – Potential embodied energy that can be saved during building lifecycle

Table A.B.3: Credits in LEED

Credit 1 - Building Reuse

The intent of this credit is to extend the life cycle of existing building stock, conserve resources, retain cultural resources, reduce waste and reduce the environmental impacts of new buildings.

Credit 1.1 awards one point for 75 per cent reuse of existing walls, floors and roof. Credit 1.2 gives one additional point for maintaining 100 per cent of the existing walls, floors and roof.

Changes proposed for LEED version 2.2 lower these thresholds to 40 per cent and 80 percent, respectively, making it easier to qualify.

Credit 1.3 awards one additional point for the reuse of 50% of interior non-structural elements. Non-structural masonry walls and floors can contribute to this point.

Credit 2 - Construction Waste Management

The intent of this credit is to divert construction, demolition and land clearing debris from landfill disposal. Scraps and broken pieces of concrete masonry can be crushed and used for aggregate or fill. Clay brick scraps can be crushed and used for landscaping as brick chips. Intact, unused masonry units can be saved to use on another project, or donated to Habitat for Humanity or other charitable organizations. One point is awarded for the diversion of 50 per cent of the construction, demolition and land clearing waste (Credit 2.1). One additional point is awarded for diverting 75 per cent (Credit 2.2). Calculations can be done on a weight or volume basis.

Credit 3 - Resource Reuse

This credit is intended for the reuse of salvaged materials and products to reduce the demand for virgin products. Materials salvaged on site do not apply to this credit, but do count toward Credit 1 — Building Reuse. Masonry materials such as brick can be salvaged, but the Brick Industry Association warns against their use. Used brick may not meet the requirements of present-day specifications and may not bond properly. Paver brick that is salvaged and used for interior applications on a new building meet the intent of this credit. Up to two points can be earned for the use of salvaged building materials for 5 and 10 per cent of building materials (Credits 3.1 and 3.2).

Credit 4 - Recycled Content

This credit is intended to increase demand for building products that incorporate recycled content materials, therefore reducing the impacts resulting from extraction and processing of new and virgin materials. This credit award up to two points for using building products that incorporate recycled content materials. Because of the inert nature of masonry products, they are ideal candidates for incorporating recycled materials. The requirement for one point is that materials with the sum of post-consumer recycled content plus half the post-industrial content constitutes at least 5 per cent of the total value of materials in the project (Credit 4.1). If the sum of post-consumer recycled content plus half the post-industrial content equals 10% or more,

one additional point is awarded (Credit 4.2).

Concrete masonry units often incorporate recycled materials. According to the NCMA, supplementary cementitious materials such as fly ash, silica fume and slag cement are considered post-industrial materials. Concrete masonry that incorporates recycled concrete masonry, glass, slag or other recycled materials such as aggregate qualify as post-consumer.

Clay brick often incorporates recycled brick ground and used as grog (i.e. crushed unglazed pottery or brick used as an additive in plaster or clay). If reclaimed from a job site, this material can qualify as post-consumer recycled content. Some manufacturers use bottom ash, a post-industrial waste, for 10 to 12 per cent (by weight) of the clay body. Other post-industrial materials used include fly ash and even sludge. Because of the inert properties of brick, even contaminated soil and sawdust is used. One company uses waste from a nearby ceramic white ware manufacturer as grog.

Mortar may contain recycled materials such as fly ash. Steel reinforcing bars used in reinforced masonry may contain post-consumer or post-industrial materials.

Credit 5 - Regional Materials

This credit encourages the use of building materials that are extracted and manufactured within the region, thereby supporting the regional economy and reducing the environmental impacts resulting from transportation. Masonry products can contribute up to one point when 20 per cent of the building materials and products are manufactured within a 500-mile radius of the project site (Credit 5.1). One additional point is earned if the regionally manufactured materials use a minimum of 50 per cent of building materials that are extracted, harvested or recovered within 500 miles of the project site (Credit 5.2). Changes to the specifics of this credit are proposed for LEED 2.2 (Subasic 2016).

Sample of the research model developed for assessment of potential construction carbon emissions reduction

The research model developed reviews six case studies from Australia and the United Kingdom. The selected case studies and their construction systems represent the general construction systems used in Australia as identified by Lawson (1996). These can include any project from any classification (residential, public, and commercial). For example, the first three case studies are taken from a paper written by Lawson (1996) – all details and information for these are provided, together with embodied energy and implemented embodied energy (Lawson 1996). The fourth and sixth case studies focus on buildings recently completed on the Springfield campus of the University of Southern Queensland (USQ). All drawings and detailed information were accessible. The Olympic Velodrome Building from the London Olympics in 2012 is the focus of the fifth case study – these Olympics achieved high sustainability levels from a range of different environmental tools (e.g. CEEQUAL, ISCA, and BREEAM).

Figure <number></number>	Bioclimatic Conditions		
	Reuse, recycle, materials resources, suppliers and		
	transport		
	Recycled		
	aggregates in		
	material production		
	Steel from recycled		
	contents		
	Reduce material		
	use in design		
	Reuse construction		
Location:	materials		
Floor construction system	Geopolymer, fly ash		
U	and cement		
	substitute		
Wall construction system	Transportation		
	reduction by reuse,		
	recycle sustainable		
	transportation mode		
Doof construction system	Material resources		
Roof construction system			
Principal architects	and suppliers, Global		
	Building Resources		

 Table A.B.1: Case Study <number>

Proc	esses w	here carbon emissions (e	mbodied energy) can be reduce	ed		
Building materials and elements		Reused recycled aggregate for concrete Steel from average recycled content				
	Reuse	en Star used recycled aggregate for concrete el from average recycled content				
I	Repla	ased and Replaced energy ced cement	<i>i</i> in process			
Implementation	Decre	Green Star Decreased and Replaced energy in process Replaced cement				
Transportation	Green	Decreased transportation of waste by reusing and recycling Green Star Decreased transportation by localizing the suppliers				
Life cycle stages of bu	ilding	Construction	Construction Construction	Embodied Energy		
Measurable energy to reduce in Building materials and elements		Potential Carbon Emission	on (Embodied Energy) Reduction	Basic		
Measurable energy to re Implementation						
Measurable energy to re Transportation	educe in					
Total Floor		MJ/m ²	MJ/m ²	MJ/ m		

 Table A.B.2: Potential carbon emission (embodied energy) reductions in <name> ground floor construction system

Table. A.B.3: Green Star, potential carbon emission (embodied energy) reductions in <name> ground floor construction system. Case Study <number>. Based on Green Star Technical Manual.

Life Cycle Stages of building	Co	Embodied	
	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	on (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation	MJ/m ²	MJ/m ²	MJ/m ²
Measurable energy to reduce in Implementation	MJ/m ²	MJ/m ²	
Measurable energy to reduce in Transportation	MJ/ m ²	MJ/ m ²	
Green Star, Total Floor	MJ/m ²	MJ/m ²	MJ/ m ²
Green Star, Total Floor		MJ/m ²	1 /1 J/ III

P	rocesses whe	re carbon emissions (er	nbodied energy) can be redu	ced				
	Reused recycled aggregate for concrete							
Building	Steel from average recycled content							
materials and	Green Star							
elements	Reused recy	Reused recycled aggregate for concrete						
	Steel from a	verage recycled content						
.		Decreased and Replaced energy in process						
Implementation		Replaced cement						
	Green Star							
	Decreased to	cansportation of waste by	v reusing and recycling					
Transportation	Decreased transportation of waste by reusing and recycling Green Star							
Transportation								
	Decreased to	cansportation by localizing	ng the suppliers					
		С	Embodied Energy					
Life Cycle Stages o	f building	Pre-Construction Construction Potential carbon emission (embodied energy) reduction		Basic				
Measurable energy	to reduce in							
Measurable energy to reduce in Building materials and elements		MJ/m²	MJ/m²	MJ/m ²				
Measurable energy to reduce in Implementation		MJ/m ²	MJ/m ²					
Measurable energy to reduce in Transportation		MJ/ m ²	MJ/ m ²					
Total F		MJ/m ²	MJ/m ²	NTL - 2				
I otal F	loor		MJ/m ²	MJ/m ²				

Table A.B.4: Potential carbon emission (embodied energy) reduction in construction stages of

 <name> upper floor construction system

Table A.B.5: Green Star, potential carbon emission (embodied energy) reduction in <name> upper floor construction system. Case Study <number>. Based on Green Star Technical Manual.

ilool combilaction by bienn					
Life Cycle Stages of building	Cor	Embodied			
	Pre-Construction	Construction	Energy		
	Potential Carbon Emission	Potential Carbon Emission (Embodied Energy) Reduction			
Measurable energy to reduce in Implementation	MJ/m ² MJ/m ²		MJ/m ²		
Measurable energy to reduce in Implementation	MJ/ m ²	MJ/m ²			
Measurable energy to reduce in Transportation	MJ/ m ²	MJ/ m ²			
Green Star, Total elevated	MJ/m ²	MJ/m ²	MJ/ m ²		
Floor		MJ/ m-			

Pı	rocesses whe	ere carbon emissions (e	mbodied energy) can be reduce	ed		
Building	Reused re	cycled materials as agg	gregate for concrete block			
materials and	Green Sta	r				
elements	Reused re	cycled materials for				
	Decreased	l and Replaced energy	in process			
Implementation	Green Sta	r				
	Decreased to	ransportation of waste by reu	ising and recycling			
Transportation	Green Star					
	Decreased to	ransportation by localizing t	ne suppliers			
Life Cycle Stages	s of building		Construction			
		Pre-Construction	Construction	Energy		
			on (embodied energy) to reduce	Basic		
Measurable energy to reduce in Building materials and elements		MJ/ m ²	MJ/ m ²	MJ/ m ²		
Measurable energy Implementation	to reduce in		MJ/m ²			
Measurable energy to reduce in Transportation		MJ/ m ²	MJ/m ²			
Total Wa		MJ/ m ²	MJ/ m ²	MJ/ m ²		
Total wans		MJ/m ²				

Table A.B.6: Potential carbon emission (embodied energy) reduction in construction stages of the <name> wall construction system.

 Table A.B.7: Green Star, potential carbon emission (embodied energy) reductions in <name> construction system. Case Study <number>. Based on Green Star Technical Manual.

Life Cycle Stages of building	Cor	Embodied	
	Pre-Construction	Construction	Energy
	Potential Carbon Emission	Basic	
Measurable energy to MJ/m ² reduce in Implementation			MJ/m ²
Measurable energy to reduce		MJ/m ²	
in Implementation		1910/111	
Measurable energy to reduce	MJ/ m ²		
in Transportation	IVIJ/ III		
	MJ/m ²	MJ/m ²	NAT/?
Green Star, Total Wall		MJ/ m ²	

Table A.B.8: Green Star, potential carbon emission (embodied energy) reduction in <name> construction system. Case Study <number>. Based on Green Star Technical Manual.

ife Cycle Stages of building	Const	nbodied Energy	
	Pre-Construction Construction		Basic
	Potential Carbon Emission (
surable energy to reduce in lementation	MJ/m ²	MJ/m ²	MJ/m ²
Green Star, Total Roof	MJ/m ²		MJ/ m ²
Green Star, Total Root	I	1v1J/ III	

	Constr	Embodied		
Life Cycle Stages of building	Pre-Construction	Construction	Energy	
	Potential Carbon Emissions (F	Embodied Energy) to reduce	Basic	
Measurable replaced and saved energy in Building materials and elements (Tables <numbers>)</numbers>	MJ/m ²	MJ/m ²	 MJ/m ²	
Measurable replaced and saved energy in Implementation (Tables <numbers>)</numbers>	MJ/m ²	MJ/m ²		
Measurable replaced and saved energy in Transportation (Tables <numbers?)< td=""><td> MJ/ m²</td><td> MJ/m²</td><td></td></numbers?)<>	MJ/ m ²	MJ/m ²		
Total, building system	MJ/m ²	MJ/m ²	M.J/m	
i oun, ounding system]	MJ/m ²		

Table A.B.9: Total potential carbon emission (embodied energy) reductions in construction stages of floor, wall and roof systems

Table A.B.10: Comparison of basic carbon emissions (embodied energy) from different sources (implemented, this research, Green Star and basic/standard) for each building system

	Implemented carbon emission (embodied energy)		CO ² Em	CO ² Emission (embodied energy) reductions		Basic carbon emission (embodied energy)		
	Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²	Embodied MJ/	0,	Carbon Emissions Kg/m ²		Embodied Energy MJ/m ²	Carbon Emissions Kg/m ²
Floor/s	-	-						
External walls	-	-						
Roof/ceiling	-	-						
Total	-	-						
L			This Research	Green Star	This Research	Green Star		

Sources

Columns 2 and 3 data are the embodied energy and reduced carbon emissions in implementation (i.e. completed construction)

Columns 3 and 5 data are the potential reductions in embodied energy and carbon emissions from this research

Columns 4 and 6 data are the potential reductions in enforced energy and carbon emissions from the Green Star tool Columns 7 and 8 data are the (expected) standard or basic embodied energy and carbon emissions

APPENDIX C DATA RELATING TO CHAPTER SEVEN APPLICATION OF RESEARCH MODEL

A.C.1.1 Case Study One – Friendly Beaches Lodge

 Table A.C.1: Potential reduction in carbon emissions (embodied energy) in an elevated timber floor (lower level) construction system. Case Study One (see Lawson 1996, p. 124)

 Potential carbon reduction by this research and Green tool

	Reuse the recycled aggregate in concrete
	- Concrete from 80 % Recycled aggregate (Uche 2008; PCA2014), embodied energy of aggregate is 0.083 MJ/Kg
	Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (26.4 kg concrete – 3.69 cement) Kg x 80% (Lawson 1996, p. 135) =1.52 MJ/m^2
	Reuse the recycled aggregate for brick, 67% (BDA 2014; Tyrell and Goode 2014), 36 kg/m ² (Lawson 1996, p. 124) x 67% x 0.083 MJ/kg = 2 MJ/ m^2
	Reuse materials and elements
	- Use recycled bricks 60% x 90 = 54MJ/m²
Building materials and elements	-Timber products re-used, post-consumer recycled timber or FSC certified timber, use recycled hardwood joist, flooring, 54 $MJ/m^2 \ge 60\% = 32.4 MJ/m^2$
	Green Star
	Reused recycled aggregate for concrete
	In Green Star technical manual, considered maximum 20%, therefore reduced embodied energy by this credit (Concrete from 20% Recycled aggregate) (Green building Council of Australia 2008) is:
	- Concrete from 20% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg
	Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (26.4 concrete $-$ 3.69 cement) Kg (Lawson 1996, p. 12; x 20% = 0.38 MJ/m ²
	Material-8 Timber, Green Star Technical Manual, Materials p. 275, 95% of all timber products re-used, post-consumer recycled timber or FSC certified timber
	60% Recycled hardwood joints use recycled hardwood joist, flooring, 54 MJ/m ² x (p. 124, L. 1), $60\% = 32.4$ MJ/m ²

Decrease and replace energy in the process, Replaced cement	
Geopolymer concrete or 100% replacing Portland with recycled cement substitute (Nath & Sarker 2014) results GHG (McLellan et al. 2011; Kotrayothar 2012) 26.4 kg/m ² (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) 97% = 3.69 kg replaced cement/ m ² in c	
3.69 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p. 13) = 20.66 MJ/m ²	
Implementation Potential 40 per cent energy savings in brick manufacturing using 67% recycled container glass brick grog (BD/ Goode 2014).	A 2014; Tyrell &
Reduced energy 90 MJ/m ² x 40% = 36 MJ/m²	
Green Star, Replaced cement	
Geopolymer concrete or 60% replacing Portland cement with recycled cement substitute (Nath & Sarker 2 reduction in GHG (McLellan et al. 2011) 26.4 kg/m^2 (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) $60\% = 2.29 \text{ kg}$ replaced cement/m ² in c	ĺ.
2.29 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p.13) = 12.82 MJ/m²	

Total Floor		168.82 M	J/m ²	4/31110/ 111			
Total Floor		51.76 MJ/m ²	117.06 MJ/m ²	293MJ / m ²			
in Transportation		8.16 MJ/ m ² Decreased transportation by reusing 4.08 MJ/ m ²	Decreased transportation by localizing 10 MJ/ m²				
Measurable energy to re in Implementation Measurable energy to re		40% saving energy in production 36 MJ/m ² Decreased transportation by reusing	Geopolymer concrete 20.66 MJ/ m ²				
Measurable energy to reduce in Building materials and elemen	ıts	Concrete from recycled aggregate 1.52 MJ/m² 67% Use recycled aggregate for brick 2KJ/m²	Use recycled brick 54MJ/m² Use recycled Hardwood 32.4 MJ/m²	293MJ/m ²			
X 11		Potential Embodied Energy					
building		Pre-Construction	Construction	Standard			
Life cycle stages of	f	Constructi	on	Embodied Energy			
	Tas The 27.7	re are three construction material suppliers, (Dev mania. decreased distance will be 237 Devonport - 157 78 kg/m ² (Lawson 1996, p. 124) /1000 T/m ² x 80	Launceston km = 80 km) km x 4.5 MJtonne/km (Lawson 1996, p. 12	$z = 10 \text{ MJ/ } \text{m}^2$			
	Dec	reased transportation by localizing the suppli	ers				
Transportation	The (609 36.3 Cor	een Star, Decreased transportation of waste by re are construction material suppliers if the mate $\% x 36 \text{ kg/m}^2$ Brick + 60% x 14.7 kg/m2 Hardw $3 \text{ kg/m} 2/1000 \text{ T/m}^2 x 50 \text{ km x 4.5 MJ/tonne/km}$ crete from recycled aggregate (26.4 kg concrete x 4.50 MJ/tonne/km (Lawson 1996, p. 12) = 1.0	rials come from the inside of estate the dista ood and Joist) (Lawson p. 12) = 8.16 MJ/ m² - 3.69 cement) Kg x2% (Lawson 1996, p.1)				
		tonne/km (Lawson 1996, p. 12) = 4.08 MJ/m^2					
		Concrete from recycled aggregate (26.4 kg concrete – 3.69 cement) Kg x80% (Lawson 1996, p.125) /1000 T/m ² x 50 km x 4.50					
	36.3	$3~kg/m2~/1000~T/m^2~x~50~km~x~4.5~MJ/tonne/km$	(Lawson 1996, p. 12) = 8.16 MJ/ m ²				
	(60	% x 36 kg/m ² Brick + 60% x 14.7 kg/m2 Hardwo	ood and Joist)				
	The	re are construction material suppliers if the mate	rials come from the inside of state, the dista	nce will be over 50 km			
	Dec	reased transportation of waste by reusing and	d use recycled materials				

Table A.C.2: Green Star. Potential reduction in carbon emission (embodied energy) in an elevated timber floor (lower level) construction system. Case Study One (see Lawson 1996, p. 124).

Life Cycle Stages of	Cor	struction	Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emission	n (Embodied Energy) Reduction	Basic
Measurable energy to	Concrete from recycled	Use recycled Hardwood 32.4	
reduce in	aggregate 0 0.38 MJ/m ²	MJ/m ²	293 MJ/m ²
Implementation			
Implementation		Geopolymer concrete 12.82 MJ/	
I · · · · · · ·		m ²	
Measurable energy to	Decreased transportation by		
reduce in	reusing 8.16 MJ/ m ²		
Transportation	Decreased transportation by		
	reusing 1.53 MJ/ m ²		
Crean Star Tatal Floor	10.07 MJ/ m ²	45.22 MJ/m ²	293 MJ/ m ²
Green Star, Total Floor	55	.29 MJ/m ²	295 IVIJ/ III ⁻

Table A.C.3: Potential reduction in carbon emissions (embodied energy) in timber frame, single skin timber wall construction system. Case Study One (see Lawson 1996, p. 125)

	Determined and an a		
	Potential carbon i	reduction by this research and Green tool	
	Reuse the recycled mat	erials	
Building materials and	Use recycled softwood s	used, post-consumer recycled timber or FSC cert tud, 60% Reuse softwood stud@100x50mm+ so (Lawson 1996, p.125) = 22.2 MJ/m ²	
elements	- Use recycled thermal in	nsulation, 49MJ/kg (Lawson 1996) - 20.90 MJ/k	$xg \ge 0.585 kg/m^2 = 16.43 MJ/m^2$
	Green Star Reuse the recycled mat Use recycled softwood s 60% x 37 MJ/m ² (p.125,	tud, 60% Reuse softwood stud@100x50mm+ so	oftwood plates@100x50 mm =,
	Decreased transportati	on of waste by reusing and recycling	
	There are construction n over 50 km	naterial suppliers if the materials come from the	inside of state, the distance will I
	7.15 kg/m2 Softwood +	Softwood plate + \dots = 22 kg/m ²	
	22 x 60% kg/m2 /1000 7	T/m2 x 50 km x 4.5 MJ/tonne/km (Lawson p. 12	$) = 2.97 \text{ MJ/ } \text{m}^2$
Transportation	There are construction n be over 50 km 7.15 kg/m2 Softwood +	on of waste by reusing and recycling naterial suppliers if the materials come from the Softwood plate + = 22 kg/m ² f/m2 x 50 km x 4.5 MJ/tonne/km (Lawson p. 12	
	Decreased transportati	on by localizing the suppliers	
	from Devonport of Tasn	tion material suppliers, (Devonport TAS 2014), nania. will be 237 Devonport - 157 Launceston km = 8	
	22 kg/m ² /1000 T/m2 x	80 km x 4.5 MJtonne/km (Lawson 1996, p. 12)	= 7.91 MJ/ m ²
Areas that Embodied Energy		Construction	Embodied Energy
can be reduced	Pre-Construction	Construction	
Maaayaahla ananay ta nady aa in	Use thermal insulation	lied Energy to Replace and Save 60% softwood stud + softwood plates	Standard
Measurable energy to reduce in Building materials and	with recycled	22.2 MJ/m^2	
elements	aggregates 23.2 MJ/m ²	Use Recycle thermal insulation 16.43 MJ/m ²	151MJ/ m ²
(Desmand	1	
Measurable energy to reduce in Transportation	Decreased transportation by reusing 2.97MJ/ m²	Decreased transportation by localizing 7.91 MJ/ m²	
T-4-1 W-11-	26.17 MJ/m ²	46.54 MJ/m ²	151MJ/ m ²
Total Walls		72.71 MJ/m ²	
	I	(1 00 NAV 2	
General Construction system		61.83 MJ/m ²	151MJ/ m ²

Table A.C.4: Green Star. Potential reduction in carbon emissions (embodied energy) in timber frame,
single skin timber wall construction system. Case Study One (see Lawson, 1996. p. 125).

		se Study One (see Edwson, 1990. p. 122	· / · _	
Life Cycle Stages of		Construction		Embodied
building	Pre-Construction	Construction		Energy
	Potential Carbon E	mission (Embodied Energy) Reduction		Basic
Measurable energy to		60% softwood stud + softwood plates 22.2		151 MJ/m ²
reduce in Implementation		MJ/m ²		151 MJ/III
Measurable energy to	Decreased transportation			
reduce in Transportation	by reusing 2.97MJ/ m²			
			1	
Career Stern Tetel Well	2.97 MJ/ m ²	22.2 MJ/m ²	[151 MJ/ m ²
Green Star, Total Wall		25.17 MJ/m ²		151 MJ/ m ⁻

Table A.C.5: Potential reduction in carbon emissions (embodied energy) in a timber frame, steel sheet roof. Case Study One (see Lawson 1996, p. 133).

	Potential carbon	n reduction by (this research and Green tool		
	Steel from average recycled conte	nt			
	Steel sheet from recycled contents 85.75 MJ/m ²	s {38 MJ/Kg (La	wson 1996) – 20.50 MJ/Kg} = 17.5 M	$IJ/Kg \ge 4.9 \text{ kg} / \text{m}^2 =$	
	Reused materials and elements				
	Softwood Trusses from recycled tr	russes 40% x 34	MJ/m ² P. 133 L.2 (Design Coalition 2	013) = 13.6 MJ/m²	
	Using recycled trusses = $60\% \times 34$	MJ/m ² (Lawson	n 1996, p. 133) 20.4 MJ/m²		
	Use recycled thermal insulation, 49 Construction Information 2014)	9MJ/kg (Lawson	n 1996) - 20.90 MJ/kg x 0.825kg/m ² =	17.57 MJ/m ² (Steel	
Building materials and	Green Star				
elements	Steel from average recycled conte	nt			
	Material-6 Steel (Green Star Technic embodied energy by this credit (Stee		terials) is considered maximum 90%, t cycled contents) (GBCA 2008) is:	herefore reduced	
	Steel sheet from recycled contents $g/m^2 \times 90\% = 77.17 \text{ MJ/m}^2$	s {38 MJ/Kg, P.	133 1.2 (Lawson 1996) – 20.50 MJ/Kg	;} = 17.5 MJ/Kg x 4.9	
	Reused materials and elements (lo	ocal salvage/re-u	se centre)		
	Material-8 Timber (Green Star Tech recycled timber or FSC certified tim		faterials), 95% of all timber products a	e-used, post-consumer	
	Softwood Trusses from recycled tr	russes 40% x 34	(Design Coalition 2013) = 13.6 MJ/m	1 ²	
	Using recycled trusses = $55\% \times 34$	MJ/m ² (Lawson	n, 1996, p. 133) = 18.7 MJ/m²		
	Decreased transportation of waste	e by reusing and	1 recycling		
	There are construction material supp (ackson (Port Jackson 2014) 297 - T		trials come from the outside of state, the cone 2014) 25.2 km = over 100 km	he distance will be Port	
	Reuse softwood trusses 11.15 (trusse 1996, p. 12) = 5.01 MJ/ m²	es 8.25, battens	2.9) kg/m ² /1000 T/m ² x 100km x 4.5	MJ/tonne/km (Lawson	
	Green Star				
Transportation			trials come from the outside of state: the come from the outside of state: the come 2014) 25.2 km = over 100 km	ne distance will be (Port	
	Reuse softwood trusses 11.15 (truss 1996, p. 12) = 5.01 MJ/ m²	es 8.25, battens	2.9) kg/m ² /1000 T/m ² x 100 km x 4.5	MJ/tonne/km (Lawson	
	Decreased transportation by local	lizing the suppli	ers		
	There are construction material suppliers if the materials come from the inside of state: Local supplier is Skyline				
	(2014) The saved distance will be (Thylacine 2014) 25.2 km				
			.2 km x 4.5 MJtonne/km (Lawson 199	71	
Life Cycle Stages of build	Pre-Constructio	Constructi	on Construction	Embodied Energy Basic	
			arbon emissions	Dasic	
Measurable energy to redu Building materials and	Tennona from enougled timb.		Use recycled trusses 60% 20.4 MJ/m ²	220141/ 2	
elements	Steel sheet from recycled co MJ/m ²	ontent 85.75	Use recycled thermal insulation 17.57 MJ/m ²	330MJ / m ²	

Total Roof, Research	144.59 MJ	/m ²	330MJ/ m ²
Measurable energy to reduce in Transportation	Decreased transportation by reusing trusses 5.01 MJ/ m ²	Decreased transportation by localizing 2.26 MJ/ m²	

Table A.C.6: Green Star, potential reduction in carbon emissions (embodied energy) in timber frame, steel sheet roof construction system. Case Study One (see Lawson 1996, p. 133)

Life Cycle Stages of	Co	nstruction	Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	n (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation	Steel sheet from 90% Recycled contents = 77.17 MJ/m² Trusses from recycled timber 40% 13.6 MJ/m²	Use recycled trusses 55% 18.7 MJ/m²	330 MJ/m ²
Measurable energy to reduce in Transportation	Decreased transportation by reusing trusses 5.01 MJ/ m²		
Green Star, Total Roof	95.78 MJ/m ²	18.7 MJ/m ²	330 MJ/ m ²

Table A.C.7: Potential reduction in carbon emissions (embodied energy) in timber floor, timber walls, steel roof construction system. Case Study One.

Life Cycle Stages of building	Constru	ction	Embodied
	Pre-Construction	Construction	Energy
	Potential Carbon En	nissions to reduce	Basic
Measurable energy to reduce in Building materials and elements	126.07 MJ/m ²	163 MJ/m ²	774 MJ/m ²
Measurable energy to reduce in Implementation	36 MJ/m²	20.66 MJ/m ²	
Measurable energy to reduce in Transportation	20.22 MJ/m ²	20.17 MJ/m²	
	· · · · ·		
	182.29 MJ/m ²	203.83 MJ/m ²	
Total, building system	386.12	MJ/m ²	774 MJ/m ²

A.C.1.2 Case Study Two – ACF Green Home

Table A.C.8: Potential reduction in carbon emissions (embodied energy) in a concrete slab on ground floor construction system. Case Study Two (see Lawson 1996, p. 124).

	Potential carbon reduction by this research and Green tool	
	Reused recycled aggregate for concrete	
	- Concrete from 80 % Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggreg	gate is 0.083
Building materials and elements	MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (290.4 concrete -39.4 (Lawson 1996, p.125) x 80% =16.67 MJ/m ² Steel from average recycled content	3 cement) Kg
	 Steel mesh +Edge beams from average recycled content = 3.882 Kg x {34 MJ/Kg (Lawson 15 MJ/Kg} = 53.96MJ/m² 	996, p13) - 20.10
	Green Star Reused recycled aggregate for concrete Material-5 (Green Star Technical Manual, Materials) is considered maximum 20%, therefore re- energy by this credit (Concrete from 20% Recycled aggregate) (GBCA 2008) is: embodied energy by this credit (Concrete from 20% Recycled aggregate) (GCBA 2008) is: - Concrete from 20% Recycled aggregate (Uche 2008; PCA) 2014), embodied energy of aggregate MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (290.4 concrete -39.4 (Lawson 1996, p. 125) x 20% = 4.16 MJ/m² Steel from average recycled content Material-6 (Green Star Technical Manual, Steel) is considered maximum 90%, therefore reduced	gate is 0.083 3 cement) Kg
	energy by this credit (Steel from Recycled content) (GBCA 2008) is: 3.882 Kg x 90% {34 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg} = 53.95 MJ/m²	
Implementation	Decreased and Replaced energy in process Replaced cement Geopolymer concrete or 100% replacement Portland cement with recycled cement substitute 2014) results 97% reduction in GHG (McLellan et al. 2011) 290.4 kg/m2 (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) 97% = 39.43 kg repla in concrete 39.43 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p. 13) = 220.83 MJ/m²	
	Green Star Replacing maximum 60% of cement 290.4 kg/m2 (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) 60% = 24.38 kg repla in concrete 24.38 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p. 13) = 136.59 MJ/m²	aced cement/ m ²
	Decreased transportation of waste by reusing and recycling There are three construction material suppliers, (Melbourne Building Supplies 2014), If the mat the interstate somewhere in Melbourne, (Boral 2014). The decreased distance will be 54.2 k Reduced transportation by Reusing aggregate, (290.4 kg/m ² - 39.43 kg/m ²) x 80% /1000 T/m ² x MJ/ton/km (Lawson p. 12) =40.80 MJ/ m ²	
Turning	Green Star There are three construction material suppliers, (Melbourne Building Supplies 2014). If the ma somewhere in Melbourne, (Boral 2014), the decreased distance will be 54.2 k	terials come from
Transportation	Reduced transportation by reusing aggregate, (290.4 kg/m ² - 39.43 kg/m ²) /1000 T/m ² x 45.2 kr MJ/ton/km (Lawson 1996, p. 12) x 20% = 10.20 MJ/m²	n x 4.5
	Decreased transportation by localizing the suppliers	
	Decreased transportation by localizing the suppliers There are three construction material suppliers, (Melbourne Building Supplies 2014), If the ma somewhere in Melbourne, (Boral 2014), the decreased distance will be 54.2 k	terials come from
	There are three construction material suppliers, (Melbourne Building Supplies 2014), If the ma	
Life cycle stages of buildin	There are three construction material suppliers, (Melbourne Building Supplies 2014), If the material somewhere in Melbourne, (Boral 2014), the decreased distance will be 54.2 k (290.4kg aggregate + mesh 3.12kg) = 293.52 kg/m ² /1000 T/m2 x 54.2 km x 4.5 MJtonne/km (12) = 15.04 MJ/ m² g Construction	Lawson 1006, p Embodied
Life cycle stages of buildin	There are three construction material suppliers, (Melbourne Building Supplies 2014), If the masomewhere in Melbourne, (Boral 2014), the decreased distance will be 54.2 k (290.4kg aggregate + mesh 3.12kg) = 293.52 kg/m² /1000 T/m2 x 54.2 km x 4.5 MJtonne/km (12) = 15.04 MJ/ m² g Construction Pre-Construction Construction	Lawson 1006, p Embodied Energy
Measurable energy to reduct in Building materials and	There are three construction material suppliers, (Melbourne Building Supplies 2014), If the ma somewhere in Melbourne, (Boral 2014), the decreased distance will be 54.2 k (290.4kg aggregate + mesh 3.12kg) = 293.52 kg/m ² /1000 T/m2 x 54.2 km x 4.5 MJtonne/km (12) = 15.04 MJ/ m² g Construction Pre-Construction Pre-Construction Construction Concrete from 30% recycled aggregate Steel mesh, beams from average recycled	Lawson 1006, p Embodied
Life cycle stages of buildin Measurable energy to reduc in Building materials and elements Measurable energy to reduce Implementation	There are three construction material suppliers, (Melbourne Building Supplies 2014), If the masses of the somewhere in Melbourne, (Boral 2014), the decreased distance will be 54.2 k (290.4kg aggregate + mesh $3.12kg$) = 293.52 kg/m² /1000 T/m2 x 54.2 km x 4.5 MJtonne/km (12) = 15.04 MJ/ m² g Construction Pre-Construction Construction Pre-Construction Construction Concrete from 30% recycled aggregate Steel mesh, beams from average recycled content = 53.96 MJ/m e in Geopolymer, replacing 100% of cement = 220.83 MJ/m²	Lawson 1006, p Embodied Energy Basic
Measurable energy to reduce in Building materials and elements Measurable energy to reduce	There are three construction material suppliers, (Melbourne Building Supplies 2014), If the masses of the somewhere in Melbourne, (Boral 2014), the decreased distance will be 54.2 k (290.4kg aggregate + mesh $3.12kg$) = 293.52 kg/m² /1000 T/m2 x 54.2 km x 4.5 MJtonne/km (12) = 15.04 MJ/ m² g Construction Pre-Construction Construction Pre-Construction Construction Concrete from 30% recycled aggregate Steel mesh, beams from average recycled content = 53.96 MJ/m e in Geopolymer, replacing 100% of cement = 220.83 MJ/m²	Lawson 1006, p Embodied Energy Basic

Table A.C.9: Green Star. Potential reduction in carbon emissions (embodied energy) in a 110 mmconcrete slab on ground floor construction system. Case Study Two (see Lawson 1996, p. 124).

Life Cycle Stages of	Construction			Embodied
building	Pre-Construction	Construction		Energy
_	Potential Carbon Emissio	n (Embodied Energy) Reduction		Basic
Measurable energy to	20% Recycled aggregate for	90%Steel mesh from average recycled		645 MJ/m ²
reduce in Implementation	concrete = 4.16 MJ/m^2	content 53.95MJ/m²		045 WIJ/III
Measurable energy to reduce		Geopolymer, 60% Cement		
in Implementation		Replacements 136.59 MJ/m ²		
Measurable energy to reduce	Decreased transportation by			
in Transportation	reuse aggregate 15.04 MJ/m ²			
	19.20 MJ/m ²	190.54 MJ/m ²		645MJ/ m ²
Green Star, Total Floor	209	9.74 MJ/m ²		0451VIJ/ m ²

Table A.C.10: Potential reduction in carbon emissions (embodied energy) in timber framed timberupper floor construction system. Case Study Two (see Lawson 1996, p. 124).

	Potential ca	rbon reduction by this	research and Green tool		
Building	Reused ma	terials and elements			
materials and elements	60% Recycled flooring @ 18 = 84.6 MJ/m²	nm + Timber wson 1996, p. 124)			
	Material-8 Tin	nnical Manual) 95% of all timber p ed timber (GBCA 2008)	products re-used,		
	flooring @ 18	softwood joints (Design Coalit mm particleboard 50 MJ/m ² + 9 teel Construction Information 2	ion 2013) @ (600 c-c) 300x 500 n 01 MJ/m ² = %60 x 141 MJ/m ² (Lav 2014)	nm + Timber vson 1996, p. 124 =	
	Decreased	transportation of waste	by reusing and recycling		
	materials come	e from somewhere in Melbourn	s, (Melbourne Building Supplies 2 e, (Boral 2014), the decreased dist AJtonne/km (Lawson 1996, p. 12)	ance will be 54.2 k	
	Green Star				
Transportation	There are three construction material suppliers (Melbourne Building Supplies 2014). If the materials come somewhere in Melbourne (Boral 2014), the decreased distance will be 54.2 k				
	11.4 kg/m ² x 60% /1000 T/m2 x 54.2 k x 4.5 MJtonne/km (Lawson 1996, p. 12) = 1.66 MJ/ m²				
	Decreased transportation by localizing the suppliers				
		are three construction material suppliers, (Melbourne Building Supplies 2014). If the ials come from somewhere in Melbourne, (Boral 2014), the decreased distance will be 54.2km			
	U	0% /1000 T/m2 x 54.2 km x 4.5	5 MJtonne/km (Lawson 1996, p. 1	2) = 2.66 MJ/ m ²	
Life Cycle Stage	es of building		struction	Embodied Energy	
		Pre-Construction Potential reduction	Construction n in carbon emissions	Basic	
Measurable energy to reduce in Building materials and elements			60% recycled timber floor 84.6 MJ/m ²	147MJ/m ²	
Measurable energy to Transportation	reduce in	Saved energy in transportation by reusing 1.66 MJ/ m²	Decreased transportation by localizing 2.66 MJ/ m²		
		1.66 MJ/m²	87.26 MJ/m ²	147MJ/ m ²	
Total Fl	oor		2 MJ/m ²		

Table A.C.11: Green Star. Potential reduction in carbon emissions (embodied energy) in timber framed timber floor upper floor construction system. Case Study Two (see Lawson 1996, p. 124).

I I	2			L /
Life Cycle Stages of	Co	onstruction		Embodied
building	Pre-Construction	Construction		Energy
	Potential Carbon Emission (Embodied Energy) Reduction			Basic
Measurable energy to		60% recycled timber floor 84.6 MJ/m ²		147 MJ/m ²
reduce in Implementation				14/ MJ/III
Measurable energy to	Saved energy in transportation			
reduce in Transportation	by reusing 1.66 MJ/ m²			
Course Steer Total Flags	1.66 MJ/m ²	84.6 MJ/m ²		147 MJ/ m ²
Green Star, Total Floor	86.26 MJ/m ²			14/ MJ/ m ⁻

Table A.C.12: Potential reduction in carbon emissions (embodied energy) in timber framed, clay brick veneer wall construction system. Case Study Two (see Lawson 1996, p. 127).

cheer wan constru	cuon s	ystem. Case Study I	wo (see Lawson 1990, p. 127).		
	Poten	tial carbon reduction	on by this research and Green tool		
	Reus	ed recycled aggrega	ates		
	Reuse	• • • •	ick, 67% (BDA 2014; Tyrell and Goode 2014), 147	kg/m ² (Lawson	
Building materials and elements	Use rec = 60% Use rec MJ/m ²	<pre>eused materials and elements (se recycled softwood stud, 60% reuse softwood stud@100x50mm+ softwood plates@100x50 mm 60% x 33 MJ/m²= 19.8 MJ/m² se recycled thermal insulation, 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.585kg/m² = 16.43 LJ/m² (Steel Construction Information 2014). Use recycled thermal insulation, 49MJ/kg (Lawson 996) - 20.90 MJ/kg x 0.585kg/m² = 16.43 MJ/m² (Steel Construction Information 2014)</pre>			
		n Star		2014)	
	Reus Use rea	ed materials and el	% Reuse softwood stud@100x50mm+ softwood pla	tes@100x50	
	Decr	eased and replaced	energy		
	Decr	ease energy			
Implementation	water.		ength and durability from the chemical reaction of f s energy is used in production than in fired clay bric		
		ial 40 per cent energy sav 3rDA2014; Tyrell & Goo	ing in brick manufacturing using 67% recycled con de 2014).	tainer glass brick	
	Reduce	ed energy 368 MJ/m ² x 40	$0\% = 147.2 \text{ MJ/m}^2$		
	-	.			
		Decreased transportation of waste by reusing and recycling			
	materia	There are three construction material suppliers, (Melbourne Building Supplies 2014). If the materials come somewhere in Melbourne, (Boral 2014), the decreased distance will be 54.2km			
		and Recycled aggregate f on 1996, p. 12) = 24.02 M	for brick 147 kg/m² x 67% /1000 T/m² x 54.2 km x 4 IJ/ m²	4.5 MJ/tonne/km	
	Reused	the recycled softwood 8	.1 kg/m ² /1000 T/m ² x 54.2 km x 4.5 MJ/tonne/km =	= 1.97 MJ/ m ²	
Transportation	There a		terial suppliers (Melbourne Building Supplies 2014 ourne, (Boral 2014), the decreased distance will be 5		
	Reused		.1 kg/m ² /1000 T/m ² x 54.2 km x 4.5 MJ/tonne/km (
	Decr	eased transportatio	n by localizing suppliers		
	There a materia	are three construction mat als come from somewhere /m ² (brick +wood) /1000	terial suppliers, (Melbourne Building Supplies 2014 e in Melbourne, (Boral 2014), the decreased distanc T/m2 x 54.2 km x 4.5 MJtonne/km (Lawson 1996,	e will be 54.2km	
Life Cycle Stages of	1		Construction	Embodied	
		Pre-Construction	Construction	Energy	
Measurable energy to	reduce	76% Use recycled	al reduction in carbon emissions 60% softwood stud + softwood plates 19.8	Standard	
in Building materials		aggregate for brick	MJ/m ²	5 61 MJ/ m²	
elements		8.17 KJ/m ²	Use Recycled thermal insulation 16.43 MJ/m²		
Implementation		40% saving energy in production 147.2 MJ/m ²			
Measurable energy to r Fransportation	educe in	Saved energy in transportation Reuse of aggregate 24.02 MJ/ m²	Reuse of softwood 1.97 MJ/ m² Decreased transportation by localizing 38.53 MJ/ m²		
		179.39 KJ/m ²	77.09 MJ/m ²		
Total Walls		1/7.37 NJ/III	256.48 MJ/m ²	561MJ/ m ²	
		1			

Table A.C.13: Green Star. Potential reduction in carbon emissions (embodied energy) in timber framed, clay brick veneer wall. Case Study Two (see Lawson 1996, p. 127).

Life Cycle Stages of	Co	Instruction	Embodied	
building	Pre-Construction Construction		Energy	
	Potential Carbon Emissio	n (Embodied Energy) Reduction	Basic	
Measurable energy to		60% softwood stud + softwood plates	561 MJ/m ²	
reduce in Implementation		19.8 MJ/m ²	501 WIJ/III	
Measurable energy to		Reuse of softwood 1.97 MJ/ m²		
reduce in Transportation				
Concern Steern Testel Well		242.57 MJ/m ²	561 MJ/ m ²	
Green Star, 10tal Wall	Green Star, Total Wall 21.77 MJ/m ²			

Table A.C.14: Potential reduction in carbon emissions (embodied energy) in timber framed, concrete
tile roof construction system. Case Study Two (see Lawson 1996, p. 134).

	Potential carbon reduction by this research and Green tool				
Building	Reused materials and elements				
materials and	- Softwood Trusses from recycled trusses 40% x 43 (Design Coalition 2013) = 17.2 MJ/m ²				
elements	- Using recycled trusses = $60\% \times 43 \text{ MJ/m}^2 = 25.8 \text{ MJ/m}^2$				
	- Use insulation from recycled materials, 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.6255 kg/m ² = 17.57 MJ/m ² (Steel Construction Information 2014)				
	Being small and modular in nature, concrete roof tile is less prone to waste. Roof tiles can be crushed and recycled (LEED 2014)				
	Use tiles from recycled roof tiles, 92 MJ/m ² x 13% (LEED 2014) = 11.96 MJ/m ²				
	Use tiles from recycled roof tiles (Herbudiman & Saptaji 2013) from 45% recycled content				
	Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (44 concrete $- 6.16$ cement) Kg/m ² (Lawson 1996, p. 134) x 45% = $0.083 \text{ x} 37.84 \text{ kg/m2 x} 50\%$ (Herbudiman & Saptaji 2013) = 1.57 MJ/m²				
	Green Star				
	Reused materials and elements (local salvage/re-use centre) Material-8 Timber (Green Star Technical Manual) Materials 95% of all timber products re-used, post-consumer recycled timber or FSC certified timber				
	- Softwood Trusses from recycled trusses 40% x 43 (Design Coalition 2013) = 17.2 MJ/m^2				
	- Using recycled trusses, 55% x 43 $MJ/m^2 = 23.65 MJ/m^2$				

i oun noon		2401913/ III				
Total Roof	21.65 MJ/m ²	69.86 MJ/m ²	240MJ/ m ²			
Measurable energy to reduce in Transportati	on Decreased transportation by reusing trusses. 4.45 MJ/ m²	Decreased transportation by localizing 14.53 MJ/ m ²				
Measurable energy to reduce in Building materials and element	Trusses from recycled trusses 17.2 MJ/m ²	Using recycled trusses 25.8 MJ/m² Use recycled thermal insulation 17.57MJ/n Use recycled roof tiles 13%, 11.96 MJ/m²	240MJ /m ²			
		rbon Emissions to reduce	Basic			
building	Pre-Construction	Construction	Embodied Energy			
Life Cycle Stages of		Construction				
	Decreased transportation by localizing suppliers There are three construction material suppliers, (Melbourne Building Supplies 2014). If the materials come from somewhere in Melbourne (Boral 2014), the decreased distance will be 54.2km. 59.6 kg/m ² /1000 T/m ² x 54.2 km x 4.5 MJtonne/km (Lawson 1996, p. 12) = 14.53 MJ/ m²					
	Reuse of trusses, 18.25 kg/m ² /100 4.45 MJ/ m ²	00 T/m ² x 54.2 km x 4.5 MJ/tonne/km (Lawson 1	996, p. 12) =			
Transportation	materials come from somewhere in 54.2km.	There are three construction material suppliers, (Melbourne Building Supplies 2014). If the materials come from somewhere in Melbourne (Boral 2014), the decreased distance will be				
	Decreased transportation by reusin 54.2 km x 4.5 MJ/tonne/km (Laws	g of trusses 18.25 kg/m ² (Lawson 1996, p.134) , on 1996, p. 12) = 4.45 MJ/ m²	/1000 T/m ² x			
		There are three construction material suppliers, (Melbourne Building Supplies 2014). If the materials come from somewhere in Melbourne (Boral 2014), the decreased distance will be 54.2km.				
	Decreased transportation					

Table A.C.15: Green Star. Potential reduction in carbon emissions (embodied energy) in timber framed, concrete tile roof construction system. Case Study Two (see Lawson 1996, p. 134).

Life Cycle Stages of	Construction		Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emission	n (Embodied Energy) Reduction	Basic
Measurable energy to	Softwood Trusses from	Using recycled trusses 23.65 MJ/m ²	
reduce in Building	recycled trusses 17.2 MJ/m ²		240 MJ/m ²
materials and elements			
Measurable energy to	Decreased transportation by		
reduce in Transportation	Reuse of truss 4.45 MJ/m ²		
	·		1
Carrow Sterry Total Dasf	21.51 MJ/ m ²	23.65 MJ/m ²	240 MJ/ m ²
Green Star, Total Roof	45.	16 MJ/m ²	240 MJ/ m ⁻

Table A.C.16: Potential reduction in carbon emissions (embodied energy) in concrete slab floor, timber framed brick veneer walls, timber framed concrete tile roof. Case Study Two.

Life Cycle Stages of building	Constru	iction	Embodied
	Pre-Construction	Construction	Energy
	Potential Carbon En	nissions to Reduce	Basic
Measurable energy to reduce in Building materials and elements (Tables 1,2,3,)	42.04 MJ/m ²	230.12 MJ/m ²	1623 MJ/m ²
Measurable energy to reduce in Implementation (Tables 1,2 and 3)	147.2 MJ/m ²	220.83 MJ/ m ²	
Measurable energy to reduce in Transportation (Tables 1,2 and 3)	49.42 MJ/m ²	94.25 MJ/m ²	
	238.66 MJ/m ²	545.20 MJ/m ²	1(22)1(1) 2
Total, building system	783.86 MJ/m ²		1623 MJ/m ²

A.C.1.3 Case Study – Three Display Project Home

Table A.C.17: Potential reduction in carbon emissions (embodied energy) in a 110 mm concrete slab on ground floor. Case Study Three (see Lawson 1996, p. 124).

Total Floor	_	106.99 MJ/m ²	308.07 MJ/m ²	645MJ/ m ²		
Transportation		aggregate 90.32 MJ/m ²	33.28 MJ/ m ²			
Implementation Implementation		Decreased transportation by reuse	cement = 220.83 MJ/m ² Decreased transportation by localizing			
feasurable energy to reduce	ce in		Geopolymer, replacing 100% of			
Measurable energy to redu Building materials and elements			Steel mesh, beams from average recycled content = 53.96 MJ/m	645MJ/m ²		
	-	Pre-Construction Potential Carbon Emission (Construction Embodied Energy) Reduction	Energy Basic		
Life cycle stages of buildi	ng		ruction	Embodied		
	(290.4k	11	2/m ² /1000 T/m2 x 25.2 km x 4.5 MJtonne/km			
		construction material supplier: aterials come from a local supplier (Sky	line 2014), the decreased distance will be 25.2	= km		
	Decreas	Decreased transportation by localizing the suppliers				
		ed transportation by reusing aggregate, (290.4 kg/m ² - 39.43 kg/m ²) /1000 T/m ² x 100 km x 4.5 /km (Lawson 1996, p. 12) x 20% = 22.58 MJ/ m²				
Transportation	(Port Jac	ckson 2014) 297 - (Thylacine 2014) 25.2	2 km = over 100 km			
	Green S There ar		materials come from the outside of stat, the di	stance will be		
	MJ/ton/ł	MJ/ton/km (Lawson 1996, p. 12) = 90.32 MJ/ m ²				
		(Port Jackson 2014) 297 - (Thylacine 2014) 25.2 km = over 100km Reduced transportation by reusing aggregate, (290.4 kg/m ² - 39.43 kg/m ²) x80% /1000 T/m ² x 100 km x 4.5				
	There ar		materials come from the outside of stat, the di	stance will be		
	Deamass	ad transportation of wasta by parsing	and recycling			
	290.4 Kg/m2 (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) 60% = 24.38 kg replaced co in concrete 24.38 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p.13) x 60% = 81.91 MJ/m²					
	Replacir	Replacing maximum 60% of cement (GBCA 2008) 290.4 kg/m2 (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) $60\% = 24.38$ kg replaced cement/ m ²				
Implementation	39.43 kg	39.43 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p.13) = 220.83 MJ/m ² Green Star				
		290.4 kg/m2 (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) 97% = 39.43 kg replaced cement/m				
	Geopoly	d cement mer concrete or 100% replacement by n in GHG (McLellan et al. 2011)	recycled cement substitute (Nath & Sarker 2	014) results 979		
		ed and Replaced energy				
	3.882 K	g x 90% {34 MJ/Kg (Lawson 1996, p13) - 20.10 MJ/Kg} = 48.56 MJ/m²			
	Material		is considered maximum 90%, therefore reducent) (GBCA 2008) is:	ed embodied		
		n 1996, p. 125) x 20% = 4.16 MJ/m² om average recycled content				
	- Concre	ete from 30% Recycled aggregate embod	lied energy of aggregate is 0.083 MJ/Kg ggregate 0.083 MJ/Kg x (290.4 concrete –39.	43 cement) Kg		
	Material		rials is considered maximum 20%, therefore r eled aggregate) (GCBA 2008) is:	educed embodie		
	Green S	J/Kg} = 53.96MJ/m ² Star recycled aggregate for concrete				
	- Steel n	from average recycled content l mesh + Edge beams from average recycled content = 3.882 Kg x {34 MJ/Kg (Lawson 1996, p13) -				
Building materials and elements	(Lawson	n 1996, p.125) x 80% = 16.67 MJ/m^2	ggregate 0.083 MJ/Kg x (290.4 concrete –39.	43 cement) Kg		
	MJ/Kg	concrete from 80% Recycled aggregate (Uche 2008; PCA 2014) embodied energy of aggregate is 0.083 //Kg				

Table A.C.18: Green Star. Potential reduction in carbon emissions (embodied energy) in a 110 mmconcrete slab on ground floor. Case Study Three (see Lawson 1996, p. 124).

Life Cycle Stages of	Co	Embodied	
building	Pre-Construction Construction		Energy
	Potential Carbon Emission	n (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation	20% Recycled aggregate for concrete = 4.16 MJ/m²	90% Steel mesh from average recycled content 48.56 MJ/m²	645 MJ/m ²
		·	
Measurable energy to reduce		Geopolymer, 60% Cement	
in Implementation		Replacements 81.91 MJ/m ²	
Measurable energy to reduce	Decreased transportation by		
in Transportation	reuse aggregate 22.58 MJ/m ²		
Career Stern Tetal Flags	26.74 MJ/m ²	130.47 MJ/m ²	645MJ/ m ²
Green Star, Total Floor	157	7.21 MJ/m ²	045IVIJ/ m ⁻

Table A.C.19: Potential reduction in carbon emissions in a timber framed, clay brick veneer wall (Lawson 1996, p. 127).

Total Walls		199.69 KJ/m ²	57.78 MJ/m ² 257.47 MJ/m ²	561MJ/ m ²		
Aeasurable energy to red Transportation	uce in	Saved energy in transportation Reuse of aggregate 44.32 MJ/ m²	Reuse of softwood 3.64 MJ/ m² Decreased transportation by localizing 17.91 MJ/ m²			
Implementation		40% saving energy in production 147.2 MJ/m ²				
elements		KJ/m ²	Use Recycle thermal insulation 16.43 MJ/m²			
Building materials and		contents brick 8.17	MJ/m ²	561 MJ/ m²		
Measurable energy to re		20% Use recycled	60% softwood stud + softwood plates 19.8			
			reduction in carbon emissions	Standard		
		Pre-Construction	Construction			
Life Cycle Stages of			Construction	Embodied Energy		
	· · · ·		2 x 25.2 km x4.5 MJtonne/km (Lawson 1996, p. 12)	= 17.91 MJ/ m ²		
		If materials come from the inside of state, local supplier is Skyline (2014), the saved distance will be (Thylacine 2014) 25.2 km				
		sed transportation by localiz	· · ·			
		2014) 25.2 km = over 100 km Reused recycled softwood 8.1 kg/m ² /1000 T/m ² x100 km x 4.5 MJ/tonne/km (Lawson p.12) = 3.64 MJ/ m²				
	If materials come from the outside of state, distance will be (Port Jackson (Port Jackson 2014) 297 - (Thylacine					
Transportation	Green Star					
	Reused recycled softwood 8.1 kg/m ² /1000 T/m ² x 100 km x 4.5 MJ/tonne/km (Lawson 1996. p.12) = 3.64 MJ/m²					
	1996, p. 12) = 44.32 MJ/m²					
	Reuse and Recycled aggregate for brick 147 kg/m ² x 67% /1000 T/m ² x 100 km x 4.5 MJ/tonne/km (Lawson					
	If materials come from the outside of state, distance will be (Port Jackson (Port Jackson 2014) 297 - (Thylacine 2014) 25.2 km = over 100 km					
	Decreas	sed transportation of the wa	ste by reusing and recycling			
	Reduced	a energy 500 mis/m x 40/0 =				
Implementation		yrell & Goode 2014). d energy 368 $MJ/m^2 \ge 40\% =$	147.2 MJ/m ²			
			in brick manufacturing using 67% recycled container	r glass brick grog (BCA		
	MJ/m ² =	= 19.8 MJ/m ²				
	- Use rec		use softwood stud@100x50mm+ softwood plates@1	100x50 mm = 60% x 33		
	Materia	1-8 Timber (Green Star Techn	nical Manual) Materials, 95% of all timber products			
	Materia	1-3 (Green Star Technical Ma	nual) Materials is considered maximum 80% reused dit (Concrete from 80% reused material) (GCBA 20			
	Green S Reused	Star materials and elements				
Building materials and elements		ction Information 2014)				
		= 19.8 MJ/m² evoled thermal insulation, 49M	4J/kg (Lawson 1996) - 20.90 MJ/kg x 0.585kg/m ² =	16.43 MJ/m ² (Steel		
		materials and elements ycled softwood stud, 60% Ret	use softwood stud@100x50mm+ softwood plates@1	100x50 mm = 60% x 33		
	Reuse recycled aggregate for brick, 67% (BDA 2014; Tyrell & Goode 2014), 147 kg/m ² (p.127, L 6) x 67% x 0.083 MJ/kg = 8.17 MJ/ m^2					
		• • • •	70((DDA 2014) Trunell & Coode 2014) 147 Ire/m2	(n 127 I 6) n 670/ n		
	Reuseu	the recycled aggregates				

Table A.C.20: Green Star. Potential reduction in carbon emissions (embodied energy) in a timber framed, clay brick veneer wall. Case Study Three (see Lawson 1996, p. 127).

Life Cycle Stages of	C	onstruction	Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emissi	on (Embodied Energy) Reduction	Basic
Measurable energy to		60% softwood stud + softwood plates	561 MJ/m ²
reduce in Implementation		19.8 MJ/m²	501 MJ/III
Measurable energy to		Reuse of softwood 3.64 MJ/ m ²	
reduce in Transportation			
Care an Stan Tatal Wall		23.44 MJ/m ²	561 MJ/ m ²
Green Star, Total Wall	2	23.44 MJ/m ²	501 MJ/ m-

Table A.C.21: Potential reduction in carbon emissions (embodied energy) in a timber framed, stee	1
sheet roof. Case Study Three (see Lawson 1996, p. 133).	

	Potentia	al carbon reduction by this re	search and Green tool	
Building materials and elements	Steel f - Steel f 85.75 M Reuse - Softwi 13.6 M - Using - Use re Constru- - Use re Green f Steel fr Materia reduced - Steel f Reused Materia consum - Softwi - Softwi - Steel f Reused Materia - Steel f - Stee	from average recycled contents sheet from recycled contents {38 MJ/k IJ/m ² ed materials and elements ood trusses from recycled trusses 40% J/m ² recycled trusses = 60% x 34 MJ/m ² = ecycled thermal insulation, 49MJ/kg - 2 lection Information 2014) ecycled thermal insulation = 40 MJ/m ²	t $f_{g} = 20.50 \text{ MJ/Kg} = 17.5 \text{ MJ/Kg}$ $f_{g} = 20.50 \text{ MJ/Kg} = 17.5 \text{ MJ/Kg}$ $f_{g} = 20.50 \text{ MJ/m}^2$ $f_{g} = 20.90 \text{ MJ/kg} \times 0.825 \text{ kg/m}^2 = 17.57$ (Steel Construction Information 20 $f_{g} = 20.50 \text{ MJ/Kg} = 17.5 \text{ MJ/Kg} \times 10.50 \text{ MJ/Kg} = 10.5$	valition 2013) = MJ/m^2 (Steel D14) m 90%, therefore CA 2008) is: 4.9 kg/ m ² x 90% used, post-
	If the m (Thylac Reuse s MJ/toni	sed transportation of waste by reusinaterials come from outside the state, the 2014) 25.2 km) = over 100 km oftwood trusses 11.15(trusses 8.25, banc/km = 5.01 MJ/ m ²	e distance will be (Port Jackson 20	
Transportation	Green Star If the materials come from outside the state, the distance will be (Port Jackson 2014) 297 - (Thylacine 2014) 25.2 km) = over 100 km			
	Reuse softwood trusses 11.15 (trusses 8.25, battens 2.9) kg/m ² /1000 T/m ² x 100 km x 4.5 MJ/tonne/km = 5.01 MJ/ m^2			
	Decreased transportation by localizing the suppliers			
	If materials come from the inside of state, local supplier is Skyline (2014). The saved distance will be (Thylacine 2014) 25.2 km			
	19.99 k	g/m ² (whole roof materials) /1000 T/m	2 x 25.2 km x 4.5 MJtonne/km = 2	.26 MJ/ m ²
Life Cycle Stages of b	uilding	Construct		Embodied
	-	Pre-Construction	Construction	Energy
		Potential reduction in		Basic
Measurable energy to reduce in Building materials and elements		Trusses from recycled timber 40% 13.6 MJ/m ² Steel sheet from recycled content 85.75 MJ/m ²	Use recycled trusses 60% 20.4 MJ/m ² Use recycled thermal insulation = 17.57 MJ/m ²	330MJ/ m ²

			1	
Measurable energy to reduce in Transportation	Decreased transportation by reusing trusses 5.01 MJ / m ²	Decreased transportation by localizing 2.26 MJ/ m²		

Total Roof	104.36 MJ/m ²	40.23 MJ/m ²	330MJ/ m ²	
1 otal Kool	144.59 M.	J/m ²	5501v1J/ III	

Table A.C.22: Green Star. Potential reduction in carbon emissions (embodied energy) in timber framed, steel sheet roof. Case Study Three (see Lawson 1996, p. 133).

Life Cycle Stages of	Construction		Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emission	n (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation	Steel sheet from 90% Recycled contents = 77.17 MJ/m² Trusses from recycled timber 40% 13.6 MJ/m²	Use recycled trusses 55% 18.7 MJ/m ²	330 MJ/m²
Measurable energy to reduce in Transportation	Decreased transportation by reusing trusses 5.01 MJ/ m²		
Green Star, Total Roof	95.78 MJ/m ²	18.7 MJ/m ²	330 MJ/ m ²

Table A.C.23: Potential reduction in carbon emissions (embodied energy) in building system: concrete slab floor, timber framed brick veneer walls, timber framed steel sheet roof. Case Study Three (see Lawson 1996, p. 124).

Life Cycle Stages of building	Const	Embodied Energy	
	Pre-Construction	Construction	
	Potential Carbon I	Emissions to Reduce	Basic
Measurable energy to reduce in building materials and elements	124.19 MJ/m ²	128.16 MJ/m ²	1536 MJ/m ²
Measurable energy to reduce in Implementation	147.2 MJ/m ²	220.83 MJ/m ²	
Measurable energy to reduce in Transportation	139.65 MJ/m ²	57.09 MJ/m ²	
	411.04 MJ/m ²	406.08 MJ/m ²	
Total, building system	817.12 MJ/m2		1536 MJ/m ²

A.C.1.4 Case Study Four – Civil Engineering Laboratory, USQ 2013

Table A.C.24: Potential reduction in carbon emissions (embodied energy) in a 200 mm concrete slab on ground floor. Case Study Four (see Lawson 1996, p. 125).

]	Potential carbon reduction by this research and Green tool					
Building materials and elements	Reused the recycled aggregates for concrete - Concrete from 80% recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083MJ/Kg x (381 kg/m ² concrete – 51.73 kg/m ² cement) x 80% = 21.84 MJ/m ² Steel from average recycled content - Steel mesh +Edge beams from average recycled content = 5.148 Kg x {34 MJ/Kg - 20.10 MJ/Kg} = 71.55 MJ/m ² Green Star Reused recycled aggregate for concrete Material-5 (Green Star Technical Manual) is considered maximum 20%, therefore reduced embodied energy by this credit (Concrete from 20% Recycled aggregate) (GBCA 2008) is: - Concrete from 30% recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (381 kg/m ² concrete – 51.73kg/m ² cement) x 20% = 5.46 MJ/m ² Steel from average recycled content MJ/Kg Steel from average recycled content					
	embodied energy by this credit (Steel from Recycled content) (GBCA 2008) is: 5.148 Kg x 90% { $34 \text{ MJ/Kg} - 20.10 \text{ MJ/Kg}$ } = 64.39 MJ/m²					

Implementation	Decreased and Replaced energy in process Replaced cement Geopolymer concrete or 100% replacement with recycled cement substitute (Nath & Sarker 2014) results 97% reduction in GHG (McLellan et al. 2011) 381kg/m ² x 14% cement (Lawson 1996) 97% = 51.73 kg replaced cement/ m ² in concrete 51.73 kg cement/m2 x 5.6 MJ/kg = 289.68 MJ/ m ²
	Green Star Replacing maximum 60% of cement (GBCA 2008) $381 \text{kg/m}^2 \times 14\%$ cement 60% = 32 kg replaced cement/ m ² in concrete 32 kg cement/m ² x 5.6 MJ/kg = 179.2 MJ/ m ²

Transportation Total Floor	75.04 MJ/m ²	417.35 MJ/m ²	908MJ / m
Transportation			
Transportation			
	by reuse aggregate 53.2 MJ/m^2	56.12 MJ/m^2	
Measurable energy to reduce in	Decreased Energy in transportation	Decreased transportation by localizing	
Measurable energy to reduce ir Implementation		Geopolymer, replacing 100% of cement = 289.68 MJ/m^2	
elements			
Building materials and	aggregate = 21.84 MJ/m^2	recycled content = 71.55 MJ/m^2	908 MJ/m ²
Measurable energy to reduce i		100% Steel mesh, beams from average	Stanualu
		on in carbon emissions	Standard
Life Cycle Stages of building	Pre-Construction	Construction	Energy
Transportation Transportation Transportation	n ² x 44.9 km x 4.5 MJ/ton/km (Lawson reen Star duced transportation by reusing aggrega 9 km x 4.5 MJ/ton/km (Lawson 1996, p creased transportation by localizing s instruction material supplier: BIG Mate he materials come somewhere in Brisba ndscape Supplies, 488 Loganlea Rd, Sla e hypothetically decreased distance will 1kg/m ² concrete +5.148 Kg/m ² steel) /10 12) = 56.12 MJ/m ²	ate, (381concrete -51.73 cement) kg/m ² /l p. 12) x 20% = 13.3 MJ/ m² suppliers Projects, Springfield QLD (BIG Mate 20 ane: acks Creek QLD 4127 (Nuway 2014)	000 T/m ² x 14)

Table A.C.25: Green Star. Potential reduction in carbon emissions (embodied energy) in a 200 mm concrete slab on ground floor. Case Study Four (see Lawson 1996, p. 125).

Co	Embodied	
Pre-Construction	Construction	Energy
Potential Carbon Emissio	on (Embodied Energy) Reduction	Basic
%20Recycled aggregate for	90% Steel mesh from average recycled	908 MJ/m ²
concrete =5.46 MJ/m^2	content 64.39 MJ/m ²	908 MJ/III
	Geopolymer, 60% Cement Replacements	
	179.2 MJ/m ²	
Decreased transportation by		
reuse aggregate 13.3 MJ/m ²		
18.76 MJ/m ²	243.59 MJ/m ²	000 MI/2
26	2.35 MJ/m ²	908 MJ/ m ²
	Pre-Construction Potential Carbon Emission %20Recycled aggregate for concrete =5.46 MJ/m ² Decreased transportation by reuse aggregate 13.3 MJ/m ² 18.76 MJ/m ²	Potential Carbon Emission (Embodied Energy) Reduction %20Recycled aggregate for concrete =5.46 MJ/m ² 90% Steel mesh from average recycled content 64.39 MJ/m ² Geopolymer, 60% Cement Replacements 179.2 MJ/m ² Decreased transportation by reuse aggregate 13.3 MJ/m ²

Table A.C.26: Potential reduction in carbon emissions (embodied energy) in a cored concrete block wall. Case Study Four (Lawson 1996, p. 129)

	Proce	sses where carbon emissions (embodied energy) can be reduced	
	Reused r	ecycled materials as aggregat	e for concrete block	
Building	- Concret 0.083 MJ Saved em	e from 100% recycled aggregat	e (Uche 2008; PCA 2014), embodied en rgy of aggregate 0.083 MJ/Kg x (275 Kg	
materials and elements	Green St Reused r Material- embodied Saved em	ar ecycled materials for concrete 5 (Green Star Technical Manua l energy by this credit (Concrete	e block 1) is considered maximum 20%, therefor e from 20% Recycled aggregate) (GBCA rgy of aggregate 0.083 MJ/Kg x (275 Kg	2008) is:
	Decrease	d and Replaced energy in pro	2291	
Implementation	Replaced Geopolym reduction Reduced	l cement ner concrete block or 100% rep in GHG (Geiger 2010)	lacement with recycled cement substitute ete Block Association 2013) / 1000 x 275	
	Green St Replacing	ar	een building Council of Australia 2008)	
Transportation	Decreased transportation of waste by reusing and recycling If the materials come from inside of state from local supplier, Big Mate Pro (BIG Mate 2014), the saved distance will be 44.9 km Reduced transport for recycled materials for reuse aggregate (275 concrete /1000 T/m2 x 44.9 km x 4.5 MJ/tonne/km = 50.62 MJ/ m² Green Star Reduced transport for Recycled materials for Reuse aggregate (275 concrete		e from local supplier, Big Mate Projects, l be 44.9 km for reuse aggregate (275 concrete – 24.4 m = 50.62 MJ/ m² s for Reuse aggregate (275 concrete – 24	.47 cement) kg/m ²
Decreas Landscap The hypo		d transportation by localizing e Supplies, 488 Loganlea Rd, S thetically decreased distance wi	llacks Creek QLD 4127 (Nuway 2014) ill be 32.3km	
Life Cycle Stages		² /1000 T/m2 x 32.3 km x 4.5 M	$JJtonne/km = 39.9 MJ/m^2$	Embodied Energy
Life Cycle Stages of building		Pre-Construction	Construction on (embodied energy) reduction	Basic
Measurable energy to reduce in Building materials and elements		Use recycled materials as aggregate 20.79 MJ/ m ²		511 MJ/ m²
Measurable energy to Implementation	reduce in		Geopolymer, replacing 100% of cement 137.03 MJ/m²	
Measurable energy to Transportation	reduce in	Decreased transportation by reusing 50.62 MJ/ m²	Decreased transportation by localizing 39.9 MJ/m²	
Total Wal	le	71.41 MJ/ m ²	176.93 MJ/ m2	511MJ/ m ²
	15	248	8.34 MJ/m2	5111vij/ III

 Table A.C.27: Green Star. Potential reduction in carbon emissions (embodied energy) in a cored concrete block wall. Case Study Four (see Lawson 1996, p. 129).

	Stady I our (See Ea mson I)		
Life Cycle Stages of	Construction		Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emissi	on (Embodied Energy) Reduction	Basic
Measurable energy to	%20Recycled aggregate for		511 MJ/m ²
reduce in Implementation	concrete block = 4.15 MJ/m^2		511 MJ/III
Measurable energy to reduce		Geopolymer, 60% Cement Replacements	
in Implementation		82.21 MJ/m ²	
Measurable energy to reduce	Decreased transportation by		
in Transportation	reusing 10.12 MJ/ m ²		
	·		·
Carrow Stern Tedal Wall	14.27 MJ/m ²	82.21 MJ/m ²	511 MJ/
Green Star, Total Wall	9	6.48 MJ/m ²	m ²

Table A.C.28: Potential reduction in carbon emissions (embodied energy) in a steel framed, steel sheet roof. Case Study Four. (Lawson 1996, p. 135).

	Potential carbon reduction by this research and Green tool
	Steel from average recycled content
	- Steel sheet from average recycled content = 5.6 Kg x {38 MJ/Kg (Lawson 1996, p.135) - 20.10 MJ/Kg} = 100.24 MJ/m ²
	 Steel frame roofing from recycled content {38 MJ/Kg - 21.5 MJ/Kg} = 17.5 MJ/Kg x (3.384 + 0.35) kg/ m² = 61.61 MJ/m² Reuse materials and elements Use 40% recycled trusses (UK Indemand 2014), 40% x 3.734 kg/m² x 34 MJ/Kg = 50.78 MJ/m²
Building materials and	- Use recycled thermal insulation, 49MJ/kg - 20.90 MJ/kg x 0.55kg/m ² = 17.57 MJ/m² (Steel Construction Information 2014)
elements	Green Star Steel from average recycled content Material-6 steel (Green Star Technical Manual) is considered maximum 90%, therefore reduced embodied energy by this credit (Steel from 90% Recycled contents) (GBCA 2008) is:
	- Steel sheet from average recycled content = 5.6 Kg x {38 MJ/Kg - 20.10 MJ/Kg} x 90% = 90.21 MJ/m ²
	- Steel frame roofing from recycled content {38 MJ/Kg – 21.5 MJ/Kg} = 17.5 MJ/Kg x (3.384 + 0.35) kg/ m^2 x 90% = 55.44 MJ/m^2
	Decreased transportation of waste by reusing and recycling

	Decreased transportation of waste	by reusing and recycling			
	If the materials come from inside state (BIG Mate 2014), the saved distance will be 44/9 km				
	Reuse recycled trusses 40% x $3.734 \text{ kg/m}^2/1000 \text{ T/m}^2 \text{ x} 44.9 \text{ km x} 4.5 \text{ MJ/tonne/km} = 0.30 \text{ MJ/m}^2$				
Transportation	Decreased transportation by localizing suppliers				
	Landscape Supplies, 488 Loganlea	Rd, Slacks Creek QLD 4127 (Nuway 2014	4) considering the local		
		hetically decreased distance will be $32.3 =$			
	9.334 kg/m ² /1000 T/m2 x 32.3 km x	x 4.5 MJtonne/km (Lawson p. 12) = 1.35 M	J/m^2		
Life Coule Steres	C C	onstruction	Embodied Energy		
Life Cycle Stages building	Pre-Construction	Construction	Basic		
building	Potential carbon emissi	on (embodied energy) reduction			
Measurable energy	to Steel frame from average	Use recycled trusses = 50.78 MJ/m^2			
reduce in Building	recycled contents 61.61 MJ/m ²	Use Recycled insulation = 17.57	401 MJ / m ²		
materials and	Steel Sheet from recycled	MJ/m ²	401 1013/ 111		
elements	contents 100.24 MJ/m ²				
Measurable energy t	o	Decreased transportation by reusing			
reduce in		0.30 MJ/ m ²			
Transportation		Decreased transportation by			
		localizing1.35 MJ/m ²			
Total Roof	161.85 MJ/m ²	70 MJ/m ²			
I Utal KOUL		70 MJ/m ²	401MJ/ m ²		
	<u> </u>	1100 110/11			

East a diad
Embodied
Energy
Basic
401 MJ/m ²
401 MJ/III
401 MJ/ m ²
401 MJ/ III

Table A.C.29. Green Star. Potential reduction in carbon emissions (embodied energy) in a steel parallel chord trussed sheet roof. Case Study Four (see Lawson 1996, p. 135).

Table A.C.30: Potential reduction in carbon emissions (embodied energy) in concrete slab floor, concrete upper floor, concrete block walls, steel framed, steel sheet roof. Case Study Four.

Life Cycle Stages of building	Construction		Embodied
	Pre-Construction	Construction	Energy
	Potential Carbon Er	missions to Reduce	Basic
Measurable energy to reduce in building materials and elements	204.48 MJ/m ²	139.9 MJ/m ²	2570 MJ/m ²
Measurable energy to reduce in Implementation			
weasurable energy to reduce in implementation		426.71 MJ/m ²	
Measurable energy to reduce in Transportation	103.82 MJ/m ²	97.67 MJ/m ²	
	308,30 MJ/m ²	664.28 MJ/m ²	
Total, building system	972.58 MJ/m ²		2570 MJ/m ²

A.C.1.5 Case Study Five – Olympics Velodrome Building, London 2012

Table A.C.31: Potential reduction in carbon emissions (embodied energy) in a 200 mm hollow coreprecast concrete slab floor. Case Study Five (Lawson 1996, p. 125).

381 kg 51.73 l Green Replac 381kg 32 kg (Decrea Transp be ove (297 + 125.87 Green (297 + 31.47 l Impro 63% tr 386.14 Energ Mod Roac Rail Ship Sour- building educe in t	ym2 x 14% cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/r kg cement/m2 x 5.6 MJ/kg = 289.74 MJ/ m ² Reduced Embodied EnergyStaring maximum 60% of cement (GBCA 2008) (m2 x 14% Cement x 60% = 32 kg replaced cement/m2 in concrete Cement/m2 x 5.6 MJ/kg = 179.2 MJ/ m ² ased transportation of waste by reusing and recycling out of material, one stop supplier. If the materials come from London, the sar r 100 km (Aggregate Industries 2014) $5.148 + 84$) 386.14 kg/m ² x 80% /1000 T/m ² x 100 km x 4.5 - (0.6 +0.25) /2 ' MJ/ m ² Star $5.148 + 84$) 386.14 kg/m ² x 20% /1000 T/m ² x 100 km x 4.5 - (0.6 +0.25) /2 ' MJ/ m ² wed and Replaced Renewable energy in transportation ransported by rail or water (London Olympics 2012) 18 kg/m2 /1000 T/m2 x 100 km = 157.3 MJ/ton/km x 63% = 99.1 MJ/M2 Tr y consumption e e Energy Consumption (MJtonne/km) UK 1 4.50 0.25 ce: Lawson (1996, p. 12)Construction Pre-Construction Pre-Construction Pre-Construction Pre-Construction Pre-Construction Pre-Construction	ved distance will } MJ/ton/km = } MJ/ton/km =				
381 kg 51.73 l Green Replac 381kg 32 kg (Decrea Transp be ove (297 + 125.87 Green (297 + 31.47 l Impro 63% tr 386.14 Energ Mod Roac Rail Ship Sour- building educe in t	ym2 x 14% cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/r kg cement/m2 x 5.6 MJ/kg = 289.74 MJ/m ² Reduced Embodied Energy . Star ring maximum 60% of cement (GBCA 2008) /m2 x 14% Cement x 60% = 32 kg replaced cement/m ² in concrete Cement/m2 x 5.6 MJ/kg = 179.2 MJ/m ² ased transportation of waste by reusing and recycling bort of material, one stop supplier. If the materials come from London, the sar r 100 km (Aggregate Industries 2014) $5.148 + 84$) 386.14 kg/m ² x 80% /1000 T/m ² x 100 km x 4.5 - (0.6 +0.25) /2 ' MJ/ m ² Star Star Stat Stat Stat Stat 15.148 + 84) 386.14 kg/m ² x 20% /1000 T/m ² x 100 km x 4.5 - (0.6 +0.25) /2 MJ/ m ² wed and Replaced Renewable energy in transportation ansported by rail or water (London Olympics 2012) $8 kg/m2 /1000 T/m2 x 100 km = 157.3 MJ/ton/km x 63% = 99.1 MJ/M2 Try consumption(MJtonne/km) UK1 4.500.600.25ce: Lawson (1996, p. 12)ConstructionPre-ConstructionPre-ConstructionM30Recycled aggregate forconcrete 21.84 MJ/m2Geopolymer 100% Cement Replacement289.74 MJ/m2Decreased transportation byReplaced Energy in transportation$	<pre>ved distance will } MJ/ton/km = } MJ/ton/km = ansportation Embodied Energy Basic</pre>				
381 kg 51.73 l Green Replac 381kg 32 kg (Decrea Transp be ove (297 + 125.87 Green (297 + 31.47 l Impro 63% tr 386.14 Energ Mod Roac Rail Ship Sour- building educe in t	ym2 x 14% cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/rkg cement/m2 x 5.6 MJ/kg = 289.74 MJ/ m 2 Reduced Embodied EnergyStarsing maximum 60% of cement (GBCA 2008)/m2 x 14% Cement x 60% = 32 kg replaced cement/ m2 in concreteCement/m2 x 5.6 MJ/kg = 179.2 MJ/ m2 ased transportation of waste by reusing and recyclingbort of material, one stop supplier. If the materials come from London, the sarr 100 km (Aggregate Industries 2014)5.148 + 84) 386.14 kg/m² x 80% /1000 T/m² x 100 km x 4.5 - (0.6 +0.25) /2/ MJ/ m²Star5.148 + 84) 386.14 kg/m² x 20% /1000 T/m² x 100 km x 4.5 - (0.6 +0.25) /2/ MJ/ m²wed and Replaced Renewable energy in transportationansported by rail or water (London Olympics 2012)// kg/m2 /1000 T/m2 x 100 km = 157.3 MJ/ton/km x 63% = 99.1 MJ/M2 Tr y consumptioneEnergy Consumption(MJ tonne/km) UK144.500.600.25ce: Lawson (1996, p. 12)ConstructionPotential Carbon Emission (Embodied Energy) Reduction%30Recycled aggregate for concrete 21.84 MJ/m2Geopolymer 100% Cement Replacement 28.74 MJ/m2	<pre>ved distance will } MJ/ton/km = } MJ/ton/km = ansportation Embodied Energy Basic</pre>				
381 kg 51.73 l Green Replac 381kg 32 kg (Decrea Transp be ove (297 + 125.87 Green (297 + 31.47 l Impro 63% tr 386.14 Energ Mod Roac Rail Ship Sour	y/m2 x 14% cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/r kg cement/m2 x 5.6 MJ/kg = 289.74 MJ/ m ² Reduced Embodied EnergyStaring maximum 60% of cement (GBCA 2008) (m2 x 14% Cement x 60% = 32 kg replaced cement/ m ² in concrete Cement/m2 x 5.6 MJ/kg = 179.2 MJ/ m ² ased transportation of waste by reusing and recycling oort of material, one stop supplier. If the materials come from London, the sar r 100 km (Aggregate Industries 2014)5.148 + 84) 386.14 kg/m ² x 80% /1000 T/m ² x 100 km x 4.5 - (0.6 +0.25) /2 / MJ/ m ² Star 5.148 + 84) 386.14 kg/m ² x 20% /1000 T/m ² x 100 km x 4.5 - (0.6 +0.25) /2 / MJ/ m ² wed and Replaced Renewable energy in transportation ransported by rail or water (London Olympics 2012) 18 kg/m2 /1000 T/m2 x 100 km = 157.3 MJ/ton/km x 63% = 99.1 MJ/M2 Tr y consumption eeEnergy Consumption (MJtonne/km) UK 114.50 0.60 0.25ce: Lawson (1996, p. 12)Construction Pre-ConstructionPre-Construction Of the full Carbon Emission (Embodied Energy) Reduction %30Recycled aggregate for%30Recycled aggregate for	<pre>ved distance will } MJ/ton/km = } MJ/ton/km = ansportation Embodied Energy Basic</pre>				
381 kg 51.73 l Green Replac 381kg 32 kg (Decrea Transp be ove (297 + 125.87 Green (297 + 31.47 l Impro 63% tr 386.14 Energ Mod Road Rail Ship Sourr	ym2 x 14% cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/r kg cement/m2 x 5.6 MJ/kg = 289.74 MJ/m² Reduced Embodied EnergyStaring maximum 60% of cement (GBCA 2008)'m2 x 14% Cement x 60% = 32 kg replaced cement/m² in concreteCement/m2 x 5.6 MJ/kg = 179.2 MJ/m²ased transportation of waste by reusing and recyclingoot of material, one stop supplier. If the materials come from London, the sarr 100 km (Aggregate Industries 2014)5.148 + 84) 386.14 kg/m²x 80% /1000 T/m² x 100 km x 4.5 - (0.6 +0.25) /2'MJ/m²Star5.148 + 84) 386.14 kg/m² x 20% /1000 T/m² x 100 km x 4.5 - (0.6 +0.25) /2'MJ/m²ved and Replaced Renewable energy in transportationransported by rail or water (London Olympics 2012)*8 kg/m2 /1000 T/m2 x 100 km = 157.3 MJ/ton/km x 63% = 99.1 MJ/M2 Try consumptioneEnergy Consumption(MJtonne/km) UK14.500.600.25ce: Lawson (1996, p. 12)ConstructionPre-ConstructionConstructionPre-ConstructionConstruction	ved distance will MJ/ton/km = MJ/ton/km = ansportation Embodied Energy				
381 kg 51.73 l Green Replac 381kg 32 kg 0 Decree Transp be ove (297 + 31.47 l Impro 63% tr 386.14 Energ Mod Roac Rail Ship Sour	$y'm2 x 14\% \text{ cement (Lawson 1996, p. 41) 97\% = 51.73 kg replaced cement/r kg cement/m2 x 5.6 MJ/kg = 289.74 MJ/m2 Reduced Embodied Energy Star Star Sing maximum 60% of cement (GBCA 2008) y'm2 x 14\% \text{ Cement x } 60\% = 32 \text{ kg replaced cement/m}^2 \text{ in concrete} Cement/m2 x 5.6 MJ/kg = 179.2 MJ/m2 ased transportation of waste by reusing and recycling bort of material, one stop supplier. If the materials come from London, the save r 100 km (Aggregate Industries 2014) 5.148 + 84) 386.14 kg/m2 x 80% /1000 T/m2 x 100 km x 4.5 - (0.6 +0.25) /2 'MJ/m2 Star 5.148 + 84) 386.14 kg/m2 x 20% /1000 T/m2 x 100 km x 4.5 - (0.6 +0.25) /2 'MJ/m2 wed and Replaced Renewable energy in transportation ransported by rail or water (London Olympics 2012) 18 kg/m2 /1000 T/m2 x 100 km = 157.3 MJ/ton/km x 63\% = 99.1 MJ/M2 Tr y consumption e Energy Consumption (MJtonne/km) UK 1 4.50 0.60 0.25 ce: Lawson (1996, p. 12) Construction$	ved distance will MJ/ton/km = MJ/ton/km = ansportation				
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381 kg 51.73 l Green Replac 381kg 32 kg (Decree Transp be ove (297 + 125.87 Green (297 + 31.47 l Impro 63% tr 386.14 Energ Mod Roac Rail	$x'm^2 x 14\%$ cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/r kg cement/m2 x 5.6 MJ/kg = 289.74 MJ/m² Reduced Embodied EnergyStarsing maximum 60% of cement (GBCA 2008) $m^2 x 14\%$ Cement x 60% = 32 kg replaced cement/m² in concreteCement/m2 x 5.6 MJ/kg = 179.2 MJ/m² ased transportation of waste by reusing and recyclingoort of material, one stop supplier. If the materials come from London, the sarr 100 km (Aggregate Industries 2014)5.148 + 84) 386.14 kg/m²x 80% /1000 T/m²x 100 km x 4.5 - (0.6 +0.25) /2MJ/m²Star5.148 + 84) 386.14 kg/m² x 20% /1000 T/m² x 100 km x 4.5 - (0.6 +0.25) /2MJ/ m²wed and Replaced Renewable energy in transportationansported by rail or water (London Olympics 2012)8 kg/m2 /1000 T/m2 x 100 km = 157.3 MJ/ton/km x 63% = 99.1 MJ/M2 Tr y consumptioneEnergy Consumption(MJtonne/km) UK14<.50	ved distance will } MJ/ton/km = } MJ/ton/km =				
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381 kg 51.73 l Green Replac 381kg 32 kg (Decree Transp be ove (297 + 125.87 Green (297 + 31.47 l	y/m2 x 14% cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/ r kg cement/m2 x 5.6 MJ/kg = 289.74 MJ/ m ² Reduced Embodied Energy Star ing maximum 60% of cement (GBCA 2008) /m2 x 14% Cement x 60% = 32 kg replaced cement/ m ² in concrete Cement/m2 x 5.6 MJ/kg = 179.2 MJ/ m² ased transportation of waste by reusing and recycling out of material, one stop supplier. If the materials come from London, the sar r 100 km (Aggregate Industries 2014) 5.148 + 84) 386.14 kg/m ² x 80% /1000 T/m ² x 100 km x 4.5 – (0.6 +0.25) /2 / MJ/ m ² Star 5.148 + 84) 386.14 kg/m ² x 20% /1000 T/m ² x 100 km x 4.5 – (0.6 +0.25) /2 / MJ/ m ²	ved distance will } MJ/ton/km =				
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381 kg 51.73 J Green Replac 381kg/ 32 kg 0 Decree Transp be ove (297 + 125.87	y/m2 x 14% cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/ r kg cement/m2 x 5.6 MJ/kg = 289.74 MJ/ m ² Reduced Embodied Energy Star ing maximum 60% of cement (GBCA 2008) /m2 x 14% Cement x 60% = 32 kg replaced cement/ m ² in concrete Cement/m2 x 5.6 MJ/kg = 179.2 MJ/ m ² ased transportation of waste by reusing and recycling out of material, one stop supplier. If the materials come from London, the sav r 100 km (Aggregate Industries 2014) 5.148 + 84) 386.14 kg/m ² x 80% /1000 T/m ² x 100 km x 4.5 – (0.6 +0.25) /2 / MJ/ m ²	ved distance will				
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381 kg 51.73 l Green Replac 381kg 32 kg	<pre>z/m2 x 14% cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/ r kg cement/m2 x 5.6 MJ/kg = 289.74 MJ/ m² Reduced Embodied Energy Star sing maximum 60% of cement (GBCA 2008) /m2 x 14% Cement x 60% = 32 kg replaced cement/ m² in concrete Cement/m2 x 5.6 MJ/kg = 179.2 MJ/ m² ased transportation of waste by reusing and recycling</pre>					
381 kg 51.73 l Green Replac 381kg/	$x/m^2 x 14\%$ cement (Lawson 1996, p. 41) $97\% = 51.73$ kg replaced cement/r kg cement/m ² x 5.6 MJ/kg = 289.74 MJ/ m² Reduced Embodied Energy Star sing maximum 60% of cement (GBCA 2008) /m ² x 14% Cement x 60% = 32 kg replaced cement/ m ² in concrete					
381 kg 51.73 l Green Replac	t/m2 x 14% cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/r kg cement/m2 x 5.6 MJ/kg = 289.74 MJ/ m² Reduced Embodied Energy Star sing maximum 60% of cement (GBCA 2008)					
381 kg 51.73 l Green	$y/m^2 x 14\%$ cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/r kg cement/m ² x 5.6 MJ/kg = 289.74 MJ/m² Reduced Embodied Energy Star					
381 kg	$y/m2 \times 14\%$ cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/ r					
		381 kg/m2 x 14% cement (Lawson 1996, p. 41) 97% = 51.73 kg replaced cement/m ² in concrete 51.73 kg cement/m ² x 5.6 MI/kg = 289.74 MI/m² Reduced Embodied Energy				
results 97% reduction in GHG (McLellan et al. 2011)						
	ased and replaced energy in reduced cement lymer concrete or 100% replacement with recycled cement substitute (Nath a	& Sarker 2014)				
embod	lied energy by this credit (Steel from Recycled content) (GBCA 2008) is:					
		efore reduced				
51.73k	rg/m^2 cement) x 20% = 5.46 MJ/m²					
		² concrete –				
- Conc	rete from 20% recycled aggregate (Uche 2008PCA) 2014) embodied energy					
		4 6				
- Steel = 71.5	mesh +Edge beams from average recycled content = 5.148 Kg x {34 MJ/Kg 5MJ/m ²	- 20.10 MJ/Kg}				
Steel f	rom average recycled content	20 10 MUR				
) x (381				
0.083	MJ/Kg					
- Conc	d the recycled aggregates for concrete rete from 80% Recycled aggregate (Uche 2008: PCA 2014) embodied energy	v of aggregate is				
.0 11001	Potential carbon reduction by this research and Green tool					
	Reuse - Conc 0.083 Saved kg/m ² c Steel f - Steel = 71.5 Green Materi reduce - Conc 0.083 Saved 51.73k Steel f Materi embod 5.148	Reused the recycled aggregates for concrete - Concrete from 80% Recycled aggregate (Uche 2008; PCA 2014) embodied energy 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (297 + 84) kg/m ² concrete – 51.73kg/m ² cement) x 80% = 21.84 MJ/m² Steel from average recycled content - Steel mesh +Edge beams from average recycled content = 5.148 Kg x {34 MJ/Kg = 71.55MJ/m² Green Star, reused recycled aggregates for concrete Material-5 (Green Star Technical Manual, Materials) is considered maximum 20%, reduced embodied energy by this credit (Concrete from 20% Recycled aggregate) (- Concrete from 20% recycled aggregate (Uche 2008PCA) 2014) embodied energy 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (381kg/m ² 51.73kg/m ² cement) x 20% = 5.46 MJ/m² Steel from average recycled content Material-6 (Green Star Technical Manual) Steel is considered maximum 60%, there embodied energy by this credit (Steel from Recycled content) (GBCA 2008) is: 5.148 Kg x 90% {34 MJ/Kg - 20.10 MJ/Kg} = 64.40 MJ/m²				

Table A.C.32: Green Star. Potential reduction in carbon emissions (embodied energy) in a 200 mm hollow core precast concrete slab floor. Case Study Five (Lawson 1996, p. 125).

Life Cycle Stages of	Co	onstruction	Embodied
building	Pre-Construction	Construction	Energy
	Potential reduction in Carl	bon Emissions (Embodied Energy)	Basic
Measurable energy to	20% Recycled aggregate for	90% Steel mesh from average recycled	908 MJ/m ²
reduce in Implementation	$concrete = 5.46 \text{ MJ/m}^2$	content 64.4 MJ/m ²	
Measurable energy to reduce		Geopolymer, 60% Cement Replacement	
in Implementation		179.2 MJ/m ²	
Measurable energy to reduce	Decreased transportation by		
in Transportation	reuse aggregate 31.47 MJ/m²		
Crean Stan Tatal Floor	36.93 MJ/m ²	243.6 MJ/m ²	908 MJ/ m ²
Green Star, Total Floor	28	0.53 MJ/m ²	900 NJ/ m

Table A.C.33: Potential reduction in carbon emissions (embodied energy) in a 125 mm eleva	ated
concrete upper floor. Case Study Five (see Lawson 1996, p. 124).	

Life Cycle Stages of Measurable energy to n Building materials an elements Measurable energy to re Implementation Measurable energy to re Transportation	reduce in deduce in	Pre-Construction Potential Carbon Emissions (Em 30% Recycled aggregate for concrete 17.20 MJ/m ² Decreased transportation by reusing 97.78 MJ/m ² 114.98 MJ/m ² 521.35 MJ	Steel mesh from average recycled content 99.38MJ/m² Use of 40% Fly ash mix = 228.14 MJ/m² Replaced Energy in transportation 78.85 MJ/m² 406.37 MJ/m²	Embodied Energy Standard 750MJ/m ²		
Measurable energy to r Building materials an elements Measurable energy to re Implementation Measurable energy to re	reduce in deduce in	Potential Carbon Emissions (Em 30% Recycled aggregate for concrete 17.20 MJ/m ² Decreased transportation by reusing 97.78	bodied Energy) to Reduce Steel mesh from average recycled content 99.38MJ/m ² Use of 40% Fly ash mix = 228.14 MJ/m ² Replaced Energy in	Energy Standard		
Measurable energy to r Building materials an elements Measurable energy to re Implementation	reduce in deduce in	Potential Carbon Emissions (Em 30% Recycled aggregate for concrete 17.20 MJ/m ²	bodied Energy) to Reduce Steel mesh from average recycled content 99.38MJ/m ² Use of 40% Fly ash mix = 228.14 MJ/m ²	Energy Standard		
Measurable energy to a Building materials an	reduce in	Potential Carbon Emissions (Em 30% Recycled aggregate for concrete	bodied Energy) to Reduce Steel mesh from average	Energy Standard		
		Potential Carbon Emissions (Em	bodied Energy) to Reduce	Energy		
Life Cycle Stages of	building			Energy		
Life Cycle Stages of	building	D C				
		Construction		Embodied		
		Lawson (1996, p. 12)	1			
	Ship	0.25				
	Rail	0.60				
	Road	(MJtonne/km) UK 4.50				
	Mode	Energy Consumption				
		rtation Energy consumption by type of t				
		sported by rail or water (London Olympics $kg/m^2/1000 T/m^2 x 100 km \{4.5 - (0.6 + 0.6)\}$		/m2 Reduced		
Transportation	-	1 80	1			
	Aggregate 300 kg/m ² x 20% /1000 T/m ² x 100 km x { $(4.5 - (0.6 + 0.25) / 2$ } MJ/ton/km = 24.45 MJ/ m ² Improved and Replaced Renewable energy in transportation					
	Waste materials have been brought from inside of state, therefore the saved energy is at least: $200 h x/z^2 = 200^{6} / 1000 T/z^2 = 100 h x = ((4.5 - (0$					
	Green Star					
	Aggregate $300 \text{kg/m}^2 \times 80\% / 1000 \text{ T/m}^2 \times 100 \text{ km} \times \{(4.5 - (0.6 + 0.25) / 2) \text{ MJ/ton/km} = 97.78 \text{ MJ/ m}^2$					
		terials have been brought from inside of state,				
		d transportation of waste by reusing and re				
		8				
	0	$2 \times 14\%$ Cement x 60% = 25.2 kg replaced ement/m2 x 5.6 MJ/kg = 141.12 MJ/ m²	cement/ m ² in concrete			
	Replacing maximum 60% of cement (GBCA 2008)					
	Green S					
Implementation		2 x 14% Cement x 97% = 40.74 kg replace cement/m2 x 5.6 MJ/kg = 228.14 MJ/m²	d cement/ m ² in concrete			
	97% redu	action in GHG (McLellan et al. 2011)	×			
		d cement mer concrete or 100% replacement by recy	cled cement substitute (Nath & Sarke	r 2014) results i		
		ed and replaced energy in process				
	7.15 Kg	$x 90\% {34 MJ/Kg - 20.10 MJ/Kg} = 89.44$	NJ/m²			
		d energy by this credit (Steel from Recycled				
	Material	6 (Green Star Technical Manual, Steel) is a		reduced		
	MJ/m ² Steel fro	m average recycled content				
	MJ/Kg, s	aved embodied energy = 0.083 MJ/Kg x (3				
		y this credit (Concrete from 20% Recycled from 20% recycled aggregate (Uche 2008;		regate is 0.083		
Building materials and elements	Reused recycled aggregate for concrete Material-5 (Green Star Technical Manual) is considered maximum 20%, therefore reduced embodied					
	Green S Reused					
	- Steel mesh +Edge beams from average recycled content = 7.15 Kg x {34 MJ/Kg - 20.10 MJ/Kg} = 99.38 MJ/m ²					
		m average recycled content	optent = 7.15 Kg v /34 MI/Kg - 20.10	$MI/K_{0} = 003$		
		cement) x 80% =17.20 MJ/m^2				
	MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 $MJ/Kg \times (300 \text{ Kg concrete} - 40.74 \text{ kg})$					
		te from 80% recycled aggregate (Uche 200	8: PCA 2014), embodied energy of as	gregate is 0.08		
	Reused	recycled aggregate for concrete				
		Potential carbon reduction by this resear	rch and Green tool			

 Table A.C.34: Green Star. Potential reduction in carbon emissions (embodied energy) in 125 mm

 elevated concrete upper floor. Case Study Five (see Lawson 1996, p. 124)

Co	Embodied	
Pre-Construction	Construction	Energy
Potential Carbon Emissio	on (Embodied Energy) Reduction	Basic
20% Recycled aggregate for	90% Steel mesh from average recycled	750 MJ/m ²
concrete = 4.30 MJ/m^2	content 89.44 MJ/m ²	/50 MJ/III
	Geopolymer, 60% Cement Replacement	
	141.12 MJ/m ²	
Decreased transportation by		
reuse aggregate 24,45MJ/m ²		
28.75 MJ/m ²	230.56 MJ/m ²	750 MJ/ m ²
25	9.31 MJ/m ²	/50 MJ/ m ²
	Pre-Construction Potential Carbon Emissio 20% Recycled aggregate for concrete = 4.30 MJ/m ² Decreased transportation by reuse aggregate 24,45MJ/m ² 28.75 MJ/m ²	Potential Carbon Emission (Embodied Energy) Reduction 20% Recycled aggregate for concrete = 4.30 MJ/m ² 90% Steel mesh from average recycled content 89.44 MJ/m ² Geopolymer, 60% Cement Replacement 141.12 MJ/m ² Decreased transportation by reuse aggregate 24,45MJ/m ²

Table A.C.35: Potential reduction in carbon emissions (embodied energy) in a cored concrete block wall. Case Study Five (see Lawson 1996, p. 129).

Measurable energy to r	educe Decr	reased transportation by reusing	Replaced Energy in transportation 76.90 MJ/m²			
Measurable energy to reduce in Implementat	tion		Geopolymer, replacing 100% of cement 137.03 MJ/m2			
Measurable energy to reduce in Building materials and elemer	20.7	00% recycled aggregates 9 MJ/ m ²		511 MJ / m ²		
~		Potential Carbon Emission (Er	nbodied Energy) Reduction	Standard		
building		Pre-Construction	Construction	Energy		
Life Cycle Stages		Construc	tion	Embodied		
		0.25 awson (1996, p. 12)				
	Rail Ship	0.60 0.25				
	Road	4.50				
	Mode	Energy Consumption (MJtonne/km) UK				
	Reduced '	Fransportation Energy consum	ption by type of transportation			
-		ported by rail or water (London C $/m^2/1000 T/m^2 x 100 km \{4.5 - ($	Olympics 2012) 0.6 +0.25) /2} MJton/km x %63 = 76	5.90 MJ/m ²		
Transportation	Improved	and replaced renewable energ				
	Decreased transportation of waste by reusing and recycling If materials come from London, the saved distance will be over 100 km Reuse aggregate (275 concrete – 24.47 cement) kg.m ² x 20% /1000 T/m ² x 100 km x 4.5 – {(0.6 +0.25) / 2} MJtonne/km = 20 41 MJ/ m²					
	2} MJtonne/km = 102.09 MJ/ m ² Green Star					
	Reuse agg	regate (275 concrete - 24.47 cem	ent) kg.m ² /1000 T/m ² x 100 km x 4.5	5 - {(0.6 +0.25) /		
		Decreased transportation of waste by reusing and recycling If materials come from London, the saved distance will be over 100 km				
	Decreased	l transportation of waste by reu	sing and recycling			
		$ement/m2 \ge 60\% \ge 5.6 \text{ MJ/kg} = 8$				
	Green Sta					
<u>F</u>	Kg/m ² Reduced F	Portland cement 24.47 Kg/ m ² x 5	.6 MJ/kg = 137.03 MJ/ m ²			
Implementation	Reduced F	e e	Concrete Block Association 2013) /10	000 x 275 = 24.47		
		er concrete block or 100% replac in GHG (Geiger 2010)	ement recycled cement substitute res	ults in 80%		
	Replaced					
		,	-			
	Saved emb		om 20% Recycled aggregate) (GBCA v of aggregate 0.083 MJ/Kg x (275 K			
elements	Material-5		s considered maximum 20%, therefore			
materials and	Green Sta	ır				
Building	Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (275 Kg concrete $- 24.47$ kg cement) = 20.79 MJ/m²					
	- Concrete from 100% recycled aggregate (Uche 2008; PCA) 2014), embodied energy of aggregate is 0.083 MJ/Kg					
				c		

Table A.C.36: Potential reduction in carbon emissions (embodied energy) in a cored concrete block wall. Case Study Five (see Lawson 1996, p. 129).

Life Cycle Stages of	Co	onstruction	Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	on (Embodied Energy) Reduction	Basic
Measurable energy to	20% Recycled aggregate and		
reduce in Implementation	60% replaced cement for		511 MJ/m ²
_	concrete block = 4.15 MJ/m^2		
Measurable energy to		Geopolymer, replacing 60% of cement	
reduce in Implementation		82.21 MJ/m ²	
Measurable energy to reduce	Decreased transportation by		
in Transportation	reusing 20 41 MJ/m ²		
Carrow Sterry Tedal Wall	24.56 MJ/m ²	82.21 MJ/m ²	511 MI/2
Green Star, Total Wall	10	6.77 MJ/m ²	511 MJ/ m ²

Table A.C.37: Potential reduction in carbon emissions (embodied energy) in a steel framed timber weatherboard wall. Case Study Five (see Lawson 1996, p. 129).

	Poten	tial carbon reduction b	y this research a	nd Green tool	
	- Steel fi	om average recycled conte rame from average recycled Kg/ m2 = 46.45 MJ/m2		x 34 MJ/Kg - 20.10 MJ	J/Kg = 3.342 KJ/Kg
		materials and elements (lo			2012)
Building materials and elements	Green Star Steel from average recycled content Material-6 Steel (Green Star Technical Manual) is considered maximum 90%, therefore reduced embodied energy by this credit (Steel from 90% Recycled contents) (GBCA 2008) is: - Steel frame roofing from recycled content {38 MJ/Kg – 21.5 MJ/Kg} = 17.5 MJ/Kg x 3.342 km² x 90% = 55.14 MJ/m² Reused materials and elements (local salvage/re-use centre) Material-8 Timber (Green Star Technical Manual) 95% of all timber products re-used, post-consumer recycled timber or FSC certified timber Reuse softwood + softwood plates + softwood weatherboard = 74 MJ/m² x 95% = 70.3 MJ/m²				
	Decreased transportation of waste by reusing and recycling If materials come from London, the saved distance will be over 100 km 22kg.m ² /1000 T/m ² x 100 km x 4.5 MJtonne/km = 9.89 MJ/ m²				
	Improved and Replaced Renewable energy in transportation				
	63% Transported by rail or water (London Olympics 2012)				
Transportation	$14.32 \text{ kg/m}2 / 1000 \text{ T/m}2 \text{ x} 100 \text{ km} \{4.5 - (0.6 + 0.25) / 2\} \text{ MJton/km x} \%63 = 3.67 \text{ MJ/m}2$				
11 ansportation	Reduced Transportation Energy consumption by type of transportation				
	Mode	Energy Consumption			
		(MJtonne/km) UK			
	Road	4.50			
	Rail Ship	0.60			
		Lawson p. 12 (Lawson 1990)		
Life Cycle Stages) onstruction		Embodied Energy
building		Pre-Construction		ruction	
		Potential Carbon Emissi	n (Embodied Ener	gy) Reduction	Standard
Measurable energy to re in Building materials a elements	y to reduce Steel frame from recycled		Use recycled softwo weatherboard 74 M	+ bod	238 MJ/ m ²
cicinciits					
Measurable energy to re in Transportation		ecreased transportation by use= 9.89 MJ/ m ²	Replaced Energy i 3.67 MJ/m ²	n transportation	
				2	
Total Walls		56.34 MJ/m ²		MJ/m ²	238 MJ/ m ²
i ouri vvano		134.01 MJ/m ²			

Table A.C.38: Green Star. Potential reduction in carbon emissions (embodied energy) in a steel framed timber weatherboard wall. Case Study Five (Lawson 1996).

Life Cycle Stages of	Co	Embodied	
building	Pre-Construction	Energy	
_	Potential Carbon Emissio	Basic	
Measurable energy to reduce in Implementation	Steel frame from 90% Recycled contents = 55.14 MJ/m ²	Use recycled softwood + weatherboard 70.3 MJ/m²	238 MJ/m ²
Green Star, Total Wall	55.14 MJ/m ²	70.3 MJ/m ²	238 MJ/ m ²
Green Star, Totar Wan	125.44 MJ/m ²		230 WIJ/ III

Table A.C.39: Potential reduction in carbon emissions (embodied energy) in a steel framed fabric roof (hemp wrap). Case Study Five (Lawson 1996).

· · · ································	,				
		Potential carbon reduction	by this rese	arch and Green tool	
Building materials and elements	- Steel 65.34 M Reuser - Use 0 make u materia - Use 4 Reduct The Vee curved 2014). - 20% 1 Green Steel f Materia by this - Steel 90% = Reduct Materia	Imaterials and elements f recycled frame and pipes - Velodrome I p the Olympic Stadium's ring beam (Kar uls (Ingenia 2014). 0% recycled trusses (UK Indemand 2014 e Materials use in design elodrome is 50% lighter than Beijing stad cable net design reduced the embodied c reduction in design x 3.734 kg/m ² x 34 M	has high perr rven 2012). 7 4) 40% x 3.7 lium (New S arbon by 27 IJ/Kg (Laws t is considere ts) (GBCA 2 8 MJ/Kg – 2 nical Manuai	centage of recycled content and le The structure involved the use of 2 34 kg/m ² x 34 MJ/Kg (Lawson 19 teel Construction 2010). A materi % compared to a steel arch option on 1996) = 25.39 MJ/m² ed maximum 90%, therefore reduce 008) is: 0.50 MJ/Kg] = 17.5 MJ/Kg x (3.3 1) is considered using 20% less ste	ftover gas pipes 28% recycled 96) = 50.78 MJ/m² ally efficient double- (UK Indemand ed embodied energy 384 + 0.35) kg/ m ² x
	- 20701	conclusion in design x 5.754 kg/m x 54 M	13/ Kg – 20.0	7 1113/111	
	If mate (3.384 m ² Green Decree If mate	ased transportation of waste by re- erials come from London, the saved kg/m ² steel frame + 3.384 x 20% k a Star ased transportation of waste by re- erials come from London, the saved x 20% kg/m ² /1000 T/m ² x 100 km	distance w g/m ²) /100 eusing and distance w	vill be over 100 km 0 T/m ² x 100 km x 4.5 MJton I recycling vill be over 100 km	ne/km = 0.82 MJ /
T		ved and Replaced Renewable energy in			
Transportation	63% Tr 14.32 k Transp Mode Road Rail Ship	ransported by rail or water (London Olym gym² /1000 T/m² x 100 km {4.5 – (0.6 + ortation Energy consumption by type e Energy Consumption (MJtonne/km) UK	npics 2012) 0.25) /2} M	Jton/km x %63 = 2.39 MJ/m² Re	luced
Life Cruele Stears of t	milding		atmastica		Embodied E
Life Cycle Stages of b	ouilding	Con Pre-Construction	struction	Construction	Embodied Energy
Life Cycle Stages of t	ouilding	Pre-Construction Potential Carbon Emission	ı (Embodied	l Energy) Reduction	Embodied Energ
Life Cycle Stages of t Measurable energy to red Building materials and	luce in	Pre-Construction	ı (Embodied		
Measurable energy to red	luce in elements	Pre-Construction Potential Carbon Emission 100% Steel frame from average recycle	ı (Embodied ed	I Energy) Reduction Use recycled elements = 50.78 MJ/m ² 20% reduce steel in design	Standard
Measurable energy to red Building materials and Measurable energy to redu	luce in elements	Pre-Construction Potential Carbon Emission 100% Steel frame from average recycle contents 65.34 MJ/m ²	ı (Embodied ed	I Energy) Reduction Use recycled elements = 50.78 MJ/m ² 20% reduce steel in design 25.39 MJ/m ² Decreased energy by	

 Table A.C.40: Green Star. Potential reduction in carbon emissions (embodied energy) in a steel framed fabric roof (hemp wrap). Case Study Five (see Lawson 1996).

Life Cycle Stages of building	C	Embodied	
	Pre-Construction	Construction	Energy
	Potential Carbon Emission	on (Embodied Energy) Reduction	Basic
Measurable energy to reduce	90% Steel from recycled	20% reduce steel in design 25.39 MJ/m²	282 MJ/m ²
in Implementation	contents 58.8 MJ/m ²		202 IVIJ/III
Measurable energy to reduce in	Decreased transportation by		
Transportation	reduce in design 0.3 MJ/ m ²		
Course Sterr Tetal Deef	59.1 MJ/m ²	25.39 MJ/m ²	282 MJ/ m ²
Green Star, Total Roof	8	4.49 MJ/m ²	282 NJ/ m-

Table A.C.41: Potential reduction in carbon emissions (embodied energy) in concrete slab floor, concrete block walls, steel framed, fabric roof. Case Study Five.

Life Cycle Stages of building	Construction		Embodied
	Pre-Construction	Construction	Energy
	Potential Carbon Emissions (Embodied Energy) to Reduce	Basic
Measurable energy to reduce in Building materials and elements	171.62 MJ/m²	321.10 358.72 MJ/m ²	2689 MJ/m ²
Measurable energy to reduce in Implementation	-	654.91 MJ/m ²	
Measurable energy to reduce in Transportation	336.45 MJ/m ²	260.91 MJ/m ²	
	508.07 MJ/m ²	1236.92 MJ/m ²	2(80 MI/2
Total, building system	1744.99 MJ/m ²		2689 MJ/m ²

A.C.1.6 Case Study Six – Multi Sports Building, USQ 2013

Table A.C.42: Potential reduction in carbon emissions (embodied energy) in a 110 mm concrete slab on ground floor. Case Study Six (Lawson 1996).

		Potential carbon reduction by this re	esearch and Green tool		
Building materials and elements	Reused recycled aggregate for concrete - Concrete from 80% recycled aggregate (Uche 2008; PCA 2014) embodied energy of agg is 0.083 MJ/Kg Saved embodied energy = 0.083 MJ/Kg x (290.4 Kg concrete – 24.38 kg cement) x 80% = MJ/m ² Steel from average recycled content - Steel mesh +Edge beams from average recycled content = 3.882 Kg x {34 MJ/Kg - 20.10 MJ/Kg} = 53.96MJ/m ²				
	Mater emboo - Cond is 0.08 Saved MJ/m Steel Mater emboo	d recycled aggregate for concrete ial-5 (Green Star Technical Manual) i died energy by this credit (Concrete fi crete from 20% recycled aggregate (U 33 MJ/Kg embodied energy = 0.083 MJ/Kg x (rom 20% Recycled aggregate) (GBC Jche 2008; PCA 2014), embodied er 290.4 Kg concrete – 24.38 kg cemen nual) is considered maximum 90%, Recycled content) (GBCA 2008) is	CA 2008) is: hergy of aggregate ht) x 20% = 4.41 therefore reduced	
Implementation	Repla Geopo results 290.4 39.43 Green Repla	ased and Replaced energy in proce ced cement blymer concrete or 100% replacement s 97% reduction in GHG (McLellan e kg/m x 14% Cement x 97% = 39.43 l kg cement/m2 x 5.6 MJ/kg = 220.83 n Star cing maximum 60% of cement (GBC kg/m2 x 14% cement x 60% = 24.38	nt by recycled cement substitute (N t al. 2011) kg replaced cement/ m ² in concrete MJ/ m² A 2008)	ath & Sarker 2014	
	Decre	kg cement/m2 x 5.6 MJ/kg = 136.59 rased transportation of waste by reu materials come from local supplier B	using and recycling	BIG Mate 2014).	
	the sat Reduc	the saved distance will be 44.9 km Reduced transportation by reusing aggregate, 80% x 290.4 kg/m ² /1000 T/m ² x 44.9 km x 4.5 MJ/ton/km = 46.93 MJ/m²			
Transportation		n Star eed transportation by reusing aggregat = = 11.73 MJ/ m ²	te, 290.4 kg/m² /1000 T/m² x 44.9 ki	m x 4.5 MJ/ton/km	
	Local If the Lands The hy (290.4	ased transportation by localizing su construction material supplier is Big materials come from somewhere in B cape Supplies, 488 Loganlea Rd, Slac ypothetically decreased distance will 4kg aggregate, mesh 3.12kg) = 293. MJ/ m²	Mate Projects, Springfield QLD (Bl risbane: cks Creek QLD 4127 (Nuway 2014) be 32.3 = km		
Life cycle stages of building		Constru		Embodied Energy	
		Pre-Construction Potential Carbon Emission (En	Construction mbodied Energy) Reduction	Basic	
		30% Concrete from recycled aggregate =	Steel mesh, beams from average	24010	
Building materials and	ice in	17.65 MJ/m ²	recycled content = 53.96 MJ/m	645MJ/m ²	
Building materials and elements Measurable energy to reduc Implementation Measurable energy to reduc	ce in	17.65 MJ/m ² Decreased transportation by reuse aggregate 46.93 MJ/m ²	recycled content = 53.96 MJ/m Geopolymer, replacing 97% of cement = 220.83 MJ/m ² Decreased transportation by localizing 42.66 MJ/m ²	645MJ/m ²	
Measurable energy to redu Building materials and elements Measurable energy to reduc Implementation Measurable energy to reduc Transportation Total Floor	ce in	Decreased transportation by reuse	Geopolymer, replacing 97% of cement = 220.83 MJ/m ² Decreased transportation by	645MJ/m ²	

 Table A.C.43: Green Star. Potential reduction in carbon emissions (embodied energy) in a 110 mm concrete slab on ground floor. Case Study Six (see Lawson 1996, p. 124).

Co	nstruction	Embodied
Pre-Construction	Construction	Energy
Potential Carbon Emission	n (Embodied Energy) Reduction	Basic
%20 Recycled aggregate for	90% Steel mesh from average recycled	645 MJ/m ²
$concrete = 4.41 \text{ MJ/m}^2$	content 53.95MJ/m²	045 MJ/III
	Geopolymer, 60% Cement	
	Replacements 136.59 MJ/m ²	
Decreased transportation by		
reuse aggregate 11.73 MJ/m ²		
16.14 MJ/m ²	190.54 MJ/m ²	645MJ/ m ²
200	6.68 MJ/m ²	045IVIJ/ M ⁻
	Pre-Construction Potential Carbon Emissio %20 Recycled aggregate for concrete = 4.41 MJ/m ² Decreased transportation by reuse aggregate 11.73 MJ/m ² 16.14 MJ/m ²	Potential Carbon Emission (Embodied Energy) Reduction %20 Recycled aggregate for concrete = 4.41 MJ/m ² 90%Steel mesh from average recycled content 53.95MJ/m ² Geopolymer, 60% Cement Replacements 136.59 MJ/m ² Decreased transportation by reuse aggregate 11.73 MJ/m ²

Table A.C.44: Potential reduction in carbon emissions (embodied energy) in a 125 mm elevated concrete upper floor. Case Study Six (see Lawson 1996, p. 124).

	Processes where carbon emissions (embodied energy) can be reduced
	Reused recycled aggregate for concrete
	- Concrete from 80% recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = 0.083 MJ/Kg x (300 Kg concrete – 40.74kg) (Lawson 1996, p. 125) x 80% = 17.20 MJ/m ²
	Embodied energy of the floor = 497 MJ/m^2 ,
	Carbon emission = 497 MJ/m ² x 0.098 kg CO ² / kg = 48.70 kg CO ² / m ²
	The reduced embodied energy = 17.20 MJ/m ² Reduced carbon emission = 17.20 MJ/m ² x 0.098 kg CO ² / kg = 1.68 kg CO ² / m ² Therefore 4.06% emissions reduction
Building materials	Steel from average recycled content
and elements	- Steel mesh +Edge beams from average recycled content = 7.15 Kg x {34 MJ/Kg (Lawson 1996, p13) - 20.10 MJ/Kg (GreenSpec 201)} = 99.38 MJ/m²
	Green Star Reused recycled aggregate for concrete Material-5 (Green Star Technical Manual) is considered maximum 20%, therefore reduced embodied energy by the credit (Concrete from 20% Recycled aggregate) (GBCA 2008) is: - Concrete from 20% Recycled aggregate (Uche 2008: PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = 0.083 MJ/Kg (Lawson 1996, p. 13) x (300 Kg concrete - 40.74kg) (Lawson 1996, p. 12) x 20% = 4.30 MJ/m ² Steel from average recycled content Material-6 (Green Star Technical Manual) Steel is considered maximum 90%, therefore reduced embodied energy by this credit (Steel from Recycled content) (GBCA 2008) is: 7.15 Kg x 90% {34 MJ/Kg (Lawson 1996, p 13) - 20.10 MJ/Kg (GreenSpec 2015)} = 89.44 MJ/m ²
Implementation	Decreased and Replaced energy in process Replaced cement Geopolymer concrete or 100% replacement with recycled cement substitute (Nath & Sarker 2014) results 97/ reduction in GHG (McLellan et al. 2011) 300kg/m2 (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) 97% = 40.74 kg replaced cement/ m ² in concrete 40.74 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p. 13) = 228.14 MJ/ m ²
	Green Star Replacing maximum 60% of cement (GBCA 2008) 300kg/m2 (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) x 60% = 25.2 kg replaced cement/ m ² in concrete
	25.2 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p.13) = 141.12 MJ/ m²
	Decreased transportation of waste by reusing and recycling
	If the materials come from locally, the saved distance will be 44.9 km
	Reduced transportation by reusing 80% x 307.12 kg/m ² /1000 T/m2 x 44.9 km x 4.5 MJtonne/km (Lawson 1996, p 12) = 49.63 MJ/m²
	Green Star
Transportation	If the materials come from locally, the saved distance will be 44.9 km
1 ransportation	Reduced transportation by reusing 307.12 kg/m ² /1000 T/m ² x 44.9 km x 4.5 MJtonne/km (Lawson 1996, p. 12)

Reduced transportation by reusing 307.12 kg/m² /1000 T/m2 x 44.9 km x 4.5 MJtonne/km (Lawson 1996, p. 12) 20%= 12.41 $MJ/\,m^2$ Decreased transportation by localizing the suppliers Landscape Supplies, 488 Loganlea Rd, Slacks Creek QLD 4127 (Nuway 2014) The hypothetically decreased distance will be 32.3 = km (Nuway 2014) 307.12 kg/m² /1000 T/m2 x 32.3 km x 4.5 MJtonne/km (Lawson 1996, p. 12) = **44.63 MJ/ m²** Embodied Energy Construction Life Cycle Stages of building Pre-Construction Basic Construction Potential carbon emission (embodied energy) reduction Measurable energy to reduce in **Building materials and** 30% Recycled aggregate for Steel mesh from average recycled 750MJ/m² concrete 17.20 MJ/m² content 99.38MJ/m² elements Geopolymer, replacing 100% of cement 228.14 MJ/m² Measurable energy to reduce in **Implementation** Decreased transportation by reusing **49.63 MJ/ m²** Measurable energy to reduce in Decreased transportation by localizing Transportation 44.63 MJ/ m²

66.83 MJ/m² 372.15 MJ/m² 750MJ/m²

Total Floor

Table A.C.45: Green Star. Potential reduction in carbon emissions (embodied energy) in 125 mm

 elevated concrete upper floor. Case Study Six (Lawson 1996, p. 124).

Life Cycle Stages of	Co	nstruction	Embodied		
building	Pre-Construction	Construction	Energy		
	Potential Carbon Emissio	n (Embodied Energy) Reduction	Basic		
Measurable energy to	20% Recycled aggregate for	90%Steel mesh from average recycled	750 MJ/m ²		
reduce in Implementation	concrete 4.30 MJ/m ²	content 89.44MJ/m²	/50 MJ/III		
Measurable energy to reduce		Geopolymer, 60% Cement Replacement			
in Implementation		141.12 MJ/m ²			
Measurable energy to reduce	Decreased transportation by				
in Transportation	reusing 12.41 MJ/m ²				
Green Star, Total elevated	16.71 MJ/m ²	230.56 MJ/m ²	750MJ/ m ²		
Floor	24	7.27 MJ/m ²	/50MJ/ m²		

Table A.C.46: Potential reduction in carbon emissions (embodied energy) in a cored concrete block wall. Case Study Six (Lawson 1996, p. 129)

			ns (embodied energy) can be reduced			
		cycled materials as aggregate				
		from 100% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083				
	MJ/Kg			55105ate 15 01000		
Building			gy of aggregate 0.083 MJ/Kg x (275 Kg concrete	– 24.47 kg		
materials and	Green Sta	awson 1996, p.129) = 20.79 M	IJ/m²			
elements		r cycled materials for concrete	block			
	Material-5	(Green Star Technical Manual) is considered maximum 20%, therefore reduced	embodied energy		
			led aggregate) (GCBA 2008) is: gy of aggregate 0.083 MJ/Kg x (275 Kg concrete	24.47.1.0		
		awson 1996, p. 129) x 20% = 4		– 24.47 Kg		
		· • · ·				
	Decreased Replaced	and replaced energy				
	-		acement recycled cement substitute results in 80%	reduction in GHG		
	(Geiger 20	10)				
Implementation			te Block Association 2013) / 1000 x 275 = 24.47]	Kg/ m ²		
	Green Sta	ement 24.47 Kg/ m ² x 5.6 MJ/kg (Lawson 1996, p.13) = 137.03 MJ/ m²				
		maximum 60% of cement (GB				
	24.47 kg C	ement/m2 x 60% x 5.6 MJ/kg	(Lawson 1996, p. 13) = 82.21 MJ/m^2			
	Decreased	l transportation of waste by	v reusing and recycling			
			er, Big Mate Projects, Springfield QLD (BIG N	Mate 2014), the		
	saved distance will be 44/9 km					
		Reduced transport for Recycled materials for Reuse aggregate (275 concrete – 24.47 cement) kg.m ²				
	Green Sta	n2 x 44.9 km x 4.5 MJ/tonne/km (Lawson 1996, p. 12) = 50.62 MJ / m^2				
Transportation		ransport for Recycled materials for Reuse aggregate (275 concrete – 24.47 cement) kg.m ²				
		$h^{2} x 44.9 \text{ km } x 4.5 \text{ MJ/tonne/km}$ (Lawson 1996, p. 12) x 20% = 10.12 MJ/ m ²				
		d transportation by localizing the suppliers				
		e Supplies, 488 Loganlea Rd, Slacks Creek QLD 4127 (Nuway 2014) thetically decreased distance will be 32.3 km (Nuway 2014)				
			MJtonne/km (Lawson 1996, p. 12) = 39.9 MJ	/ m ²		
Life Cycle Stages	of building		Construction	Embodied		
		Pre-Construction	Construction	Energy		
Maagumahla ananay	to raduce in		ission (embodied energy) to reduce	Basic		
Building materials		Use recycled materials as aggregate 20.79 MJ/ m²		511 MJ/ m ²		
elements	unu			011000		
Measurable energy to Implementation	o reduce in		Geopolymer, replacing 100% of cement 137.03 MJ/m ²			
Measurable energy to	o reduce in	Decreased transportation	Decreased transportation by localizing			
Transportation	o reduce ill	by reusing 50.62 MJ/ m²	39.9 MJ/m²			
	•	71.41 MJ/ m ²	176.93 MJ/ m2	7113 / 11 / 2		
Total Wal	IS		248.34 MJ/m2	511MJ/ m ²		

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Table A.C.47: Green Star. Potential reduction in carbon emissions	(embodied energy) in a cored
concrete block wall. Case Study Six (Lawson 1996, p. 129).	

	.48 MJ/m ²	511 MJ/ m ²
14.27 MJ/m ²	82.21 MJ/m ²	
reusing 10.12 MJ/ m ²		
	Replacements 82.21 MJ/m ²	
	Geopolymer 60% Cement	
-		
concrete block 4.15 MJ/m ²		311 WIJ/III
20% Recycled aggregate for		511 MJ/m ²
Potential Carbon Emission	Basic	
Pre-Construction	Construction	Energy
Construction		Embodied
	Co Pre-Construction Potential Carbon Emissio 20% Recycled aggregate for concrete block 4.15 MJ/m ² Decreased transportation by reusing 10.12 MJ/ m ²	Pre-Construction Construction Potential Carbon Emission (Embodied Energy) Reduction 20% Recycled aggregate for concrete block 4.15 MJ/m ² Geopolymer 60% Cement Replacements 82.21 MJ/m ² Decreased transportation by reusing 10.12 MJ/m ² Geopolymer 60% Cement

Table A.C.48: Potential reduction in carbon emissions (embodied energy) in a steel parallel chord trussed sheet roof. Case Study Six (Lawson 1996, p. 135).

Processes where carbon emissions (embodied energy) can be reduced					
Steel from average recycled content					
	- Steel sheet from average re MJ/Kg = 100.24 MJ/m^2	- Steel sheet from average recycled content = 5.6 Kg x {38 MJ/Kg (Lawson 1996, p.135) - 20.10 MJ/Kg } = 100.24 MJ/m^2			
	17.5 MJ/Kg x (3.384 + 0.35) Reuse materials and element	 Steel frame roofing from recycled content {38 MJ/Kg (Lawson 1996, p. 135) - 21.5 MJ/Kg = 17.5 MJ/Kg x (3.384 + 0.35) kg/ m² = 61.61 MJ/m² Reuse materials and elements Use 40% recycled trusses (UK Indemand 2014), 40% x 3.734 kg/m2 x 34 MJ/Kg = 50.78 			
Building materials	- Use recycled thermal insulation, 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.55kg/m ² = 17.57 MJ/m ² (Steel Construction Information 2014)				
and elements	- Use thermal insulation with recycled contents = 40 MJ/m2 (Steel Construction Information 2014)				
	Green Star				
		cycled content Technical Manual) is considered maximum 90% dit (Steel from 90% Recycled contents) (GBCA	· · · · · · · · · · · · · · · · · · ·		
	- Steel sheet from average re MJ/Kg} x 90% = 90.21 MJ /	- Steel sheet from average recycled content = 5.6 Kg x { 38 MJ/Kg (Lawson 1996, p.135) - 20.10 MJ/Kg} x 90% = 90.21 MJ/m²			
		- Steel frame roofing from recycled content {38 MJ/Kg (Lawson 1996) – 21.5 MJ/Kg} = 17.5 MJ/Kg x ($3.384 + 0.35$) kg/ m ² x 90% = 55.44 MJ/m²			
Transportation	Decreased transportation of waste by reusing and recycling If the materials come from local supplier Big Mate Projects (BIG Mate 2014), the saved distance will be 44/9 km Reuse recycled trusses 40% x 3.734 kg/m ² /1000 T/m ² x 44.9 km x 4.5 MJ/tonne/km (Lawson 1886, p. 12) = 0.30 MJ/ m²				
Tansportation	Decreased transportation b	ov localizing suppliers			
	Landscape Supplies, 488 Lo local supplier (BIG Mate 20	Landscape Supplies, 488 Loganlea Rd, Slacks Creek QLD 4127 (Nuway 2014), considering the local supplier (BIG Mate 2014), the hypothetically decreased distance will be 32.3km $9.334 \text{ kg/m}^2/1000 \text{ T/m}2 \times 32.3 \text{ km} \times 4.5 \text{ MJtonne/km}$ (Lawson 1996, p. 12) = 1.35 MJ/ m ²			
Life Cycle		Construction Embodied Energy			
Stages of	Pre-Construction	Construction	Basic		
building		sion (embodied energy) to reduce			
Measurable energy to reduce in Building	Steel frame from average recycled content 61.61 MJ/m² Steel Sheet from recycled	Use Recycled insulation = 17.57 MJ/m ² Use Recycled insulation = 17.57 MJ/m ²	401 MJ/ m ²		
materials and elements	content 100.24 MJ/m ²				
Measurable energy		Decreased transportation by reusing 0.30 MJ/ m ²			
to reduce in Transportation		MJ/ m ² Decreased transportation by localizing1.35 MJ/m ²			
Total Roof	161.85 MJ/m ²	70 MJ/m ²	401N41/ ²		
	2	31.85 MJ/m ²	401MJ/ m ²		

 Table A.C.49: Green Star. Potential reduction in carbon emissions (embodied energy) in a steel parallel chord trussed sheet roof. Case Study Six (Lawson 1996, p. 135).

	Et loon Case Staal Shi (Ba	······································	
Life Cycle Stages of	Construction		Embodied
building	Pre-Construction Construction		Energy
	Potential Carbon Emission	Basic	
Measurable energy to	Steel sheet from 90% Recycled		
reduce in Implementation	contents = 90.21 MJ/m^2		401 MJ/m ²
_	Steel frame from 90% Recycled		401 WIJ/III
	contents = 55.44 MJ/m^2		
Croop Stor Total Doof	145.65 MJ/m ²		401 MJ/ m ²
Green Star, Total Roof	145.65 MJ/m ²		401 MJ/ m ⁻

Table A.C.50: Potential reduction in carbon emissions (embodied energy) in concrete slab floor, concrete upper floor; concrete block walls, steel parallel chord trussed roof. Case Study Six.

	Construction		Embodied Energy	
Life Coule Sterrer of huilding	Pre-Construction	Construction	Basic	
Life Cycle Stages of building	Potential Carbon Emissions (Embodied Energy) reduction			
Measurable replaced and saved energy in Building materials and elements	217.49 MJ/m ²	221.69 MJ/m ²	2307 MJ/m ²	
Measurable replaced and saved energy in Implementation		586 MJ/m ²		
Measurable replaced and saved energy in Transportation	147.18 MJ/ m ²	128.84 MJ/m ²		
	364.67 MJ/m ²	936.53 MJ/m ²		
Total, building system	1301.20 MJ/m ²		2307 MJ/m ²	

A.C.1.7 Implemented Calculations (example)

Olympic Velodrome Building, London 2012. Case Study Five

The following are calculations of the implemented embodied energy and generated carbon emissions for the main building elements (floor, wall and roof) of Case Study Five. These are based on the actual bioclimatic conditions achieved during the construction process, as presented in the following table.

Olympic Velodrome Building, London 2012	Bioclimatic conditions		
	Reuse, recycle material resources; Localise suppliers and reduce transport		
	Aggregates for concrete	80 per cent recycled aggregate was used in the concrete (Ingenia 2014)	
	Steel and steel mesh	100 per cent steel and steel mesh was used from average recycled content (Steel Construction Information 2014)	
	Reduce material use in design	Reduced materials in structural design 50 per cent	
Source: London Olympics (2012)	Reuse construction materials	Reuse of leftover gas pipes for construction of the Olympic stadium's ring beam (Karven 2012) Reuse softwood from local salvage/re-use centre (JLL 2012)	
Location: Olympic Park, London			
Floor construction system: Concrete slab floor, concrete upper floor	Geopolymer, fly ash and cement substitute	Geopolymer cement replaces Portland cement	
Wall construction system: Concrete block walls, steel frame timber wall	Transportation reduction by	By reusing and recycling, transportation was reduced.	
Roof construction system: Steel frame, fabric roof (commercial)	reuse, recycle, and sustainable transportation mode	Transport when necessary was by rail or water (London Olympics 2012)	
Principal architects: Jonathan Watts, George Oates, Olympic Park London Construction completed in 2012	Material resources and suppliers	Construction material suppliers are outside London; thus, distance is more than 100km (Aggregate Industries 2014)	

Table A.C.51: Bioclimatic conditions in the London Olympic Velodrome.

The Velodrome is 50 per cent lighter than Beijing's stadium (New Steel Construction 2010). It achieved 34 per cent use of recycled materials, well above its target of 20 per cent; and 63 per cent (by weight) of construction materials were transported to the Olympic Park by rail or water (London Olympics 2012). A quarter of all materials used in the building are recycled, including up to 76 per cent recycled aggregate (using stent, a by-product of the Cornish china clay industry), and 40 per cent recycled cement substitute (ground granulated blast furnace slag) in the concrete; 60 per cent recycled content in the interior block work (Ingenia 2014).

The velodrome has a high percentage of recycled content, and leftover gas pipes make up the Olympic Stadium's ring beam, reducing the need for new steel to be produced (Institution of Civil Engineers 2012). The roof design for the stadium is a fabric 'wrap' made of hemp (London Olympics 2012). The cable-net design reduced the embodied carbon by 27 per cent compared to a steel arch option (UK Indemand 2014).

Table A.C.52: Potential reduction in carbon emissions (embodied energy) in a 200mm hollow core precast concrete slab floor (see Lawson 1996, p 125).

Proc	esses w	here carbon emissions (embodied energy) can be reduce	d		
Building materials and elements	- Conc is 0.08 Saved kg/m ² c Steel - Steel	Reuse recycled aggregates for concrete Concrete from 76% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate c 0.083 MJ/Kg aved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (297 + 84) x (381 g/m ² concrete - 51.73kg/m ² cement) (Lawson 1996, p. 125) x 76% = 20.74 MJ/m² iteel from average recycled content Steel mesh +Edge beams from average recycled content = 5.148 Kg x {34 MJ/Kg (Lawson 1996, 13) - 20.10 MJ/Kg} = 71.55MJ/m²				
Implementation	Redu Geopo results 381 kg cemen	97% reduction in GHG (McLel y/m2 (Lawson 1996, p. 124) x 14 t/ m ² in concrete kg Cement/m2 x 5.6 MJ/kg (Law	ement with recycled cement substitute (Nati	1.73 kg replaced		
	Transp Bespol (Aggre (297 + (Lawse	bort of material, one stop supplie ke products. If the materials con- spate Industries 2014) 5.148 + 84) 386.14 kg/m ² x 76 f on 1996, p. 12) = 119.57 MJ/ m	waste by reusing and recycling r, Great sustainability rating for products a ne from London, the saved distance will be % /1000 T/m ² x 100 km x 4.5 – (0.6 +0.25) P ewable energy in transportation	over 100 km /2} MJ/ton/km		
Transportation	63% T 386.14 12) x 9 Mod Road Rail	Transported by rail or water .8 kg/m2 /1000 T/m2 x 100 km %63 = 99.1 MJ/M2 Transporta e Energy Consumption (MJtonne/km) UK 1 4.50 0.60	$\{4.5 - (0.6 + 0.25)/2\} = 157.3 \text{ MJ/ton/km}$			
	Source	0.25 e: Lawson (1996, p.12)				
Life Cycle Stages of I		C Pre-Construction	Construction Construction	Embodied Energy Basic		
Potential Carbon Emission (Embodied Energy) Reduction Measurable energy to reduce in Building materials and elements 76% Recycled aggregate for concrete 20.74 MJ/m ² 100% Steel from average recycled content 71.55MJ/m ² 90						
Measurable energy to re Implementation	educe in		Geopolymer 100% Cement Replacement 289.74 MJ/m²			
Measurable energy to re Transportation	educe in	Decreased transportation by reuse 119.57 MJ/ m²	Replaced Energy in transportation 99.1 MJ/M ²			
Total Floor		140.31 MJ/m ²	460.39 MJ/m ²	908MJ / m ²		

Table A.C.53: Potential reduction in carbon emissions (embodied energy) in a 125-mm elevated concrete upper floor (Lawson 1996, P. 124).

oncrete upper floor	(Lawso	ll 1990, F. 124).			
Proce	esses wh	ere carbon emissions (embo	died energy) can be reduce	d	
Building materials and elements	- Concr aggrega Saved e 40.74 k Steel f - Steel f	Leused recycled aggregate for concrete Concrete from 76% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of ggregate is 0.083 MJ/Kg aved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (300 Kg concrete – 0.74 kg cement) (Lawson 1996,125, Legend 3) x 76% =16.34 MJ/m ² teel from average recycled content Steel mesh +Edge beams from average recycled content = 7.15 Kg x {34 MJ/Kg (Lawson 1996, 13) - 20.10 MJ/Kg} = 99.38 MJ/m²			
Implementation	Repla Geopoly 2014) r 300kg/r cement/	ased and Replaced energy i ced cement ymer concrete or 100% replacement esults 97% reduction in GHG (McLe n2 (Lawson 1996, p. 124) x 14% Ces m ² in concrete g Cement/m2 x 5.6 MJ/kg (Lawson 1	with recycled cement substitute (Nat llan et al. 2011) ment (Lawson 1996, p. 41) 97% = 40		
Transportation	If mater materia Aggre Impro 63% Tr 307.153	ased transportation of wast ials come from outside London, the ls have been reused, therefore the sav egate300 kg/m ² x76% /1000T/m ² x10 1996, p.1 oved and Replaced Renewal ansported by rail or water 8 kg/m ² /1000 T/m ² x 100 km {4.5 – 78.85 MJ/m2 Reduced Transportation	distance would be over 100 km, but /// // // // // // // // // // // // //	996, p. 12) x	
	transpo Mode Road Rail Ship	ortation			
Life Cycle Stages of b		Lawson (1996, p. 12) Constru	ction	Embodied	
	0	Pre-Construction	Construction	Energy	
		Potential Carbon Emissions (I		Standard	
Measurable energy to reduce in Building materials and elements		30% Recycled aggregate for concre 16.34 MJ/m ²	tee Steel mesh from average recycled content 99.38MJ/m ²	750MJ/m ²	
Measurable energy to re Implementation			Use of 40% Fly ash mix = 228.14 MJ/m ²		
Measurable energy to re Transportation	educe in	Decreased transportation by reusing 92.89 MJ/ m ²	Replaced Energy in transportation 78.85 MJ/m²		
Total Floor		109.23 MJ/m ² 515.60	406.37 MJ/m ²	750MJ/m ²	

_	- · ·				
Proc	esses whe	ere carbon emissions (emi	oodied energy) can be redu	iced	
Building materials and elements	Reused recycled materials as aggregate for concrete block - Concrete from100% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (275 Kg concrete – 24.47 kg cement) (Lawson 1996, p. 129) = 20.79 MJ/m²				
Implementation	Decreased and Replaced energy Replaced cement Geopolymer concrete block or 100% replacement with recycled cement substitute results 80% reduction in GHG (Geiger 2010) Reduced Portland Cement= 89Kgs/tonne (Concrete Block Association 2013) /1000 x 275 =24.47 Kg/m ² Reduced Portland cement 24.47 Kg/ m ² x 5.6 MJ/kg (Lawson 1996, p.13) = 137.03 MJ/ m ²				
Transportation	Materials a Reuse aggr MJtonne/I Improv 63% Tran 299.57 kg 76.90 MJ	the from London, thus saved distance to the form London, thus saved distance to the form of the form	ent) kg.m ² /1000 T/m ² x 100 km x 4	.5 - {(0.6 +0.25) / 2} Dn 1996, p. 12) x 63% =	
	Mode Road Rail Ship	Energy Consumption (MJtonne/km) UK 4.50 0.60 0.25 awson (1996, p.12)			
Life Cycle Stages building	of	Construction	Construction	Embodied Energy	
		Potential Carbon Emission (Er	nbodied Energy) Reduction	Standard	
Measurable energy to reduce in Building materials and elemen	20.7	00% recycled aggregates 9 MJ/ m ²		511 MJ/ m²	
Measurable energy to reduce in Implementation	ion		Geopolymer, replacing 100% of cement 137.03 MJ/m2		
Measurable energy to re in Transportation	educe Dect 102.	reased transportation by reusing 09 MJ/m²	Replaced Energy in transportation 76.90 MJ/m²		
Total Walls		122.88 MJ/ m ² 336.81 M	213.93 MJ/ m ²	511MJ/ m ²	

 Table AC.54: Potential reduction in carbon emissions (embodied energy) in a cored concrete block wall (Lawson 1996, p. 129).

Table A.C.55: Potential reduction in carbon emissions (embodied energy) in a steel framed timber weatherboard wall (Lawson 1996, p. 125).

Proc	cesses v	vhere carbon emissions	(embodied energy) can be redu	ıced		
Building	- Steel	Steel from average recycled content - Steel frame from average recycled content = 3.342 Kg x 34 MJ/Kg (Lawson 1996, p. 13 - 20.10 MJ/Kg GreenSpec = 3.342 KJ/Kg X 13.9 Kg/ m2 = 46.45 MJ/m2				
materials and elements		softwood + softwood plates + s	nts (local salvage/re-use centre) oftwood weatherboard = 74 MJ/m ² (Lav	wson 1996, p. 125;		
	Constr	uction materials from London,	waste by reusing and recycling thus saved distance will be over 100 km Jtonne/km (Lawson 1996, p. 12) = 9.89	-		
Transportation	63% T 14.32	ransported by rail or water kg/m2 /1000 T/m2 x 100 km {4	ewable energy in transportation .5 – (0.6 +0.25) /2} MJton/km (Lawson n Energy consumption by type of transport	1996, p. 12) x 63% =		
	Mod	e Energy Consumption (MJtonne/km) UK				
	Road	· · · · · · · · · · · · · · · · · · ·				
	Rail	0.60				
	Ship	0.25				
	Source	: Lawson (Lawson 1996, p. 12)				
Life Cycle Stages of			onstruction	Embodied Energy		
-	-	Pre-Construction	Construction			
		Potential Carbon Emission	on (Embodied Energy) Reduction	Standard		
Measurable energy to re Building materials and elements		Steel frame from recycled content 46.45 MJ/m²	Use recycled softwood + weatherboard 74 MJ/m ²	238 MJ/ m ²		
Measurable energy to r Transportation	educe in	Decreased transportation by reuse= 9.89 MJ/ m ²	Replaced Energy in transportation 3.67 MJ/m²			

	56.34 MJ/m ²	77.67 MJ/m ²	238 MJ/ m ²
Total Walls	134	4.01 MJ/m ²	238 NJ/ m-

Table A.C.56: Potential reduction in carbon emissions (embodied energy) in a steel framed, fabric roof (hemp wrap) (Lawson 1996, p. 133).

	Proce	sses where carbon emissions (embo	died energy) can be re	duced
Building materials and elements	- Steel MJ/Kg Reus - Use r gas pij of 28% - Use 4 p. 13) Redu A mate compa	from average recycled content frame roofing from recycled content {38 MJ g x $(3.384 + 0.35)$ kg/ m ² = 65.34 MJ/m ² ed materials and elements recycled frame and pipes - Velodrome has a hi bes make up the Olympic Stadium's ring beam be recycled materials (Ingenia 2014). 40% recycled trusses (UK Indemand 2014) 40 = 50.78 MJ/m ² the Materials use in design erially efficient double-curved cable net design red to a steel arch option (UK Indemand 2014 reduce in design x 3.734 kg/m ² x 34 MJ/Kg (1	igh percentage of recycled con n (Karven 2012) The structure % x 3.734 kg/m ² x 34 MJ/Kg (n reduced the embodied carbon).	tent and leftover involved the use (Lawson 1996, 1 by 27%
	Materi 3.734 12) = 0	eased transportation of waste by reals from London, thus saved distance will be a kg/m ² steel frame x 50% kg/m ² /1000 T/m ² x 30.84 MJ/ m ²	over 100 km 100 km x 4.5 MJtonne/km (La	wson 1996, p.
Transportation	63% T 14.32	Transported by rail or water $kg/m^2/1000$ T/m² x 100 km {4.5 – (0.6 +0.25) IJ/m² Reduced Transportation Energy cons e Energy Consumption (MJtonne/km) UK 1 4.50 0.60) /2} MJton/km (Lawson 1996	
		0.25 e: Lawson (1996, p. 12)		
Life Cycle Stages of b		Construction Pre-Construction	Construction	Embodied Energy
Measurable energy to reduce in Building materials and elements		Potential Carbon Emission (Embodie 100% Steel frame from average recycled contents 65.34 MJ/m ²	Use recycled elements = 50.78 MJ/m² 50% reduce steel in design 63.47 MJ/m²	Standard 282MJ/m ²
Measurable energy to re in Transportation	educe	Decreased transportation by reuse $0.84\ MJ/$ $$m^2$$	Decreased energy by replacing 2.39 MJ/m²	
Total Roof		66.18MJ/m ² 182.82 MJ/m ²	116.64 MJ/m ²	282MJ/ m

Table A.C.57: Case Study 5. Potential reduction in carbon emissions (embodied energy) in a concrete slab floor, concrete upper floor; concrete block walls, steel framed, fabric roof construction system

Life Cycle Stages of building	Construct	tion	Embodied Energy
	Pre-Construction	Construction	
	Potential Carbon Emissions Reduce		Basic
Measurable energy to reduce in Building materials and elements	169.66 MJ/m ²	359.18 MJ/m ²	2689 MJ/m ²
Measurable energy to reduce in			
Implementation	-	654.91 MJ/m ²	
Implementation Measurable energy to reduce in Transportation	- 325.28 MJ/m ²	654.91 MJ/m ² 260.91 MJ/m ²	

A.C.2 RESEARCH MODEL APPLIED TO GENERAL AUSTRALIAN FLOOR, WALL AND ROOF CONSTRUCTION SYSTEMS

A.C.2.1 Potential carbon emission reductions in general Australian floor

construction systems

a. Elevated Timber Floor (lowest level)

Table A.C.58: Potential reduction in carbon emissions in an elevated timber floor (lowest level) (see Lawson 1996, p. 124),

Processes where carbon emissions (embodied energy) can be reduced						
Building materials and elements	Reuse the recycled aggregate for concrete - Concrete from 80 % Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (26.4 kg concrete – 3.69 cement) Kg x 80% (Lawson, 1996, p.125) =1.52 MJ/m ² Reuse the recycled aggregate for brick, 67% (Brick Development Association 2014; Tyrell & Goode 2014) 36 kg/m ² (Lawson, 1996, p.124, L 1) x 67% x 0.083 MJ/kg = 2 MJ/m ² Reuse materials and elements - Use recycled bricks 60% x 90 = 54MJ/m ² - Timber products re-used, post-consumer recycled timber or FSC certified timber, use recycled hardwood joist, flooring 54 MI/m ² x (Lawson 1996, p. 124), 60% = 32 4 MI/m ²					

	Decrease and replace energy in process					
	reduction in GHG (McLellan et al. 2011; Koth	Geopolymer concrete or 100% replacement with recycled cement substitute (Nath & Sarker 2014) results 97% reduction in GHG (McLellan et al. 2011; Kotrayothar 2012) 26.4 kg/m ² (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) = 3.69 kg replaced cement/ m ² in				
	3.69 kg Cement/m2 x 5.6 MJ/kg (Lawson 199	96, p.13) = 20.66 MJ/ m²				
Implementation	Potential 40 per cent energy savings in brick r (Brick Development Association 2014; Tyrell		ainer glass brick grog			
	Reduced energy 90 MJ/m ² x 40% = 36 MJ/m	2				
Green Star Replaced cement Geopolymer concrete or 60% replacement with recycled cement substitute (Nath & Sarker 2014) resur- reduction in GHG (McLellan et al. 2011) 26.4 kg/m ² (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) 60% = 2.29 kg replaced cement concrete 2.29 kg Cement/m2 x 5.6 MJ/kg (Lawson1996, p. 13) = 12.82 MJ/m ²						
Life cycle stages of	f Constructi	Construction				
building	Pre-Construction	Construction	Standard			
	Potential Embodied Energy	to Replace and Save				
Measurable energy t reduce in Building materials and elements		Use recycled brick 54MJ/m² Use recycled Hardwood 32.4 MJ/m²	293MJ/m ²			
Measurable energy to reduce in Implementation	40% saving energy in production 36 MJ/m ²	Geopolymer concrete 20.66 MJ/ m ²				
Total Floor	39.52 MJ/m ² 146.58 M	107.06 MJ/m ²	293MJ / m ²			

level) (Lawson 1996, p.	124).			
Life Cycle Stages of	Co	Embodied		
building	Pre-Construction	Construction	Energy	
	Potential Carbon Emissio	Potential Carbon Emission (Embodied Energy) Reduction		
Measurable energy to reduce in Implementation	Concrete from recycled aggregate 0.38 MJ/m²	Use recycled Hardwood 32.4 MJ/m²	293 MJ/m ²	
Implementation		Geopolymer concrete 12.82 MJ/ m²		
Green Star, Total Floor	0.38 MJ/ m ²	45.22 MJ/m ²	293 MJ/ m ²	
Green Star, Total Floor	45.60 MJ/m ²		295 IVIJ/ III	

Table A.C.59: Green Star. Potential reduction in carbon emissions in an elevated timber floor (lowest level) (Lawson 1996, p. 124).

b. Elevated Timber Floor (upper level)

Table A.C.60: Potential reduction in carbon emissions in a timber framed timber floor upper floor (Lawson 1996, p. 124).

Pro	ocesses where o	arbon emissions (emb	odied energy) can be redu	uced		
Building	Reused mat	erials and elements				
materials and elements	flooring @ 18 n		tion 2013) @ (600 c-c) 300x 500 91 MJ/m ² = 60% x 141 MJ/m ² P.			
	nual, 95% of all timber products r mber (Green building Council of A	· 1				
	60% Recycled softwood joints (Design Coalition 2013) @ (600 c-c) 300x 500 mm + Timber flooring @ 18 mm particleboard 50 MJ/m^2 + 91 MJ/m^2 = %60 x 141 MJ/m^2 P. 124 = 84.6 MJ/n (Steel Construction Information 2014)					
Life Cycle Stag	ges of building	Construction		Embodied Energy		
		Pre-Construction	Construction	Basic		
		Potential reduction	on in carbon emissions			
Measurable energy to reduce in Building materials and elements			60% Recycled timber floor 84.6 MJ/m ²	147MJ/m ²		
			84.60 MJ/m ²	147MJ/ m ²		
Total F	loor	84.	60 MJ/m ²			

Table A.C.61: Green Star. Potential reduction in carbon emissions in a timber framed timber floor upper floor (Lawson 1996, p. 124)

Life Cycle Stages of	Co	Embodied	
building	Pre-Construction Construction		Energy
	Potential Carbon Emissio	Basic	
Measurable energy to reduce in Implementation	60% Recycled timber floor 84.6 MJ/m²		147 MJ/m ²
		94 (MTL-2	
Green Star, Total Floor	84.6 MJ/m ² 84.60 MJ/m ²		147 MJ/ m ²

c. 110 mm Concrete Slab on ground

Table A.C.62: Potential reduction in carbon emissions in a 110-mm concrete slab on ground floor (Lawson 1996, p. 124).

Pro	cesses where carbon emissions (embodied energy) can be reduced
	Reused recycled aggregate for concrete
Building materials and elements	 Concrete from 80% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (290.4 concrete –39.43 cement Kg (Lawson 1996, p.125) x 80% =16.67 MJ/m² Steel from average recycled content
	- Steel mesh +Edge beams from average recycled content = $3.882 \text{ Kg x} \{34 \text{ MJ/Kg} (Lawson 1996, p. 13 - 20.10 \text{ MJ/Kg}\} = 53.96 \text{MJ/m}^2$
	Green Star Reused recycled aggregate for concrete Material-5 Green Star Technical Manual is considered maximum 20%, therefore reduced embodied energy by this credit (Concrete from 20% Recycled aggregate) (Green building Council of Australia 2008) is: - Concrete from 20% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (290.4 concrete –39.43 cement Kg (Lawson 1996, p.125) x 20% = 4.16 MJ/m² Steel from average recycled content Material-6 Green Star Technical Manual, steel is considered maximum 90%, therefore reduced embodied energy by this credit (Steel from Recycled content) (Green building Council of Australia 2008) is: 3.882 Kg x 90% {34 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg} = 53.95 MJ/m²
Implementation	Decreased and Replaced energy in process Replaced cement Geopolymer Concrete or 100% replacing with recycled cement substitute (Nath & Sarker 2014) results 97% reduction in GHG (McLellan et al. 2011) 290.4 kg/m2 (Lawson1996, p. 124) x 14% Cement (Lawson 1996, p. 41) = 39.43 kg replaced cement/ m ² in concrete 39.43 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p. 13) = 220.83 MJ/ m² Green Star

Replacing maximum 60% of cement (Green building Council of Australia 2008) 290.4 kg/m2 (Lawson1996, p. 124) x 14% Cement (Lawson 1996, p. 41) 60% = 24.38 kg replaced cement/ m² in concrete 24.38 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p. 13) x 60% = **81.91 MJ/m²**

Life cycle stages of building	Co	nstruction	Embodied
	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	n (Embodied Energy) Reduction	Basic
Measurable energy to reduce	Concrete from 80% recycled	Steel mesh, beams from average recycled	
in Building materials and elements	aggregate = 16.67 MJ/m ²	content = 53.96 MJ/m	645MJ/m ²
Measurable energy to reduce in Implementation		Geopolymer, replacing 100% of cement = 220.83 MJ/m^2	
	16.67 MJ/m ²	274.79 MJ/m ²	
Total Floor	29	1.46 MJ/m ²	645MJ / m ²

Table A.C.63: Green Star. Potential reduction in carbon emissions in a 110-mm concrete slab on ground floor (Lawson 1996, p. 124)

Life Cycle Stages of building	Co	Embodied	
	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	n (Embodied Energy) Reduction	Basic
Measurable energy to	20% Recycled aggregate for	90%Steel mesh from average recycled	645 MJ/m ²
reduce in Implementation	concrete = 4.16 MJ/m^2	content 53.95MJ/m ²	045 MJ/III
Measurable energy to reduce		Geopolymer, 60% Cement Replacements	
in Implementation		136.59 MJ/m ²	
Courses Steve Testal Flager	4.16 MJ/m ²	190.54 MJ/m ²	(A5) A11
Green Star, Total Floor	194	1.70 MJ/m ²	645MJ/ m ²

d. 125mm Elevated Concrete Slab (temporary framework)

Table A.C.64: Potential reduction in carbon emissions in a 125-mm elevated concrete upper floor (Lawson 1996, p. 124-6)

Proc	esses wł	nere carbon emissions (embodi	ed energy) can be reduced	I
	- Concre 0.083 M Saved en kg ceme Steel fro	nbodied energy = embodied energy of ag nt) (Lawson 1996, p. 125) x 80% =17.20 m average recycled content	ggregate 0.083 MJ/Kg x (300 Kg o MJ/m ²	concrete – 40.74
Building materials and elements	- Steel mesh +Edge beams from average recycled content = 7.15 Kg x { 34 MJ/Kg (Lawson 1996, p13) - 20.10 MJ/Kg} = 99.38 MJ/m ² Green Star Reused recycled aggregate for concrete Material-5 Green Star Technical manual is considered maximum 20%, therefore reduced embodied energy by this credit (Concrete from 20% Recycled aggregate) (Green building Council of Australia 2008) is: Concrete from 20% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg saved embodied energy = 0.083 MJ/Kg x (300 Kg concrete – 40.74 kg cement) (Lawson 1996, p.125) x 20% = 4.30 MJ/m ² Steel from average recycled content Material-6 Green Star Technical Manual, Steel is considered maximum 90%, therefore reduced embodied energy by this credit (Steel from Recycled content) (Green building Council of Australia 2008) is: 7.15 Kg x 90% { 34 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg} = 89.44 MJ/m ²			
Implementation	Replaced Geopolyn 97% redu 300kg/mi concrete 40.74 kg Green Sta Replacin 300kg/mi	ner concrete or 100% replacing with recycl action in GHG (McLellan et al. 2011) 2 (Lawson 1996, p. 124) x 14% Cement (La Cement/m2 x 5.6 MJ/kg (Lawson 1996, p.) ar g maximum 60% of cement (Green building 2 (Lawson 1996, p. 124) x 14% Cement (La	awson 1996. p. 41) = 40.74 kg repla (3) = 228.14 MJ/ m ² g Council of Australia 2008)	ced cement/ m ² in
Life Cycle Stages of b		ncrete Cement/m2 x 5.6 MJ/kg (Lawson 1996, p.12 Construction		Embodied
of the burges of b		Pre-Construction	Construction	Energy
		Potential Carbon Emission (Emb		Standard
Measurable energy to reduce in Building materials and elements		80% Recycled aggregate for concrete 17.20 MJ/m ²	Steel mesh from average recycled content 99.38MJ/m ²	750MJ/m ²
Measurable energy to re Implementation	educe in		Use of 40% Fly ash mix = 228.14 MJ/m ²	
Total Floor		17.20 MJ/m ² 344.72 MJ	327.52 MJ/m ²	750MJ/m ²

Table A.C.65: Green Star. Potential reduction in carbon emissions in a 125-mm elevated concrete upper floor (Lawson 1996, p. 124-6).

Life Cycle Stages of	Co	Embodied	
building	Pre-Construction	Energy	
	Potential Carbon Emissio	n (Embodied Energy) Reduction	Basic
Measurable energy to	20% Recycled aggregate for	90% Steel mesh from average recycled	750 MJ/m ²
reduce in Implementation	$concrete = 4.30 \text{ MJ/m}^2$	content 89.44 MJ/m ²	/ 50 Ivij/III
Measurable energy to reduce		Geopolymer, 60% Cement Replacements	
in Implementation		141.12 MJ/m ²	
Crean Stan Tatal Flagn	4.30 MJ/m ²	230.56 MJ/m ²	750 MJ/ m ²
Green Star, Total Floor	23	4.76 MJ/m ²	/50 IVIJ/ III

e. 110mm elevated concrete slab (permanent frame work)

Table A.C.66: Potential reduction in carbon emissions in a 110-mm concrete slab (permanent framework) (Lawson 1996, p. 125)

	Reused recycled aggregate for concrete
Building materials and elements	 - Concrete from 80 % Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (264 concrete -36.96 cement) Kg (Lawson 1996, p.125) x 80% =15.07 MJ/m² Steel from average recycled content
	- Steel mesh +Edge beams from average recycled content = 2.5 Kg x {34 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg} = 34.75 MJ/m ²
	Steel formwork from average recycled content = $3.66 \text{ Kg x} \{38 \text{ MJ/Kg} (Lawson 1996, p. 13) - 20.10 \text{ MJ/Kg} \}$ 65.51MJ/m ²
	Green Star Reused recycled aggregate for concrete Material-5 Green Star Technical manual is considered maximum 20%, therefore reduced embodied energy by this credit (Concrete from 20% Recycled aggregate) (Green building Council of Australia 2008) is: - Concrete from 20% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (264 concrete -36.96 cement) Kg (Lawson 1996, p.125) x 20% = 3.76 MJ/m² Steel from average recycled content Material-6 Green Star Technical Manual, Steel is considered maximum 90%, therefore reduced embodied energy by this credit (Steel from Recycled content) (Green building Council of Australia 2008) is: Steel mesh, 2.5 Kg x 90% {34 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg} = 31.27 MJ/m² Steel formwork 3.66 Kg x 90% {38 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg} = 58.96 MJ/m²

	Decreased and Replaced energy in process
	Replaced cement
	Geopolymer Concrete or 100% replacing with recycled cement substitute (Nath & Sarker 2014) results 97% reduction in GHG (McLellan et al. 2011)
	264 kg/m2 (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) = $36.96 kg$ replaced cement/ m ² in
Implementation	concrete
implementation	$36.96 \text{ kg Cement/m2 x } 5.6 \text{ MJ/kg (Lawson 1996, p. 13)} = 206.97 \text{ MJ/ m}^2$
	Green Star
	Replacing maximum 60% of cement (Green building Council of Australia 2008)
	264 kg/m2 (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) $60% = 22.17 kg$ replaced cement/ m ²
	in concrete
	22.17 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p.13) = 124.15 MJ/ m²

Life cycle stages of building	(Construction	Embodied
	Pre-Construction	Construction	Energy
	Potential Carbon Emiss	ion (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Building materials and elements	Concrete from 80% recycled aggregate = 15.07 MJ/m²	Steel mesh, beams from average recycled content = 34.75MJ/m ² Steel formwork from average recycled content = 65.51 MJ/m	665MJ/m ²
Measurable energy to reduce in Implementation		Geopolymer, replacing 100% of cement = 206.97 MJ/m^2	
	15.07 MJ/m ²	277.23 MJ/m ²	
Total Floor		292.3 MJ/m ²	665MJ / m ²

Table A.C.66-1: Green Star. Potential reduction in carbon emissions in a 110-mm concrete slab(permanent framework) (Lawson 1996, p. 124)

Life Cycle Stages of building	Co	Embodied	
	Pre-Construction	Construction	Energy
	Potential Carbon Emission	n (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation	20% Recycled aggregate for concrete = 3.76 MJ/m ²	90%Steel mesh from average recycled content 31.27MJ/m² Steel formwork from average recycled content = 58.96 MJ/m	665 MJ/m ²
Measurable energy to reduce in Implementation		Geopolymer, 60% Cement Replacement 124.15 MJ/m ²	
Green Star, Total Floor	3.76 MJ/m ²	214.38 MJ/m ²	665MJ/ m ²

f. 200mm Precast Concrete Tee Beam/Infill flooring

Table A.C.67: Potential reduction in carbon emissions in a 200-mm precast concrete tee beam/infill floor (Lawson 1996, p. 125).

	Reused recycled aggregate for concrete
Building materials and	 - Concrete from 80% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (182.88 concrete – 25.60 cement) Kg (Lawson 1996, p. 125) x 80% =10.44 MJ/m² Steel from average recycled content
elements	- Steel mesh +Edge beams from average recycled content = 4.216 Kg x {34 MJ/Kg (Lawson 1996, p.13) - 20.10 MJ/Kg} = 58.51 MJ/m²
	Steel formwork from average recycled content = 3.66 Kg x {38 MJ/Kg (Lawson 1996, p.13) - 20.10 MJ/Kg} + 65.51MJ/m ²
	Green Star Reused recycled aggregate for concrete Material-5 Green Star Technical Manual, considered maximum 20%, therefore reduced embodied energy by this credit (Concrete from 20% Recycled aggregate) (Green building Council of Australia 2008) is: - Concrete from 20% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (182.88 concrete - 25.60 cement) Kg (Lawson 1996, p. 125) x 20% = 2.61 MJ/m ² Steel from average recycled content Material-6 Green Star Technical Manual, Steel is considered maximum 90%, therefore reduced embodied energy by this credit (Steel from Recycled content) (Green building Council of Australia 2008) is: Steel mesh, 4.216 Kg x 90% {34 MJ/Kg (Lawson 1996, p.13) - 20.10 MJ/Kg} = 52.74 MJ/m ² Steel formwork 3.66 Kg x 90% {38 MJ/Kg (Lawson 1996, p.13) - 20.10 MJ/Kg} = 58.96 MJ/m ²

	Decreased and Replaced energy in process
	Replaced cement
	Geopolymer Concrete or 100% replacing with recycled cement substitute (Nath & Sarker 2014) results 97% reduction in GHG (McLellan et al. 2011)
	182.88 kg/m2 (Lawson p. 124) x 14% Cement (Lawson 1996, p. 41) = 24.83 kg replaced cement/ m^2 in
T	concrete
Implementation	24.83 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p.13) = 139.04 MJ / \mathbf{m}^2
	Green Star
	Replacing maximum 60% of cement (Green building Council of Australia 2008)
	182.88 kg/m2 (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) 60% = 15.36 kg replaced cement/
	m ² in concrete
	15.36 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p.13) = 86.01 MJ/m ²

Life cycle stages of building	Co	Construction		
	Pre-Construction	Construction		Energy
	Potential Carbon Emissio	n (Embodied Energy) Reduction	[Basic
Measurable energy to reduce in Building materials and elements	Concrete from 80% recycled aggregate = 10.44 MJ/m ²	Steel mesh, beams from average recycled content = 58.51MJ/m² Steel formwork from average recycled content = 65.51 MJ/m		665MJ/m ²
Measurable energy to reduce in Implementation		Geopolymer, replacing 100% of cement = 139.04 MJ/ m ²		
	10.44 MJ/m ²	263.06 MJ/m ²	[
Total Floor	27	3.50 MJ/m ²		665MJ / m ²

Table A.C.68: Green Star Potential reduction in carbon emissions in a 200-mm precast concrete tee beam/infill floor (Lawson 1996, p. 124).

Life Cycle Stages of building	Co	nstruction	Embodied Energy
	Pre-Construction	Construction	Basic
	Potential Carbon Emissio	n (Embodied Energy) Reduction	
Measurable energy to reduce	%20 Recycled aggregate for concrete	90% Steel mesh from average recycled content	
in Implementation	$= 2.61 \text{ MJ/m}^2$	52.74MJ/m ²	
		Steel formwork from average recycled content	665 MJ/m ²
		= 58.96 MJ/m	
Measurable energy to reduce in		Geopolymer, 60% Cement Replacements	
Implementation		124.15 MJ/m ²	
Course Steer Total Floor	2.61 MJ/m ²	235.85 MJ/m ²	665MJ/ m ²
Green Star, Total Floor	238	3.46 MJ/m ²	665MJ/ m ²

g. 200mm Hollow Core Precast Concrete flooring

Table A.C.69: Potential reduction in carbon emissions in a 200-mm hollow core precast concrete slab floor (Lawson 1996, p. 125).

Proc	Processes where carbon emissions (embodied energy) can be reduced					
Building materials and elements	Reused the recycled aggregates for concrete - Concrete from 80% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083MJ/Kg x (381 kg/m ² concrete – 51.73kg/m ² cement) (Lawson, 1996, p.125) x 80% = 21.84 MJ/m ² Steel from average recycled content - Steel mesh +Edge beams from average recycled content = 5.148 Kg x {34 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg} = 71.55 MJ/m ² Green Star Reused recycled aggregate for concrete Material-5 Green Star Technical Manual, considered maximum 20%, therefore reduced embodied energy by this credit (Concrete from 20% Recycled aggregate) (Green building Council of Australia 2008) is: - Concrete from 20% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (381 kg/m ² concrete – 51.73kg/m ² cement) (Lawson 1996, p. 125) x 20% = 5.46 MJ/m ² Steel from average recycled content Material-6 Green Star Technical Manual, Steel is considered maximum 90%, therefore reduced embodied energy by this credit (Steel from Recycled content) (Green building Council of Australia 2008) is: 5.148 Kg x 90% {34 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg} = 64.39 MJ/m ²					

I otal Floor		383.07 MJ/m ²				
Total Floor		21.84 MJ/m ²	361.23 MJ/m ²	908MJ / m ²		
• · · · · · · · · · · · · · · · · · · ·		1		1		
Measurable energy to reduce in Implementation			cement = 289.68 MJ/ m^2			
Massurable energy to rec	duce in	1	Geopolymer, replacing 100% of			
elements						
Building materials and	1	$aggregate = 21.84 \text{ MJ/m}^2$	recycled content = 71.55 MJ/m^2	908 MJ/m ²		
Measurable energy to re	educe in	30 % Concrete from recycled	100% Steel mesh, beams from average			
		Potential reduction in carbon emissions		Standard		
.,	0	Pre-Construction	Construction	Energy		
Life Cycle Stages of bui	<u> </u>	Construction		Embodied		
		$\frac{1}{2}$ mm m concrete 1990, $\frac{1}{2}$ mm m concrete 1990, p.13) =179.2 MJ/m ²				
		381kg/m ² (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) 60% = 32 kg replaced cement/ m ² in concrete 1996,				
			een building Council of Australia 2008) Compart (Lawson 1006, p. 41) $60\% = 32$ kg	raplaced		
	Green					
Implementation		8 8 9	on 1996, p.13) = 289.68 MJ/ m ²			
		/ m ² in concrete		1		
			Cement (Lawson 1996, p. 41) = 51.73 kg r	eplaced		
	_ <u> </u>	97% reduction in GHG (McLella	6 7	5 Jarker 2014		
	Replaced cement Geopolymer Concrete or 100% replacing with recycled cement substitute (Nath & Sarker 2014)					
		sed and Replaced energy				

Table A.C.70: Green Star. Potential reduction in carbon emissions in a 200-mm hollow core precastconcrete slab floor (Lawson 1996, p. 125)

Life Cycle Stages of	Co	onstruction	Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	on (Embodied Energy) Reduction	Basic
Measurable energy to	20% Recycled aggregate for	90% Steel mesh from average recycled	908 MJ/m ²
reduce in Implementation	concrete =5.46 MJ/m^2	content 64.39 MJ/m ²	908 MJ/m-
Measurable energy to reduce		Geopolymer, 60% Cement Replacements	
in Implementation		179.2 MJ/m ²	
Crean Stan Tatal Flaan	5.46 MJ/m ²	243.59 MJ/m ²	908 MJ/ m ²
Green Star, Total Floor	249.05 MJ/m ²		908 IVIJ/ III

A.C.2.2 Potential carbon emission reduction in general Australian wall construction systems

a. Timber Framed, Single Skin Timber Wall

Table A.C.71: Potential reduction in carbon emissions in a timber framed, single skin timber wall (Lawson 1996, p. 125).

Processe	s where carbon e	missions (embodied energy) can	be reduced	
	Reuse recycled	materials		
		er and post-consumer 60% FSC timber + 1 8.4 = 24.93 MJ/m² (Lawson 1996, p. 125;		
Building materials and elements	Use recycled therma 16.43 MJ/m ²	l insulation, 49MJ/kg (Lawson 1996) - 20	.90 MJ/kg x 0.585kg/m ² =	
	Green Star Reuse recycled materials			
	Use recycled softwood studs, 95% Reuse softwood stud@100x50mm+ softwood plates@100x50 mm =, 95% x 11 MJ/m ² (Lawson 1996, p.125, L. 7) 3.4 = 23.68 MJ/m²			
Areas that Embodied		Construction	Embodied Energy	
Energy can be reduced	Pre-Construction	Construction		
	Potential Embod	lied Energy to Replace and Save	Standard	
Measurable energy to reduce in Building materials and elements		softwood studs + softwood plates 24.93 MJ/m ² Use Recycle thermal insulation 16.43 MJ/m ²	151MJ/ m ²	
Total Walls		41.36 MJ/m ²	151MJ/ m ²	

Table A.C.72: Green Star. Potential reduction in carbon emissions in a timber frame, single skin timber wall (Lawson 1996, p. 125).

Life Cycle Stages of		Embodied	
building	Pre-Construction	Construction	Energy
	Potential Carbon Er	nission (Embodied Energy) Reduction	Basic
Measurable energy to		95% softwood studs + softwood plates	
reduce in Implementation	23.68MJ/m ²		151 MJ/m ²
_		Use Recycle thermal insulation 16.43 MJ/m²	
Crean Stan Tatal Wall		36.43 MJ/m ²	151 MJ/ m ²
Green Star, Total Wall	40.11 MJ/m ²		151 NJ/ m-

b. Timber Frame, Timber Weatherboard Wall

Table A.C.73: Potential reduction in carbon emissions in a timber framed timber weatherboard wall (Lawson 1996, p. 125-127).

Processes where carbon emissions (embodied energy) can be reduced					
	Use = 15 Reu (7.1. Use	Aluminium from recycled c 5.78 MJ/m² used materials and el se recycled timber and post- 5+2.75+1.1+11) x 3.4 Mj/kg	average recycled content ontent 0.0975 kg/m2 (170 Mj/kg new – 8.1 M ements (local salvage/re-use centre) consumer 60% FSC timber + Reuse the recyc g = 74.80 MJ/m ² (Lawson 1996), p. 125; JLL 2 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.5 rmation 2014)	led timber 40% 2012)	
	Green Star Reused materials and elements (local salvage/re-use centre) Material-8 Timber, Green Star Technical Manual, 95% of all timber products re-used, post- consumer recycled timber or FSC certified timber Reuse softwood + softwood plates + softwood weatherboard = 22 MJ/m ² (Lawson 1996, p. 125) x 3.4 Mj/kg x 95% = 71.06 MJ/m²				
Life Cycle Stages	of		Construction	Embodied Energy	
building		Pre-Construction	Construction		
		Potential Carbon Em	ission (Embodied Energy) Reduction	Standard	
Measurable energy to re		Aluminium from	Use recycled softwood + weatherboard		
e i		recycled contents =	74.80 MJ/m ²	188 MJ/ m ²	
elements	elements 15.78 MJ/m2 Recycled thermal insulation16.43 MJ/m ²				
Total Walls		15.78 MJ/m2	91.23 MJ/m ²	188MJ/ m ²	
10001 (700115		107.01 MJ/m ²		100100/ 11	

Table A.C.74: Green Star, Potential reduction in carbon emissions in a timber framed timber weatherboard wall (Lawson 1996, p. 135).

Life Cycle Stages of building	Construction Pre-Construction		Embodied Energy
	Potential Carbon Emissio	Basic	
Measurable energy to reduce in Implementation	Use recycled softwood + weatherboard 71.06 MJ/m ²		188 MJ/ m ²
Green Star, Total Wall	71	71.06 MJ/m ²	188 MJ/ m ²

c. Timber Frame, Reconstituted Timber Weatherboard Wall

Table A.C.75: Potential reduction in carbon emissions in a timber framed reconstituted timber weatherboard wall (Lawson 1996, p. 126).

Proc	esses	where carbon emission	s (embodied energy) can be red	uced
	Use		verage recycled content tent 0.0975 kg/m2 (170 Mj/kg new – 8.1 1	Mj/kg from recycled)
	Reus (7.1: 11 k Use	ised materials and elen se recycled timber and post-co 5+2.75+1.1) x 3.4 Mj/kg = 37. g/m2 x 24.2 Mj/kg = 266.20 M	MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.	cled timber 40% 2)
	Reu Mate cons Reus 95%	erial-8 Timber, Green Star Tec umer recycled timber or FSC of	nsumer, FSC timber + Reuse the recycled = 35.53 MJ/m²	· 1
Life Cycle Stages building		6	Construction Construction	Embodied Energy
			sion (Embodied Energy) Reduction	Standard
Measurable energy to reduce in Building materials and elements		Aluminium from recycled contents = 15.78 MJ/m2	Use recycled softwood + weatherboard 37.4 MJ/m² Weatherboard 266.20 MJ/m² Thermal insulation = 16.43 MJ/m²	377 MJ/ m ²
Total Walls		15.78 MJ/m ²	320.03 MJ/m ²	377MJ/ m ²
i oun vi ans			335.81 MJ/m ²	5771107 III

Table A.C.76: Green Star. Potential reduction in carbon emissions in a timber frame, reconstituted timber weatherboard wall (Lawson 1996, p. 126)

Life Cycle Stages of		Embodied	
building	Pre-Construction	Construction	Energy
	Potential Carbon	Emission (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation		Use recycled softwood + weatherboard 35.53 MJ/m ² Weatherboard 252.20 MJ/m ²	377 MJ/ m ²
		287.73 MJ/m ²	
Green Star, Total Wall		287.73 MJ/m ²	377 MJ/ m ²

d. Timber Frame, Fiber Cement Weatherboard Wall

Table A.C.77: Potential reduction in carbon emissions in a timber framed fibre cement weatherboard wall (Lawson 1996, p. 126).

	15.78 MJ/m2	Thermal insulation = 16.43 MJ/m ² 58.82 MJ/m ²	169 M.I/ m ²
		Geopolymer 0.98 MJ/ m²	
		FC Weatherboard 0.018 MJ/m²	169 MJ/ m ²
	contents = 15.78 MJ/m2	weatherboard 37.4 MJ/m^2	
educe			
			Standard
, 51			Entrotated Entry
	0 0		Embodied Energy
			timber 95%
			. 1 050/
			re-used, post-
Gr	een Star		
	0 0	(Lawson 1996, p.13) = 0.98 MJ/ m ²	
	,	14% Cement (Lawson 1996, p. 41) 50% =	= 0.175 kg replaced
		and cement with geopolymer (McLellan	et al. 2011; Nath and
cem	ent) Kg/m ² (Lawson 1996, p. 1		
			<i>`</i>
Use	FC weatherboard from recycle	ed 50% aggregate (Herbudiman & Saptaji 2	.013)
11 k Use	$g/m2 \ge 24.2 \text{ Mj/kg} = 266.20 \text{ N}$ recycled thermal insulation, 49	1J/m² 9MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.	, ,
Reu	se the recycled timber and post	t-consumer 60% FSC timber + Reuse the r	ecycled timber 40%
		nents (local salvage/re-use centre	ESC)
Use	Aluminium from recycled con		Mj/kg from recycled)
			uccu
PECEE	where carbon emission	s (embodied energy) can be red	uced
	Ste Use = 15 Reu (7.1: 11 k Use MJ/ Use Save cem = 0.4 Geo Sark 2.5 l cem 0.17 Gro Reu (7.1:	Steel (Aluminium) from an Use Aluminium from recycled con = 15.78 MJ/m²Reused materials and elem Reuse the recycled timber and post (7.15+2.75+1.1) x 3.4 Mj/kg = 37. 11 kg/m2 x 24.2 Mj/kg = 266.20 M Use recycled thermal insulation, 4% MJ/m² (Steel Construction Information Use FC weatherboard from recycled Saved embodied energy = embodiation cement) Kg/m² (Lawson 1996, p. 1 = 0.018 MJ/m² Geopolymer 50% replacing Portla Sarker 2014) 2.5 kg/m² (Lawson 1996, p. 124) x cement/m² 0.175 kg Cement/m2 x 5.6 MJ/kg d Green Star Reuse materials and element Material-8 Timber, Green Star Tec consumer recycled timber or FSC on sumer recycled timber or FSC on sumer recycled timber and post-co (7.15+2.75+1.1) x 3.4 Mj/kg = 35. 11 kg/m2 x 24.2 Mj/kg x 95% = 25 ofofPre-Construction Pre-ConstructionPre-ConstructionPre-ConstructionPre-Construction	Reused materials and elements (local salvage/re-use centre, Reuse the recycled timber and post-consumer 60% FSC timber + Reuse the r (7.15+2.75+1.1) x 3.4 Mj/kg = 37.4 MJ/m² (Lawson 1996, p. 125; JLL 2012 11 kg/m2 x 24.2 Mj/kg = 266.20 MJ/m² Use recycled thermal insulation, 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.3 MJ/m² (Steel Construction Information 2014) Use FC weatherboard from recycled 50% aggregate (Herbudiman & Saptaji 2 Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (2.5 cement) Kg/m² (Lawson 1996, p. 134) = 0.083 x 2.15 kg/m2 x 50% (Herbudi = 0.018 MJ/m²

Table A.C.78: Green Star. Potential reduction in carbon emissions in a timber framed fibre cement weatherboard wall (Lawson 1996, p. 126)

Life Cycle Stages of		Embodied	
building	Pre-Construction	Construction	Energy
	Potential Carbon	Emission (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation		Use recycled softwood + weatherboard 35.53 MJ/m^2	169 MJ/ m ²
Green Star, Total Wall		35.53 MJ/m ² 35.53 MJ/m ²	169 MJ/ m ²

e. Timber Frame, Steel Clad Wall

Table A.C.79: Potential reduction in carbon emissions in a timber framed steel clad wall (Lawson	
1996, p. 126)	

Proces	sses w	here carbon emissions ((embodied energy) can be red	luced
	Steel Use Ah = 15.78 - Steel of MJ/Kg Reuse Reuse r (7.15+2) Use rec	(Aluminium) from aver aminium from recycled conten MJ/m ² cladding from average recycled } = 87.71MJ/m ² cd materials and element recycled timber and post-consu 2.75+1.1) x 3.4 Mj/kg = 37.40	rage recycled content ts 0.0975 kg/m2 (170 Mj/kg new – 8.1 d content = 4.9 Kg x {38 MJ/Kg (Lawa nts (local salvage/re-use centre mer 60% FSC timber + Reuse the recy MJ/m ² (Lawson 1996, p. 125; JLL 20 J/kg (Lawson 1996) - 20.90 MJ/kg x 0	Mj/kg from recycled) son 1996, p13) - 20.10) /cled timber 40% 12)
	Materia consum Reuse s 3.4 Mj/ Materia embodi 2008) is - Steel o	e materials and element ul-8 Timber, Green Star Techni her recycled timber or FSC cert offwood + softwood plates + s kg x 95% = 35.53 MJ/m² ul-6 Green Star Technical Manu ed energy by this credit (Steel s	ts (local salvage/re-use centre) ical Manual, 95% of all timber product iffied timber softwood weatherboard = 11 MJ/m ² (Li ual, Steel is considered maximum 90% from Recycled content) (Green buildin d content = 4.9 Kg x {38 MJ/Kg (Laws	awson 1996, p. 125) x , therefore reduced ng Council of Australia
Life Cycle Stages o		Cor	nstruction	Embodied Energy
building		Pre-Construction	Construction	Ctorr Joy 1
Measurable energy to red in Building materials an elements	nd co Si	Potential Carbon Emission luminium from recycled ontents = 15.78 MJ/m^2 teel cladding from recycled ontent 87.71 MJ/m^2	a (Embodied Energy) Reduction Use recycled softwood + weatherboard 37.40 MJ/m ² Recycled thermal insulation16.43 MJ/m ²	Standard 336 MJ/ m ²
Total Walls		103.49 MJ/m2 157	53.83 MJ/m ²	336MJ/ m ²

Table A.C.80: Green Star. Potential reduction in carbon emissions in a timber framed steel clad wall (Lawson 1996, p. 126)

Life Cycle Stages of	Construction		Embodied	
building	Pre-Construction Construction		Energy	
	Potential Carbon Emissio	Potential Carbon Emission (Embodied Energy) Reduction		
Measurable energy to reduce in Implementation	Steel cladding from recycled content 78.93 MJ/m²	Use recycled softwood + weatherboard 35.53 MJ/m ²	336 MJ/ m ²	
Green Star, Total Wall	78.93 MJ/m ²	35.53 MJ/m ²	336 MJ/ m ²	
Green Star, Totar Wan	11	4.46 MJ/m ²	550 WJ/ III	

f. Steel Frame, Steel Clad Wall

Table A.C.81: Potential reduction in carbon emissions in a steel framed steel clad wall (Lawson 1996, p. 127)

Proce	sses where carbon emissions ((embodied energy) can be redu	iced
	MJ/Kg = 3.342 KJ/Kg X 13.9 Kg/ m2 - Steel cladding from average recycled 20.10 MJ/Kg} = 87.71MJ/m ² Aluminium from average red Use Aluminium from recycled conten = 15.78 MJ/m ² Reused materials and element Use recycled thermal insulation, 49M. MJ/m ² (Steel Construction Information Reuse 40% recycled steel 3.342 Kg x 3	ontent = 3.342 Kg x 34 MJ/Kg (Lawson = 46.45 MJ/m2 d content = 4.9 Kg x {38 MJ/Kg (Lawso cycled content ts 0.0975 kg/m2 (170 Mj/kg new – 8.1 M hts (local salvage/re-use centre) J/kg (Lawson 1996) - 20.90 MJ/kg x 0.5	n 1996, p. 13) - Aj/kg from recycled) 85kg/m ² = 16.43
	Reuse materials in design Reduce 20% steel in design 3 342 Kg	x 34 MJ/Kg (Lawson 1996, p. 13) x 209	% – 22 72 MI/m2
	Green Star	x 34 MJ/Kg (Lawson 1990, p. 13) x 207	0 – 22.72 WIJ/III2
Life Cycle Stages o building	consumer recycled timber or FSC cert Material-6 Green Star Technical Manu embodied energy by this credit (Steel 2008) is - Steel frame from average recycled cc MJ/Kg = 3.342 KJ/Kg X 13.9 Kg/ m2 - Steel cladding from average recycled 20.10 MJ/Kg 90% = 78.93 MJ/m² Reduce 20% steel in design 3.342 Kg of Cor	cal Manual, 95% of all timber products ified timber ual, Steel is considered maximum 90%, from Recycled content) (Green building ontent = 3.342 Kg x 34 MJ/Kg (Lawson x 90% = 41.80 MJ/m2 d content = 4.9 Kg x {38 MJ/Kg (Lawson x 34 MJ/Kg (Lawson 11996, p. 13) x 20 instruction Construction	therefore reduced Council of Australia 1996, p. 13) - 20.10 n 1996, p. 13) - 0% = 22.72 MJ/m2 Embodied Energy
		(Embodied Energy) Reduction	Standard
Measurable energy to rec in Building materials an elements		Recycled thermal insulation 16.43 MJ/m ² Reuse steel = 45.44 MJ/m2 Reduce in design 22.72 MJ/m2	425 MJ/ m ²
Total Walls	149.94 MJ/m2 234	84.59 MJ/m ²	425 MJ/ m ²

Table A.C.82: Green Star. Potential reduction in carbon emissions in a steel framed steel clad wall (Lawson 1996, p. 127)

Life Cycle Stages of	Co	onstruction	Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	on (Embodied Energy) Reduction	Basic
Measurable energy to	Steel frame from recycled	Reduce in design 22.72 MJ/m2	
reduce in Implementation	content 41.80 MJ/m2		$425 \text{ MJ}/\text{m}^2$
	Steel cladding from recycled		423 WIJ/ III
	content 78.93 MJ/m ²		
Green Star, Total Wall	120.73 MJ/m ²	22.72 MJ/m2	425 MJ/ m ²
Green Star, Totai wan	14	425 NJ/ III	

g. Timber Frame, Aluminium Weatherboard Wall

Table A.C.83: Potential reduction in carbon emissions in a timber framed aluminium weatherboard wall (Lawson 1996, p. 126)

Process	ses where carbon emissions	(embodied energy) can be red	luced
5 	Steel (Aluminium) from ave Jse Aluminium from recycled conte = 15.78 MJ/m² Jse Aluminium from recycled conte = 240.42 MJ/m² Reuse materials and elemen Reuse recycled timber and post-com 7.15+2.75+1.1) x 3.4 Mj/kg = 37.4 Jse recycled thermal insulation, 490	erage recycled content ents 0.0975 kg/m2 (170 Mj/kg new – 8.1 ents 1.485 kg/m2 (170 Mj/kg new – 8.1) nts (local salvage/re-use centre) sumer 60% FSC timber + Reuse the recy 0 MJ/m ² (Lawson 1996, p. 125; JLL 20 MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0	Mj/kg from recycled) Mj/kg from recycled) vcled timber 40% 12)
	MJ/m ² (Steel Construction Informat Green Star	10n 2014)	
	Material-8 Timber, Green Star Tech consumer recycled timber or FSC cc Reuse softwood + softwood plates + $3.4 \text{ Mj/kg x } 95\% = 35.53 \text{ MJ/m}^2$ Material-6 Green Star Technical Ma embodied energy by this credit (Stee 2008) is Jse Aluminium from recycled contect $x = 90\% = 14.20 \text{ MJ/m}^2$	ents (local salvage/re-use centre nical Manual, 95% of all timber product ertified timber - softwood weatherboard = 11 MJ/m ² (La nual, Steel is considered maximum 90% el from Recycled content) (Green buildin ents 0.0975 kg/m2 (170 Mj/kg new – 8.1) ents 1.485 kg/m2 (170 Mj/kg new – 8.1)	s re-used, post- awson 1996, p. 125) x , therefore reduced ng Council of Australia Mj/kg from recycled)
Life Cycle Stages of		onstruction	Embodied Energy
building	Pre-Construction	Construction	
		on (Embodied Energy) Reduction	Standard
Measurable energy to redu in Building materials and elements		Use recycled softwood 37.40 MJ/m ² Recycled thermal insulation 16.43 MJ/m ²	403 MJ/ m ²

Table A.C.84: Green Star. Potential reduction in carbon emissions in a timber framed aluminium weatherboard wall (Lawson 1996, p. 126).

Life Cycle Stages of	Co	nstruction	Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	n (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation	Aluminium from recycled contents = 14.20 MJ/m ² Aluminium from recycled contents = 216.37 MJ/m ²	Use recycled softwood + weatherboard 35.53 MJ/m ²	403 MJ/ m ²
	230.57 MJ/m ²	35.53 MJ/m ²	
Green Star, Total Wall	all 266.10 MJ/m ²		403 MJ/ m ²

h. Timber Frame, Clay Brick Veneer Wall

Table A.C.85: Potential reduction in carbon emissions in a timber framed clay brick veneer wall (Lawson 1996, p. 127).

Processes where carbon emissions (embodied energy) can be reduced				
	Reused the recycled aggregates			
	Reuse recycled aggregate for brick, 67% (Brick Development Association 2014; Tyrell & Goode 2014), 147 kg/m ² (Lawson, p.127) x 67% x 0.083 MJ/kg = 8.17 MJ/ m²			
Building materials and elements	 Reused materials and elements Use recycled softwood stud, 60% Reuse softwood stud@100x50mm+ softwood plates@100x50 mm (Lawson 1996, p.127) 60% x 33 MJ/m² = 19.8 MJ/m² Use recycled thermal insulation, 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.585kg/m² = 16.43 MJ/m² (Steel Construction Information 2014) 			
	Green Star Reuse materials and elements Use recycled softwood stud, 60% Reuse softwood stud@100x50mm+ softwood plates@100x50 mm = 60% x 33 MJ/m ² = 19.8 MJ/m ²			

Decreased and Replaced energy Decrease energy					
Implementation	water. Magaz	-made fly ash brick gains strength and durability from the chemical reaction of fly ash with ter. However, 85 per cent less energy is used in production than in fired clay brick, (Structure Igazine 2015); potential 40 per cent energy savings in brick manufacturing using 67% recycled Itainer glass brick grog (Brick Development Association 2014; Tyrell & Goode 2014).			
		ed energy 368 MJ/m ² x 40			
Life Cycle Stages of I	building		Construction	Embodied	
		Pre-Construction	Construction	Energy	
		Potential	Reduction in Carbon Emissions	Standard	
in Building materials and aggregate for brick MJ/m ²		60% softwood stud + softwood plates 19.8 MJ/m² Use Recycle thermal insulation 16.43 MJ/m²	5 61 MJ/ m ²		
			· · · · · · · · · · · · · · · · · · ·	-	
Implementation		40% saving energy in production 147.2 MJ/m ²			
		155 25 1/1 2	26 22 MAL 2		
Total Walls		155.37 KJ/m ²	36.23 MJ/m ²	561MJ/ m ²	
			191.60 MJ/m ²		

Table A.C.86: Green Star. Potential reduction in carbon emissions in a timber framed clay brick veneer wall (Lawson 1996, p. 127).

Life Cycle Stages of	Construction		Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	n (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation		60% softwood stud + softwood plates 19.80 MJ/m²	561 MJ/m ²
Green Star, Total Wall		19.80MJ/m ²	561 MJ/ m ²
Green Star, Totar Wall	19	9.80 MJ/m ²	501 WJJ/ III

i. Steel Frame, Clay Brick Veneer Wall

Table A.C.87: Potential reduction in carbon emissions in a steel framed clay brick veneer wall (Lawson 1996, p. 128).

Pro	cesses where carbon emissions (embodied energy) can be reduced
	Reuse recycled aggregates - Steel frame from average recycled content = 3.342 Kg x 34 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg = 3.342 KJ/Kg X 13.9 Kg/ m2 = 46.45 MJ/m2 - Use Aluminium from recycled contents 0.0975 kg/m2 (170 Mj/kg new – 8.1 Mj/kg from recycled) = 15.78 MJ/m ²
	 - Reuse recycled aggregate for brick, 67% (Brick Development Association 2014; Tyrell & Goode 2014) 147 kg/m² (Lawson 1996, p.127) x 67% x 0.083 MJ/kg = 8.17 MJ/ m²
Building materials and elements	Reused materials and elements- Use recycled thermal insulation, 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.585kg/m² = 16.43MJ/m² (Steel Construction Information 2014)Reuse 40% recycled steel 3.342 Kg x 34 MJ/Kg (Lawson 1996, p. 13) x 40% = 45.44 MJ/m2Reduced materials in designReduce 20% steel in design 3.342 Kg x 34 MJ/Kg (Lawson 1996, p. 13) x 20% = 22.72 MJ/m2
	Green Star Reuse materials and elements
	 Steel frame from average recycled content = 3.342 Kg x 34 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg = 3.342 KJ/Kg X 13.9 Kg/ m2 x 90% = 41.80 MJ/m2 Use Aluminium from recycled contents 0.0975 kg/m2 (170 Mj/kg new – 8.1 Mj/kg from recycled)
	x 90% = 15.78 MJ/m² Reduced materials in design Reduce 20% steel in design 3.342 Kg x 34 MJ/Kg (Lawson 1996, p. 13) x 20% = 22.72 MJ/m2

Life Cycle Stages of building	Cor	struction	Embodied
	Pre-Construction	Construction	Energy
	Potential reduction	on in carbon emissions	Standard
Measurable energy to reduce	Steel from recycled content	Use Recycle thermal insulation	
in Building materials and	46.45 MJ/m ²	16.43 MJ/m ²	
elements	Aluminium from recycled content 15.78 MJ/m²	Reuse steel = 45.44 MJ/m2	650MJ/ m ²
	76% Use recycled aggregate for brick 8.17 KJ/m²	Reduce in design 22.72 MJ/m2	
	·		
Total Walls	70.40 KJ/m ²	84.59 MJ/m ²	650MJ/ m ²
Total wans	154	.99 MJ/m ²	050IVIJ/ M-

Table A.C.88: Green Star. Potential reduction in carbon emissions in a steel framed clay brick veneer wall (Lawson 1996, p. 128)

Life Cycle Stages of	Co	Embodied	
building	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	n (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation	Steel from recycled content 41.80 MJ/m ² Aluminium from recycled content 14.20 MJ/m ²	Reduce in design 22.72 MJ/m2	650 MJ/m ²
	-		
Green Star, Total Wall	56 MJ/m ²	22.72 MJ/m2	650 MJ/ m ²
Green Star, Total Wall	78	8.72 MJ/m ²	0.0 MJ/ III

j. Timber Frame, Concrete Block Veneer Wall

Table A.C.89: Potential reduction in carbon emissions in a timber framed concrete block veneer wall (Lawson 1996, p. 128).

	Reused recycled aggregates
	Reuse recycled aggregate for brick, 100% (Brick Development Association 2014; Tyrell & Goode 2014), 137.5 kg/m ² (Lawson 1996, p.127) x 0.083 MJ/kg = 11.41 MJ/ m²
	- Use Aluminium from recycled contents 0.0975 kg/m2 (170 Mj/kg new – 8.1 Mj/kg from recycled) = 15.78 MJ/m ²
Building	Reused materials and elements
materials and	Use recycled softwood stud, 60% Reuse softwood stud@100x50mm+ softwood plates@100x50 mm,
elements	(Lawson 1996, p.127) 60% x 33 MJ/m ² = 19.8 MJ/m²
ciements	- Use recycled thermal insulation, 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.585kg/m ² = 16.43 MJ/m ² (Steel Construction Information 2014)
	Green Star
	Reuse materials and elements
	Use recycled softwood stud, 60% Reuse softwood stud@100x50mm+ softwood plates@100x50 mm = $60\% \times 33 \text{ MJ/m}^2 = 19.8 \text{ MJ/m}^2$

	Decrea	sed and Replaced energ	y in process			
	Decrease energy					
	Geopolyi 2010)	ner concrete brick or 100% rep	lacing with recycled results 80% reduction in	n GHG (Geiger		
Implementation			ete Block Association 2013) / 1000 x 137.5 = /kg (Lawson 1996, p.13) = 68.53 MJ/ m²	=12.23 Kg/m ²		
	Green Star - Use Aluminium from recycled contents 0.0975 kg/m2 (170 Mj/kg new – 8.1 Mj/kg from 90% = 15.78 MJ/m ² Reduced Cement = 89Kgs/tonne (Concrete Block Association 2013) / 1000 x 137.5 = 12 Reduced cement 12.23 Kg/ m ² x 5.6 MJ/kg (Lawson 2996, p.13) x 60% = 41.11 MJ/m ²					
Life Cycle Stages o		Construction		Embodied		
	-	Pre-Construction	Construction	Energy		
		Potential reduction in carbon emissions		Standard		
Measurable energy to reduce in Building materials and elements		76% Use recycled aggregate for brick 11.41 KJ/m² Aluminium from recycled content 15.78 MJ/m²	60% softwood stud + softwood plates 19.8 MJ/m² Use Recycle thermal insulation 16.43 MJ/m²	61 MJ/ m²		
Implementation		Replacing Geopolymer 68.53 MJ / m ²				
Total Walls		95.72 KJ/m²	36.23 MJ/m ²	361MJ/ m ²		
i otai vvalis		131.95 MJ/m ²		5011VIJ/ M ⁻		

Table A.C.90: Green Star. Potential reduction in carbon emissions in a timber framed concrete block veneer wall (Lawson 1996, p. 127).

Life Cycle Stages of	Construction			Embodied
building	Pre-Construction Construction			Energy
	Potential Carbon Emission (Em		Basic	
Measurable energy to	Replacing Geopolymer 41.11 MJ/ m ²	60% softwood stud + softwood		
reduce in Implementation	Aluminium from recycled content	plates 19.80 MJ/m ²		361 MJ/m ²
	15.78 MJ/m ²			
Crean Star Tatal Wall	56.89 MJ/m ²	19.80MJ/m ²		361 MJ/ m ²
Green Star, Total Wall	76.69 MJ/m ²			301 IVIJ/ III

k. Steel Frame, Concrete Block Veneer Wall

Table A.C.91: Potential reduction in carbon emissions in a steel framed concrete block veneer wall (Lawson 1996, p. 128).

Pro	ocesses v	vhere carbon emissions	(embodied energy) can be reduce	d	
	Reuse	recycled aggregates			
	Reuse ree	cycled aggregate for brick, 100	% (Brick Development Association 2014; Ty 7) x 0.083 MJ/kg = 11.41 MJ/ m²	rell & Goode	
Building materials and	- Steel frame from average recycled content = $3.342 \text{ Kg x} 34 \text{ MJ/Kg}$ (Lawson 1996, p.13) - 20.10 MJ/Kg = $3.342 \text{ KJ/Kg x} 13.9 \text{ Kg/m2} = 46.45 \text{ MJ/m2}$ - Use Aluminium from recycled contents 0.0975 kg/m2 (170 Mj/kg new – 8.1 Mj/kg from recycled) = 15.78 MJ/m ² Reused materials and elements - Use recycled thermal insulation, 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.65kg/m ² = 18.25 MJ/m ² (Steel Construction Information 2014) Reuse 40% recycled steel $3.342 \text{ Kg x} 34 \text{ MJ/Kg}$ (Lawson 1996, p. 13) x 40% = 45.44 MJ/m2				
elements		d materials in design 0% steel in design 3.342 Kg x 3	34 MJ/Kg (Lawson 1996, p. 13) x 20% = 22.7	72 MJ/m2	
	Green		• · · · · · ·		
	Reuse materials and elements - Steel frame from average recycled content = 3.342 Kg x 34 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg = 3.342 KJ/Kg X 13.9 Kg/ m2 x 90% = 41.80 MJ/m2 - Use Aluminium from recycled contents 0.0975 kg/m2 (170 Mj/kg new – 8.1 Mj/kg from recycled) x 90% = 15.78 MJ/m ²				
		ed materials in design			
		0	34 MJ/Kg (Lawson1996, p. 13) x 20% = 22.	72 MJ/m2	
Implementatio	Decrea Geopolyn 2010) Reduced	gy in process lacing with recycled results 80% reduction in ete Block Association 2013) / 1000 x 137.5 = /kg (Lawson 1996, p.13) = 68.53 MJ/ m ²			
	Green Reduced	Star Cement =89Kgs/tonne (Concre	te Block Association 2013) / 1000 x 137.5 = /kg (Lawson 1996, p. 13) x 60% = 41.11 MJ	. 0	
Life Cycle Stages of		Ū	Construction	Embodied	
		Pre-Construction	Construction	Energy	
Maagumahla anarree t	o modulos		Iction in carbon emissions	Standard	
Measurable energy to reduce in Building materials and elements		 76% Use recycled aggregate for brick 11.41 KJ/m² Steel from recycled content46.45 MJ/m2 Aluminium from recycled content 15.78 MJ/m² 	Use Recycle thermal insulation 18.25 MJ/m ² Reuse recycled steel 45.44 MJ/m2 Reduce steel use in design 22.72 MJ/m2	453MJ/ m ²	
Implementation	1	Replacing Geopolymer 68.53 MJ/ m²			
Total Walls	;	142.17 KJ/m ²	86.41 MJ/m ² 228.58 MJ/m ²	453MJ/ m ²	

Table A.C.92: Green Star. Potential reduction in carbon emissions in a steel framed concrete block veneer wall (Lawson 1996, p. 127).

Life Cycle Stages of	Constru	Embodied	
building	Pre-Construction	Construction	Energy
	Potential Carbon Emission (E	mbodied Energy) Reduction	Basic
Measurable energy to	Replacing Geopolymer 41.11 MJ/	Steel from recycled content 41.80	
reduce in Implementation	m^2	MJ/m2	453 MJ/m ²
_	Aluminium from recycled content	Reduce steel use in design 22.72	455 MJ/III
	14.20 MJ/m ²	MJ/m2	
Green Star, Total Wall	56.89 MJ/m ²	64.52 MJ/m ²	453 MJ/ m ²
Green Star, Total wan	121.41	MJ/m ²	455 IVIJ/ III

<u>l. Steel Frame, timber weatherboard Wall</u>

Table A.C.93: Potential reduction in carbon emissions in a steel framed timber weatherboard wall (Lawson 1996, p. 125)

Proc	esses where carbon emissi	ons (embodied energy) can be redu	iced
	MJ/Kg = 3.342 KJ/Kg X 13.9 K - Use Aluminium from recycled recycled) = 15.78 MJ/m² Reuse materials and eler Reuse softwood + softwood plat JLL 2012) - Use recycled thermal insulation MJ/m² (Steel Construction Infor Reuse 40% recycled steel 3.342 I	eled content = 3.342 Kg x 34 MJ/Kg (Lawson g/ m2 = 46.45 MJ/m2 contents 0.0975 kg/m2 (170 Mj/kg new – 8.1 ments (local salvage/re-use centre) es + softwood weatherboard = 74 MJ/m ² (La , 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.0 mation 2014) Kg x 34 MJ/Kg (Lawson 1996, p. 13) x 40% =	Mj/kg from wson 1996, p. 125; 55kg/m ² = 18.25
Building	Reuse materials in design		
materials and		2 Kg x 34 MJ/Kg (Lawson 1996, p. 13) x 209	% = 22.72 MJ/m2
elements	Green Star		
	reduced embodied energy by thi Council of Australia 2008) is: - Steel frame roofing from recyc 17.5 MJ/Kg x 3.342 kg/ m ² x 90 Reuse materials and eler Material-8 Timber, Green Star T consumer recycled timber or FS Reuse softwood + softwood plat 70.3 MJ/m²	 chnical Manual, steel is considered maximum s credit (Steel from 90% Recycled contents) (led content {34 MJ/Kg (Lawson 1996, p. 135 % = 41.80 MJ/m² ments (local salvage/re-use centre) cennical Manual, 95% of all timber products 	Green building) – 21.5 MJ/Kg} = re-used, post- yson p. 125) x 95% =
Life Cycle Stages		Construction	Embodied Energy
building	Pre-Construction	Construction	
		ission (Embodied Energy) Reduction	Standard
Measurable energy to re in Building materials a elements		Use recycled softwood + weatherboard 74 MJ/m ² Use Recycle thermal insulation 18.25 MJ/m ² Reuse recycled steel 45.44 MJ/m2 Reduce steel use in design 22.72 MJ/m2	238 MJ/ m ²
Total Walls	62.23 MJ/m ²	160.41 MJ/m ² 222.64 MJ/m ²	238 MJ/ m ²

Table A.C.94: Green Star. Potential reduction in carbon emissions in a steel framed timber weatherboard wall (Lawson 1996, p. 125).

Life Cycle Stages of	Co	Embodied	
building	Pre-Construction	Energy	
	Potential Carbon Emissio	on (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation	Steel frame from 90% Recycled contents = 41.80 MJ/m² Use recycled softwood + weatherboard 70.30 MJ/m² Reduce steel use in design 22.72 MJ/m2		151MJ/ m ²
	41.80 MJ/m ²	93.02 MJ/m ²	
Green Star, Total Wall		4.82 MJ/m ²	151MJ/ m ²

m. Cavity Clay Brick Wall

Table A.C.95: Potential reduction in carbon emissions in a cavity clay brick wall (Lawson 1996, p. 129)

Proc	esses w	where carbon emissions (embodie	d energy) can be reduced	l		
	Reuse	e recycled aggregates				
		recycled aggregate for brick, 67% (Brick D 291 kg/m ² (Lawson 1996, p.127) x 67% x (rell & Goode		
Building materials and		Aluminium from recycled contents 0.0975 k 3 MJ/m ²	g/m2 (170 Mj/kg new – 8.1 Mj/k	g from recycled)		
elements	Gree	n Star				
	- Use A	e materials and elements Aluminium from recycled contents 0.0975 k = 14.20 MJ/m ²	g/m2 (170 Mj/kg new – 8.1 Mj/k	g from recycled)		
	Decre	eased and Replaced energy in pro	DCess			
	Decre	ease energy				
	water. I	US-made fly ash brick gains strength and durability from the chemical reaction of fly ash with water. However, 85 per cent less energy is used in production than in fired clay brick, (Volz & Stovner 2010; Structure Magazine 2015).				
	Potential 40 per cent energy savings in brick manufacturing using 67% recycled container glass brick grog (Brick Development Association 2014; Tyrell & Goode 2014).					
Implementation	- Geopo (Geiger 89Kgs/	Reduced energy 728 MJ/m ² x 40% = 291.2 MJ/m ² - Geopolymer mortar or replacing Portland with geopolymer cement results 80% reduction in GHG (Geiger 2010), Reduced Cement = 89Kgs/tonne (Concrete Block Association 2013) / 1000 x 50.224 = 4.45 Kg/m ² Reduced cement 4.45 Kg/ m ² x 5.6 MJ/kg (Lawson 1996, p. 13) = 24.92 MJ/m²				
	Green	Green Star				
		ing maximum 60% of cement (Green buildi t/m2 x 60% x 5.6 MJ/kg (Lawson 1996, p.		45 kg		
Life Cycle Stages of	building	Construction		Embodied		
		Pre-Construction	Construction	Energy		
		Potential reduction in car	bon emissions	Standard		
Measurable energy to in Building materials	and	76% Use recycled aggregate for brick 8.17 KJ/m²		854MJ/ m ²		
elements		Aluminium from recycled content 15.78 MJ/m ²		0541 01 3/ 111		
Implementation		40% saving energy in production 291.2 MJ/m ² Replacing geopolymer = 24.92 MJ/ m ²				
		340.07 KJ/m ²				
Total Walls		340.07 KJ/III		854MJ/ m ²		

Table A.C.96: Green Star. Potential reduction in carbon emissions in a cavity clay brick wall (Lawson 1996, p. 129).

Life Cycle Stages of	Construction		Embodied
building	Pre-Construction	Energy	
	Potential Carbon Emissio	Basic	
Measurable energy to reduce in Implementation	Aluminium from recycled Replacing geopolymer = 14.95MJ/ m ²		854 MJ/m ²
Green Star, Total Wall	14.20 MJ/m ²	14.95 MJ/m ²	854 MJ/ m ²
Green Star, Total wan	2	9.15 MJ/m ²	054 IVIJ/ III

n. Cavity Concrete Block Wall

Table A.C.97: Potential reduction in carbon emissions in a cavity concrete block wall (Lawson 1996, p, 129).

Pr	ocesses w	here carbon emissions (embodied energy) can be red	uced		
	Reuse r	Reuse recycled materials as aggregate for concrete block				
	- Concrete 0.083 MJ		e (Uche 2008; PCA 2014), embodied e	nergy of aggregate is		
Building	Saved em		gy of aggregate 0.083 MJ/Kg x (299.57 8 MJ/m ²	Kg concrete – 41.93		
materials and	Green S	Star				
elements	Reuse r	ecycled materials for co	ncrete block			
		,	is considered maximum 20%, therefore			
	energy by 2008) is:	this credit (Concrete from 20%	Recycled aggregate) (Green building G	Council of Australia		
			gy of aggregate 0.083 MJ/Kg x (299.57	7 Kg concrete – 24.47		
	kg cemen	t) (Lawson 1996, p. 129) x 20%	$= 4.27 \text{ MJ/m}^2$			
Implementation	Geopolyn (Geiger 20 Reduced 0	eplaced cement eopolymer concrete block or 100% replacing recycled cement results 80% reduction in GHG ieiger 2010) educed Cement = 89Kgs/tonne (Concrete Block Association 2013) / 1000 x 275 = 24.47 Kg/ m ² educed cement 41.93 Kg/ m ² x 5.6 MJ/kg (Lawson1996, p. 13) = 234.80 MJ/ m²				
	Replacing	g maximum 60% of cement (Gre	en building Council of Australia 2008)			
Life Cycle Stages			(Lawson 1996, p. 13) = 140.88 MJ / m ²	Embodied Energy		
Life Cycle Stages	or building	Pre-Construction	Construction	Basic		
			on (embodied energy) to reduce			
Measurable energy to reduce in Building materials and elements		Use recycled materials as aggregate 21.38 MJ/ m²		511 MJ/ m ²		
Measurable energy t Implementation	o reduce in		Geopolymer, replacing 100% of cement 234.80 MJ/m²			
		21.38 MJ/ m ²	234.80 MJ/ m ²			
Total Wal	ls		6.18 MJ/m ²	511MJ/ m ²		

Table A.C.98: Green Star. Potential reduction in carbon emissions in a cavity concrete block wall (Lawson 1996, p. 129).

Life Cycle Stages of	Construction		Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	on (Embodied Energy) Reduction	Basic
Measurable energy to	20% Recycled aggregate for		511 MJ/m ²
reduce in Implementation	concrete block = 4.27 MJ/m^2		511 WJ/III
Measurable energy to reduce		Geopolymer, 60% Cement Replacement	
in Implementation		140.88 MJ/m ²	
Crean Stan Tatal Wall	4.27 MJ/m ²	140.88 MJ/m ²	511 MJ/
Green Star, Total Wall	14	15.15 MJ/m ²	m ²

o. Single Skin Stabilized Rammed Earth Wall

Table A.C.99: Potential reduction in carbon emissions in a single skin stabilized rammed earth wall (Lawson 1996, p. 130).

	Proce	sses where carbon emissi	ons (embodied energy) can be reduced		
	Decreas	sed and Replaced en	ergy in process		
	Replaced				
	1 .	ner Concrete or 100% rep in GHG (McLellan et al. 2	lacing with recycled cement (Nath & Sarker 011)	2014) results 97%	
	570 kg/m ²	2 (Lawson 1996, p. 124) x 3	5% Cement (Lawson 1996, p. 41) = 28.5 kg re	eplaced cement/ m ²	
Implementation	28.5 kg C	ement/m ² x 5.6 MJ/kg (Lav	wson 1996, p.13) = 273.72 MJ / m ²		
	Green S	Star			
	Replacing	60% of cement (Green bu	ilding Council of Australia 2008)		
	570 kg/m^2 (Lawson 1996, p. 124) x 5% Cement (Lawson 1996, p. 41) x 60% = 17.10 kg replaced				
		cement/ m ²			
	17.10 kg (Cement/m ² x 5.6 MJ/kg (La	awson 1996, p.13) = 95.76 MJ/ m²		
Life Cycle Stages	of building		Construction	Embodied Energ	
		Pre-Construction	Construction	Basic	
		Potential reduction in	n carbon emissions (embodied energy)		
Measurable energy	to reduce		Replacing geopolymer = 273.72 MJ/ m ²		
in Building materials and				405MJ/ m ²	
elements					
			273.72 MJ/ m ²	4053 534 2	
Total Walls		273 72 MI/m ²		405MJ/ m ²	

Table A.C.100: Green Star. Potential reduction in carbon emissions in a single skin stabilized rammed earth wall (Lawson 1996, p. 129).

273.72 MJ/m²

Life Cycle Stages of	Co	onstruction	Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	on (Embodied Energy) Reduction	Basic
Measurable energy to		Replacing geopolymer = 95.76MJ/ m2	405 MJ/m ²
reduce in Implementation			405 MJ/m-
Crean Star Tatal Wall		95.76 MJ/m ²	405 MJ/ m ²
Green Star, Total Wall	95.76 MJ/m ²		405 IVIJ/ M

p. Single Skin autoclaved Aerated Concrete Block (AAC) wall

Table A.C.101: Potential reduction in carbon emissions in a single skin autoclaved aerated concrete block (AAC) wall (Lawson 1996, p. 129).

	Proce	sses where carbon emissions	(embodied energy) can be reduced				
	Reused recycled materials as aggregate for concrete block						
		- Concrete from 800% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg					
Building	Saved em	bodied energy = embodied ene	rgy of aggregate 0.083 MJ/Kg x (102 + 96, 9. 129) x 80% = 9.76 MJ/m²	8.11+ 18.98) Kg			
materials and	Green S	Star					
elements	Reuse r	ecycled materials for co	oncrete block				
			, is considered maximum 20%, therefore				
	energy by 2008) is:	this credit (Concrete from 20%	6 Recycled aggregate) (Green building C	Council of Australia			
			rgy of aggregate 0.083 MJ/Kg x (129.09	Kg concrete – 11.49			
	kg cemen	t) (Lawson 1996, p. 129) x 20%	$b = 1.95 \text{ MJ/m}^2$				
	Decress	sed and Replaced energ	v in process				
	Decreased and Replaced energy in process Replaced cement						
	Geopolymer concrete block or 100% replacing with recycled cement results 80% reduction in GHG						
	(Geiger 2010)						
Implementation	Reduced Cement = 89 Kgs/tonne Concrete Block Association 2013) / 1000 x 129.09 = 11.49 Kg/m ² Reduced compart 11 40 Kg/m ² x 5.6 MU/cg (Lawson 1006 p 12) = 64.24 MU/m ²						
	Reduced cement 11.49 Kg/ m ² x 5.6 MJ/kg (Lawson 1996, p. 13) = 64.34 MJ/ m² Green Star						
	Green Star Replacing max. 60% of cement (Green building Council of Australia 2008)						
	11.49 kg Cement/m2 x 60% x 5.6 MJ/kg (Lawson1996, p. 13) = 38.60 MJ/m²						
Life Cycle Stages	of building	C	onstruction	Embodied Energ			
		Pre-Construction	Construction	Basic			
			on (embodied energy) reduction				
Measurable energy		Use recycled materials as aggregate 9.76 MJ/ m ²		440MJ/ m ²			
in Building materials and elements		aggregate 9.70 MJ/ III		4401913/ 111			
		1					
Measurable energy to reduce in Implementation			Geopolymer, replacing 100% of cement 64.34 MJ/m²				
		9.76 MJ/ m ²	64.34 MJ/ m ²				
Total Wal	ls		4.10 MJ/m ²	440MJ/ m ²			

Table A.C.102: Green Star. Potential reduction in carbon emissions in a single skin autoclaved aerated concrete block (AAC) wall (Lawson 1996, p. 129).

74.10 MJ/m²

Life Cycle Stages of	Construction		Embodied
building j	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	on (Embodied Energy) Reduction	Basic
Measurable energy to	20% Recycled aggregate for		440 MJ/m ²
reduce in Implementation	concrete block = 1.95 MJ/m^2		440 MJ/m ⁻
Measurable energy to reduce		Geopolymer, 60% Cement Replacements	
in Implementation		38.60 MJ/m ²	
Conserv Steve Tetal Wall	1.95 MJ/m ²	38.60 MJ/m ²	440 MI/2
Green Star, Total Wall	4	0.55 MJ/m ²	440 MJ/ m ²

q. Single Skin Cored Concrete Block Wall

Table A.C.103: Potential reduction in carbon emissions in a single skin cored concrete block wall (Lawson 1996, p. 129).

	Proce	esses where carbon emissions (embodied energy) can be reduced		
	Reuse recycled materials as aggregate for concrete block				
Building			e (Uche 2008; PCA 2014), embodied e	energy of aggregate is	
		6	gy of aggregate 0.083 MJ/Kg x (175 +) = 14.80 MJ/m ²	1.6+ 1.8) Kg concrete	
materials and	Green S	Star			
elements	Reused	recycled materials for o	concrete block		
	energy by 2008) is:	this credit (Concrete from 20%	is considered maximum 20%, therefore Recycled aggregate) (Green building (gy of aggregate 0.083 MJ/Kg x (1178.4	Council of Australia	
		cement) (Lawson 1996, p. 129)		to hig concrete	
	Ũ				
Implementation	Decreased and Replaced energy in process Replaced cement Geopolymer concrete block or 100% replacing with recycled cement results 80% reduction in GHG (Geiger 2010) Reduced Cement = 89 Kgs/tonne (Concrete Block Association 2013) / 1000 x 178.40 = 15.88 Kg/ m ² Reduced cement 15.88 Kg/ m ² x 5.6 MJ/kg (Lawson 1996, p. 13) = 88.91 MJ/ m²				
	Green Star				
	Replacing max. 60% of cement (Green building Council of Australia 2008) 15.88 kg Cement/m2 x 60% x 5.6 MJ/kg (Lawson 1996, p. 13) = 53.34 MJ/ m ²				
Life Cycle Stages		2	$(Lawson 1996, p. 13) = 53.34 \text{ MJ/ m}^2$	Embodied Energy	
Life Cycle Stages	or building	Pre-Construction	Construction	Basic	
			n (embodied energy) reductions		
Measurable energy to reduce in Building materials and elements		Use recycled materials as aggregate 14.80 MJ/ m²	,	317MJ/ m ²	
Measurable energy to reduce in Implementation			Geopolymer, replacing 100% of cement 88.91 MJ/m²		
		14.80 MJ/ m ²	88.91 MJ/ m ²		
Total Walls		10	3.71 MJ/m ²	317MJ/ m ²	

Table A.C.104: Green Star. Potential reduction in carbon emissions in a single skin cored concrete block wall (Lawson 1996, p. 129)

Life Cycle Stages of		Embodied	
building j	Pre-Construction	Construction	Energy
	Potential Carbon Emiss	sion (Embodied Energy) Reduction	Basic
Measurable energy to	20% Recycled aggregate for		317 MJ/m ²
reduce in Implementation	concrete block = 2.96 MJ/m^2		517 WJ/III
N 11 / 1			
Measurable energy to reduce in Implementation		Geopolymer 60% Cement Replacement 53.34 MJ/m ²	
Green Star, Total Wall	2.96 MJ/m ²	53.34 MJ/m ²	317 MJ/ m ²
Green Star, Totai wan	56.30 MJ/m ²		517 WJ/ III

r. Steel Frame, Compressed Fibre Cement Clad Wall

Table A.C.105: Potential reduction in carbon emissions in a steel framed compressed fibre cement clad wall (Lawson 1996, p. 129)

Pr	Processes where carbon emissions (embodied energy) can be reduced					
Building materials and elements	Reused the recycled aggregates- Steel frame from average recycled content = $(3.552 + 3.06)$ Kg x 38 MJ/Kg (Lawson 1996, p, 13) - 20.10 MJ/Kg = 6.612 KJ/Kg x 17.9 Kg/ m2 = 118.35 MJ/m2Reused materials and elementsReuse 40% recycled steel, 6.612 Kg x 38 MJ/Kg (Lawson 1996, p.13) x 40% = 100.50 MJ/m2recused materials in designReduce 20% steel in design 6.612 Kg x 38 MJ/Kg (Lawson 1996, p. 13) x 20% = 50.25 MJ/m2Green StarReuse materials and elements- Steel frame from average recycled content = 6.612 Kg x 38 MJ/Kg (Lawson 1996, p. 13) - 20.10MJ/Kg = 6.612 KJ/Kg X 17.9 Kg/ m2 x 90% = 106.51 MJ/m2Reused materials in designReused materials in designReused materials in designReused materials and elements- Steel frame from average recycled content = 6.612 Kg x 38 MJ/Kg (Lawson 1996, p. 13) - 20.10MJ/Kg = 6.612 KJ/Kg X 17.9 Kg/ m2 x 90% = 106.51 MJ/m2Reused materials in designReused materials in designReduce 20% steel in design 6.612 Kg x 38 MJ/Kg (Lawson 1996, p. 13) x 20% = 50.25 MJ/m2					

	Decrea	sed and Replaced energ	gy in process		
	Decrease energy				
	Geopoly	mer or 100% replacing cement	results 80% reduction in GHG (Geiger 2010)		
Implementation		Cement = 14% x 16.9 = 2.366 K			
implementation	Reduced	cement 2.366 Kg/ m ² x 5.6 MJ	/kg (Lawson 1996, p.13) = 13.24 MJ / m^2		
	Green	Star			
	Replacin	g with geopolymer, Reduced C	ement = 14% x 16.9 = 2.366 Kg/m2		
	Reduced	cement 2.366 Kg/ m ² x 5.6 MJ	/kg (Lawson 1996, p. 13) x 60% = 7.94 MJ / m	n ²	
Life Cycle Stages o	f building	Construction		Embodied	
		Pre-Construction	Construction	Energy	
		Potential Reduction in Carbon Emissions		Standard	
Measurable energy to	o reduce	Steel from recycled content	Reuse recycled steel 100.50 MJ/m2		
in Building materia elements	ls and	118.35 MJ/m2	Reduce steel use in design 50.25 MJ/m2	385MJ/ m ²	
		1			
Implementation		Replacing Geopolymer 13.24 MJ/ m ²			
Total Walls	2	131. 59 KJ/m ²	150.75 MJ/m ²	385MJ/ m ²	
Total Walls		282.34 MJ/m ²		565MJ/ III	

Table A.C.106: Potential reduction in carbon emissions in a steel framed compressed fibre cement clad wall (Lawson 1996, p. 129).

Life Cycle Stages of	Construction		Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emission (E	mbodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation	Replacing Geopolymer 7.94 MJ/m ²	Steel from recycled content 106.51 MJ/m2 Reduce steel use in design 50.25 MJ/m2	385 MJ/m ²
	7.94 MJ/m ²	150.76 MJ/m ²	
Green Star, Total Wall		MJ/m ²	385 MJ/ m ²

s. 200 mm Hollow-Core Precast Concrete Wall

Table A.C.107: Potential reduction in carbon emissions in a 200-mm hollow core precast concrete slab wall (Lawson 1996, p. 125-126).

Proce	sses wh	ere carbon emissions (em	bodied energy) can be reduced	l
	Reused	the recycled aggregates for con	crete	
Building materials and elements - Concr is 0.083 Saved e 41.79kg Steel fr - Steel 1 1996, p Green 1 Materia embodi Counci - Concr is 0.083 saved e		MJ/Kg mbodied energy = embodied energy (m ² cement) (Lawson 1996, p. 12 om average recycled content nesh +Edge beams from average . 13) - 20.10 MJ/Kg} = 47.70 MJ Star recycled aggregate for concrete 1-5 Green Star Technical Manual, ed energy by this credit (Concrete of Australia 2008) is: ete from 20% Recycled aggregate MJ/Kg mbodied energy = embodied ener	e (Uche 2008; PCA 2014), embodied energy of aggregate 0.083MJ/Kg x (298.5 kg 25) x 80% = 17.04 MJ/m² recycled content = 3.432 Kg x {34 MJ/k /m ² , is considered maximum 20%, therefore e from 20% Recycled aggregate) (Green e (Uche 2008; PCA 2014) embodied ener gy of aggregate 0.083 MJ/Kg x (298.50	g/m ² concrete – Cg (Lawson reduced building rgy of aggregate
	Steel fr Materia embodi Australi	ed energy by this credit (Steel fro a 2008) is:	 25) x 20% = 4.26 MJ/m² is considered maximum 90%, therefore m Recycled content) (Green building Co 96, p. 13) - 20.10 MJ/Kg} = 42.93MJ/m 	uncil of
ImplementationDecreased and Replaced energy Replaced cement Geopolymer Concrete or 100% replacing with recycle 97% reduction in GHG (McLellan et al. 2011) 298.50 kg/m² (Lawson 1996, p. 124) x 14% Cement (Law cement/ m² in concrete 41.79 kg Cement/m2 x 5.6 MJ/kg (Lawson 1996, p. 13) = Green Star Replacing maximum 60% of cement (Green building Co 298.50kg/m² (Lawson 1996, p. 124) x 14% Cement (Law cement/ m² in concrete			2011) 4% Cement (Lawson 1996, p. 41) = 41.7 on 1996. p. 13) = 234.02 MJ/ m² een building Council of Australia 2008)	9 kg replaced
Life Cycle Stages of bu		•	nstruction	Embodied
Life Cycle Stages Of Du	nung	Pre-Construction	Construction	Energy
			ion in carbon emissions	Standard
Measurable energy to reduce in Building materials and elements		80 % Concrete from recycled aggregate = 17.04 MJ/m ²	100% Steel, beams from average recycled content = 47.70 MJ/m^2	908 MJ/m ²
Measurable energy to re Implementation	duce in		Geopolymer, replacing 100% of cement = $234.02 \text{ MJ}/\text{m}^2$	
		17 04 3411.2	101 70 3431 ?	
Total Floor		17.04 MJ/m ²	281.72 MJ/m ²	
Total Floor			8.76 MJ/m ²	908MJ/ m ²

Table A.C.108: Green Star. Potential reduction in carbon emissions in a 200-mm hollow core precast concrete slab wall (Lawson 1996, p. 125)

Life Cycle Stages of	Co	Embodied	
building	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	n (Embodied Energy) Reduction	Basic
Measurable energy to	20% Recycled aggregate for	90% Steel mesh from average recycled	908 MJ/m ²
reduce in Implementation	concrete = 4.26 MJ/m^2	content 42.93 MJ/m²	908 IVIJ/III
Measurable energy to reduce		Geopolymer, 60% Cement Replacements	
in Implementation		140.41 MJ/m ²	
Crean Star Tatal Elsan	4.26 MJ/m ²	183.34 MJ/m ²	908 MJ/ m ²
Green Star, Total Floor	187.60 MJ/m ²		908 IVIJ/ III

t. 150 mm Tilt-up Precast Concrete Wall

Table A.C.109: Potential reduction in carbon emissions in a tilt-up precast concrete wall (Lawson 1996, p. 131).

]	Processes where carbon emissions (embodied energy) can be reduced
	Reuse recycled aggregates for concrete
	 Concrete from 80% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083MJ/Kg x (360 kg/m²concrete - 50.14 kg/m² cement) (Lawson 1996, p. 125) x 80% = 20.57 MJ/m² Steel from average recycled content Steel from average recycled content = 4 Kg x {34 MJ/Kg (Lawson1996, p. 13) - 20.10 MJ/Kg} =
Building	55.60 MJ/m ² Green Star
materials	Reused recycled aggregate for concrete
and elements	Material-5 Green Star Technical Manual, is considered maximum 20%, therefore reduced embodied energy by this credit (Concrete from 20% Recycled aggregate) (Green building Council of Australia 2008) is:
	 Concrete from 20% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg
	saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (360 kg/m ² concrete – 50.14 kg/m ² cement) (Lawson 1996, p. 125) x 20% = 5.14 MJ/m²
	Steel from average recycled content Material-6 Green Star, Steel is considered maximum 90%, therefore reduced embodied energy by this credit (Steel from Recycled content) (Green building Council of Australia 2008) is:
	4 Kg x 90% {34 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg} = 50.40MJ/m²

	Decreased	and Replaced energy in	process			
	Replaced cement					
			ent (Nath & Sarker 2014) results 97% re	duction in GHG		
	(McLellan et a	1 0	, , , , , , , , , , , , , , , , , , , ,			
	360 kg/m ² (La	awson 1996, p. 124) x 14% Ceme	ent (Lawson 1996, p. 41) = 50.14 kg repla	ced cement/ m ²		
Implement	in concrete	• ·				
ation	50.14 kg Cem	ent/m2 x 5.6 MJ/kg (Lawson 119	96, p. 13) = 280.78 MJ / m ²			
	Green Star	r				
	Replacing ma	ximum 60% of cement (Green bu	ilding Council of Australia 2008)			
	298.50kg/m^2 ((Lawson 1996, p. 124) x 14% Cer	ment (Lawson 1996, p. 41) 60% = kg rep	laced cement/		
	m ² in concrete	m ² in concrete				
	32 kg Cement	/m ² x 5.6 MJ/kg (Lawson 1996, J	b. 13) x 60% =168.48 MJ/ m ²			
Life Cycle Stage	es of building	Construction		Embodied		
		Pre-Construction	Construction	Energy		
		Potential reduct	ion in carbon emissions	Standard		
Measurable ener		Concrete from 80% recycled	Steel from 100% average recycled			
Building materi	ials and	$aggregate = 20.57 \text{ MJ/m}^2$	$content = 55.60 \text{ MJ/m}^2$	818 MJ/m ²		
elements						
Measurable energ	av to reduce in		Geopolymer, replacing 100% of			
Implementation			$cement = 280.78 \text{ MJ/ }m^2$			
• • • • • • • • • • • • • • • • • • •						
Total	Floor	20.57 MJ/m ²	336.38 MJ/m ²	818MJ / m		
Total Floor		356.95 MJ/m ²		0101013/ 11		

Table A.C.110: Green Star. Potential reduction in carbon emissions in a tilt-up precast concrete wall (Lawson 1996, p. 125).

Life Cycle Stages of	Construction		Embodied	
building	Pre-Construction	Construction	Energy	
	Potential Carbon Emissio	on (Embodied Energy) Reduction	Basic	
Measurable energy to	Concrete from 20% recycled	Steel mesh from 100% average recycled	818 MJ/m ²	
reduce in Implementation	$aggregate = 5.14 \text{ MJ/m}^2$	content 50.40 MJ/m ²	010 IVIJ/III	
Measurable energy to reduce		Geopolymer, 60% Cement Replacements		
in Implementation		168.48 MJ/m ²		
Crean Stan Total Flags	5.14 MJ/m ²	218.88 MJ/m ²	818 MJ/ m ²	
Green Star, Total Floor	224.02 MJ/m ²		010 NIJ/ M-	

u. Porcelain-Enamelled Steel Curtain Wall

Table A.C.111: Potential reduction in carbon emissions in a porcelain-enamelled steel curtain wall (Lawson 1996, p. 131).

Processes where carbon emissions (embodied energy) can be reduced				
Building materials and elements	Reused the recycled aggregates- Steel frame from average recycled content = $(2.43 + 4.31)$ Kg x 38 MJ/Kg (Lawson 1996. p. 13) -20.10 MJ/Kg = 6.74 KJ/Kg x 17.9 Kg/ m2 = 120.64 MJ/m2- Enamelled Steel facing from average recycled content = 4.86 Kg x 38 MJ/Kg (Lawson 1996, p. 13) -20.10 MJ/Kg = 4.86 KJ/Kg x 17.9 Kg/ m2 = 86.99 MJ/m2Use Aluminium from recycled contents 1.62 kg/m2 (170 Mj/kg new – 8.1 Mj/kg from recycled) = 262.27 MJ/m²reduced materials in designReduce 20% steel in design 6.74 Kg x 38 MJ/Kg (Lawson 1996, p. 13) x $20\% = 51.22$ MJ/m2Green StarReused materials and elements- Steel frame from average recycled content = 6.74 Kg x 38 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg = 6.74 KJ/Kg x 17.9 Kg/ m2 x $90\% = 108.58$ MJ/m2- Enamelled Steel facing from average recycled content = 4.86 Kg x $(38$ MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg = 4.86 KJ/Kg x 17.9 Kg/ m2 x $90\% = 78.29$ MJ/m2- Enamelled Steel facing from average recycled content = 4.86 Kg x $(38$ MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg = 4.86 KJ/Kg x 17.9 Kg/ m2 x $90\% = 78.29$ MJ/m2Use Aluminium from recycled contents 1.485 kg/m2 $(170$ Mj/kg new – 8.1 Mj/kg from recycled) x $90\% = 236.05$ MJ/m²Reused materials in designReduce 20% steel in design 6.74 Kg x 38 MJ/Kg (Lawson 1996, p. 13) x $20\% = 51.22$ MJ/m2			

Implementation	Decreased and Replaced energy in process Decrease energy Geopolymer or 100% replacing with recycled cement results 80% reduction in GHG (Geiger 2010) Reduced Cement = $14\% x 14 \text{ kg/m}^2 = 1.96 \text{ Kg/m}^2$ Reduced cement 1.96 Kg/ m ² x 5.6 MJ/kg (Lawson 1996, p. 13) = 10.97 MJ/ m ² Green Star Replacing geopolymer or recycled cement = $14\% x 16.9 = 2.366 \text{ Kg/m}^2$ Reduced cement 1.96 Kg/ m ² x 5.6 MJ/kg (Lawson 1996, p. 13) x 60% = 6.58 MJ/ m ²				
Life Cycle Stages of	f building	Construct	ion	Embodied	
		Pre-Construction	Construction	Energy	
		Potential reduction in C	Carbon Emissions	Standard	
Measurable energy to reduce in Building materials and elements		Steel from recycled content 120.64 MJ/m² Enamelled steel from recycled content 86.99 MJ/m² Aluminium from recycled content 262.27 MJ/m²	Reduce steel use in design 51.22 MJ/m2 Geopolymer replaced 10.97 MJ/m ²	865MJ/ m ²	
Implementation		Replacing with Geopolymer 13.24 MJ/ m^2			
Total Walls		469.90 KJ/m ²	62.19 MJ/m ²	865MJ/ m ²	
i otar Walls		523.09 M	J/m ²		

Table A.C.112: Green Star. Potential reduction in carbon emissions in a porcelain-enamelled steel curtain wall (Lawson 1996, p. 131).

Life Cycle Stages of	Construction		Embodied	
building	Pre-Construction	Construction	Energy	
	Potential Carbon Emission (E	mbodied Energy) Reduction	Basic	
Measurable energy to	Steel from recycled content 108.58	Reduce steel use in design 51.28		
reduce in Implementation	MJ/m2	MJ/m2		
	Enamelled steel from recycled content	Replacing with Geopolymer 6.58	865 MJ/m ²	
	78.29 MJ/m ²	MJ/m ²	005 IVIJ/III	
	Aluminium from recycled content			
	236.05 MJ/m ²			
Crean Star Tatal Wall	422.92 MJ/m ²	57.86 MJ/m ²	865 MJ/ m ²	
Green Star, Total Wall 480.78 MJ/m ²			005 IVIJ/ III	

v. Glass Curtain Wall

Table A.C.113: Potential reduction in carbon emissions in a glass curtain wall (Lawson 1996, p. 131).

Р	rocesse	s where carbon emissions (em	bodied energy) can be reduced	
Building	Use A from r Reduc	ecycled) = $2.512 \text{ kg/m2 x } 161.9 = 406.0$ ed materials in design 2.20% Aluminium in design $2.512 Kg x$	+ 0.77 + 0.288) kg/m2 (170 Mj/kg new 59 MJ/m ² 170 MJ/Kg (Lawson 1996, p. 13) x 20%	
materials and elements	Use A 90% = Reuse	materials and elements luminium from recycled contents 2.512 : 366.02 MJ/m ² d materials in design e 20% Aluminium in design 2.512 Kg y	kg/m2 (170 Mj/kg new – 8.1 Mj/kg fror x 170 MJ/Kg (Lawson 1996, p. 13) x 209	•
Life Cycle Stages	of buildin	§ Constr	uction	Embodied
		Pre-Construction	Construction	Energy
		Potential reduction in Carbon Emissions		Standard
Measurable energy to reduce in Building materials and elements		Aluminium from recycled content 406.69 MJ/m ²	Reduce Aluminium use in design 85.40 MJ/m2	770MJ/ m ²
		406.69 KJ/m ²	85.40 MJ/m ²	
Total Walls		400.09 KJ/m 492.09 MJ/m ²		770MJ/ m ²

Table A.C.114: Green Star. Potential reduction in carbon emissions in a glass curtain wall (Lawson 1996, p. 131).

Life Cycle Stages of	Construction		Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emission (E	mbodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation	Aluminium from recycled content 366.02 MJ/m ²	Reduce Aluminium use in design 85.40 MJ/m2	770 MJ/m ²
Croop Stor Total Wall	366.02 MJ/m ²	85.40 MJ/m ²	770 MJ/ m ²
Green Star, Total Wall	451.42 MJ/m ²		//U/NJ/ M-

w. Steel Faced Sandwich Panel Wall

Table A.C.115: Potential reduction in carbon emissions in a steel faced sandwich panel wall (Lawson 1996, p. 132).

Pr	ocesses	s where carbon emissions (embo	died energy) can be reduced	1
Building	- Steel 20.10 - Enan - 20.10 Reduce	recycled aggregates frame from average recycled content = (0 MJ/Kg = 0.959 KJ/Kg x 17.9 Kg/ m2 = 1 nelled Steel facing from average recycled MJ/Kg = 9.734 KJ/Kg x 19.9 Kg/ m2 = 220 d materials in design 20% steel in design 0.959 Kg x 38 MJ/Kg	7.16 MJ/m2 content = 9.734 Kg x 40 MJ/Kg (Law 193.70 MJ/m2	vson 1996, p. 13)
materials and	Green	8 8 9	$g(Eawson 1770, p. 13) \times 20\% = 7.20$	0 1010/1112
elements	0	d materials and elements		
	$\label{eq:steel} \begin{array}{l} - \text{Steel frame from average recycled content} = 0.959 \ \text{Kg} \ x \ 38 \ \text{MJ/Kg} \ (\text{Lawson 1996, p. 13}) \\ \text{MJ/Kg} = 0.959 \ \text{KJ/Kg} \ X \ 17.9 \ \text{Kg}/\ \text{m2} \ x \ 90\% = \textbf{15.44 \ \text{MJ/m2}} \\ - \ \text{Enamelled Steel facing from average recycled content} = 9.734 \ \text{Kg} \ x \ 40 \ \text{MJ/Kg} \ (\text{Lawson 1} \\ - \ 20.10 \ \text{MJ/Kg} = 9.734 \ \text{KJ/Kg} \ x \ 19.9 \ \text{Kg}/\ \text{m2} \ x \ 90\% = \textbf{174.33 \ \text{MJ/m2}} \\ \textbf{Reduced materials in design} \end{array}$			
Life Cycle Stages o		e 20% steel in design 0.959 Kg x 38 MJ/k Construct		Embodied
Life Cycle Stages 0	1 Dunung	Pre-Construction	Construction	Energy
		Potential reduction in		Standard
Measurable energy to reduce in Building materials and elements		Steel from recycled content 17.16 MJ/m² Enamelled steel from recycled content 193.70 MJ/m²	Reduce steel use in design 7.28 MJ/m2	1087MJ/ m ²
T. 4. 1 XX7. 11.		210.86 KJ/m ²	7.28 MJ/m ²	1007341/2
Total Walls		218.24 MJ/m ²		1087MJ/ m ²

Table A.C.116: Green Star. Potential reduction in carbon emissions in a steel faced sandwich panel wall (Lawson 1996, p. 132).

Life Cycle Stages of	Construction		Embodied	
building	Pre-Construction	Construction	Energy	
	Potential Carbon Emission (E	mbodied Energy) Reduction	Basic	
Measurable energy to	Steel from recycled content 15.44	Reduce steel use in design 7.28		
reduce in Implementation	MJ/m2	MJ/m2		
-	Enamelled steel from recycled content		1087 MJ/m ²	
	174.33 MJ/m ²			
Crean Stan Tatal Wall	189.77 MJ/m ²	7.28 MJ/m ²	1087 MJ/ m ²	
Green Star, Total Wall	197.05	MJ/m ²	1007 IVIJ/ III	

x. Aluminium Curtain Wall

Table A.C.117: Potential reduction in carbon emissions in an aluminium curtain wall (Lawson 1996, p. 132).

	Reuse	recycled aggregates		
	Use A	luminium from recycled content (1.4544 +		(170 Mj/kg new -
Building	8.1 Mj	/kg from recycled) = 4.95 64 kg/m2 x 161.	$.9 = 802.44 \text{ MJ/m}^2$	
materials and	Green	Star		
elements	Reuse	materials and elements		
	Use A	luminium from recycled content (1.4544 +	0.7704 + 0.288 + 2.4435) kg/m2	(170 Mj/kg new -
	8.1 Mj	/kg from recycled) = 4.95 64 kg/m2 x 161.	.9 x 90%= 722.19 MJ/m ²	
Life Cycle Stages	of building	Construction		Embodied
		Pre-Construction	Construction	Energy
		Potential reduction in carbon emissions		Standard
Measurable energy	y to	Aluminium from recycled content		
reduce in Building	g	802.44 MJ/m ²		935MJ/ m ²
materials and ele	ments			
		· · · · · · · · · · · · · · · · · · ·		
Total Walls		802.44 KJ/m ²		935MJ/ m
		802.44 MJ/m ²		935MJ/m ²

Table A.C.118: Green Star. Potential reduction in carbon emissions in an aluminium curtain wall(Lawson 1996, p. 132).

Life Cycle Stages of	Constru	Embodied			
building	Pre-Construction	Construction	Energy		
	Potential Carbon Emission (En	nbodied Energy) Reduction	Basic		
Measurable energy to	Aluminium from recycled content		935 MJ/m ²		
reduce in Implementation	722.19 MJ/m2		955 MJ/III		
Career Sterr Tetel Well	722.19 MJ/m ²		935 MJ/ m ²		
Green Star, Total Wall	722.19 MJ/m ²		955 MJ/ m-		

A.C.2.3 Potential carbon emission reduction in general Australian roof construction systems

a. Timber Frame, Timber Shingle Roof

Table A.C.119: Potential reduction in carbon emissions in a timber framed timber shingle roof (Lawson 1996, p. 134).

Proces	ses where carbon emission	s (embodied energy) can be reduced		
Building	Reused materials and elements			
materials and	- Softwood Trusses from recycled	trusses 40% x 51 (Design Coalition 2013) = 20.4	40 MJ/m ²	
elements	- Using recycled trusses = $60\% x$	51 $MJ/m^2 = 30.60 MJ/m^2$		
	- Use insulation from recycled materials, 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.6255kg/m ² = 17.57 MJ/m² (Steel Construction Information 2014)			
	Green Star Reuse materials and elements (local salvage/re-use centre) Material-8 Timber, Green Star Technical Manual, 95% of all timber products re-used, post- consumer recycled timber or FSC certified timber			
	 Softwood Trusses from recycled Using recycled trusses, 55% x 5 	trusses 40% x 51 (Design Coalition 2013) = 20. 1 $MJ/m^2 = 28.05 MJ/m^2$	40 MJ/m ²	
Life Cycle Stages of		Construction	Embodied	
building	Pre-Construction	Construction	Energy	
	Potential Red	uction in Carbon Emissions	Basic	
Measurable energy to reduce in Building materials and elements	20.4 MJ/m ²	Using recycled trusses 30.60 MJ/m² Use recycled thermal insulation 17.57MJ/m²	151MJ /m ²	
T-4-1 Df	20.4 MJ/m ²	48.17 MJ/m ²	151341/	
Total Roof		68.57 MJ/m ²	151MJ/ m	

Table A.C.120: Green Star. Potential reduction in carbon emissions in a timber framed timber shingle roof (Lawson 1996, p. 134).

Life Cycle Stages of	Cor	Embodied	
building	Pre-Construction	Construction	Energy
	Potential Carbon Emission	n (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Building materials and elements	Softwood Trusses from recycled trusses 20.40 MJ/m²	Using recycled trusses 28.05 MJ/m ²	151 MJ/m ²
	-	-	
Green Star, Total Roof	20.40 MJ/ m ²	28.05 MJ/m ²	151 MJ/ m ²
Green Star, Total Roof	48.	.45 MJ/m ²	131 WIJ/ III

b. Timber Frame, Fiber Cement Shingle Roof

Table A.C.121: Potential reduction in carbon emissions in a timber framed fibre cement shingle roof (Lawson 1996, p. 134).

Process	ses where carbon emission	s (embodied energy) can be reduced			
Building	Reused materials and elements				
materials and	- Softwood Trusses from recycled	l trusses 40% x 43 (Design Coalition 2013) = 17.	2 MJ/m ²		
elements	- Using recycled trusses = 60% x	43 $MJ/m^2 = 25.8 MJ/m^2$			
	- Use insulation from recycled ma = 17.57 MJ/m ² (Steel Construction	aterials, 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x on Information 2014)	0.6255kg/m ²		
	Being small and modular in natur crushed and recycled (LEED 201-	e, concrete roof tile is less prone to waste. Roof ti 4)	iles can be		
	Use tiles from recycled roof tiles,	144 MJ/m ² x 13% (LEED 2014) = 18.72 MJ/m²			
	Use tiles from recycled roof tiles	(Herbudiman & Saptaji 2013) from 45% recycled	l content		
	Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (19 concrete – 2.66 cement) Kg/m ² (Lawson 1996, p. 134) x 50% = 0.083 x 16.34 kg/m2 x 50% (Herbudiman & Saptaji 2013) = 6.78 MJ/m²				
	Green Star				
	Reuse materials and elements (local salvage/re-use centre) Material-8 Timber, 95% of all timber products re-used, post-consumer recycled timber or FSC certified timber				
	- Softwood Trusses from recycled trusses 40% x 43 (Design Coalition 2013) = 17.2 MJ/m^2				
	- Using recycled trusses, 55% x 43 $MJ/m^2 = 23.65 MJ/m^2$				
Life Cycle Stages of		Construction	Embodied		
building	Pre-Construction	Construction	Energy		
		uction in Carbon Emissions	Basic		
Measurable energy to reduce in Building materials and elements	Trusses from recycled trusses 17.2 MJ/m ²	Using recycled trusses 25.8 MJ/m² Use recycled thermal insulation 17.57MJ/m² Recycled fibre cement 13% - 18.72 MJ/m² Use fibre cement with recycled contents 6.78 MJ/m²	291MJ /m ²		
	17.2 MJ/m ²	55.33 MJ/m ²			
Total Roof		74.1 MJ/m ²	291MJ/ m		

Table A.C.122: Green Star. Potential reduction in carbon emissions in a timber framed fibre cement shingle roof (Lawson 1996, p. 134).

Life Cycle Stages of	Cor	struction	Embodied
building	Pre-Construction	Energy	
	Potential Carbon Emission	n (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Building materials and elements	Softwood Trusses from recycled trusses 17.2 MJ/m²	Using recycled trusses 23.65 MJ/m ²	291 MJ/m ²
mater fais and elements			
Green Star, Total Roof	17.2 MJ/ m ²	23.65 MJ/m ²	291 MJ/ m ²
Green Star, Total Root	40.	.85 MJ/m ²	271 WIJ/ III

c. Timber Frame, Steel Sheet Roof

Table A.C.123: Potential reduction in carbon emissions in a timber framed steel sheet roof (Lawson 1996, p. 133).

	Proce	sses where carbon emissions	(embodied energy) can be	e reduced	
	- Stee 4.9 kg Reus - Soft - Usin - Use	I from average recycled conte I sheet from recycled contents {38 MJ $y' m^2 = 85.75 MJ/m^2$ sed materials and elements wood Trusses from recycled trusses 40 g recycled trusses = 60% x 34 MJ/m ² recycled thermal insulation, 49MJ/kg μ^2 (Steel Construction Information 201-	/Kg (Lawson 1996) – 20.50 MJ/H % x 34 MJ/m ² (Design Coalition (Lawson 1996, p. 133) = 20.4 M (Lawson 1996) - 20.90 MJ/kg x 0	2013) = 13.6 MJ/m² J/m ²	
Building	Gree	en Star			
materials and			ont		
elements	Mater emboo Austra - Stee MJ/K Reus Mater consu - Soft - Usin	el from average recycled content rial-6 Steel, Green Star Technical Manual, is considered maximum 90%, therefore reduced died energy by this credit (Steel from 90% Recycled contents) (Green building Council of ratia 2008) is: el sheet from recycled content {38 MJ/Kg (Lawson 1996. p. 144) – 20.50 MJ/Kg} = 17.5 Kg x 4.9 kg/ m ² x 90% = 77.17 MJ/m ² sed materials and elements (local salvage/re-use centre) rial-8 Timber, Green Star Technical Manual, 95% of all timber products re-used, post- imer recycled timber or FSC certified timber twood Trusses from recycled trusses 40% x 34 (Design Coalition 2013) = 13.6 MJ/m ² ng recycled trusses = 55% x 34 MJ/m ² (Lawson 1996, p. 133) = 18.7 MJ/m ²			
Life Cycle Stages of be	anding	Construc Pre-Construction	Construction	Embodied Energy Basic	
		Potential reduction in		Busic	
Measurable energy to reduce in Building materials and elements		Trusses from recycled timber 40% 13.6 MJ/m ² Steel sheet from recycled content 85.75 MJ/m ²	Use recycled trusses 60% 20.4 MJ/m² Use recycled thermal insulation 17.57 MJ/m²	330MJ / m ²	
	_	99.35 MJ/m ²	37.97 MJ/m ²		
Total Roof, Research		137.32 N	IJ/m ²	330MJ/ m ²	

Table A.C.124: Green Star. Potential reduction in carbon emissions in a timber framed steel sheet roof (Lawson 1996, p. 133).

Life Cycle Stages of	Co	nstruction	Embodied
building	Pre-Construction	Construction	Energy
	Potential Carbon Emissio	n (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation	Steel sheet from 90% recycled content = 77.17 MJ/m ² Trusses from recycled timber 40% 13.6 MJ/m ²	Use recycled trusses 55% 18.7 MJ/m²	330 MJ/m ²
Green Star, Total Roof	90.77 MJ/m ²	18.7 MJ/m ²	330 MJ/ m ²
Green Star, Total Root	109.47 MJ/m ²		550 MJ/ III

d. Steel Frame, Steel Sheet Roof

Table A.C.125: Potential reduction in carbon emissions in a steel framed steel sheet roof (Lawson 1996, p. 135).

	Processes where carbon emissions (embodied energy) can be reduced				
	Steel from average recycled content				
	- Steel sheet from average recycled c MJ/Kg = 87.71 MJ/m^2	ontent = 4.9 Kg x $\{38 \text{ MJ/Kg} (\text{Lawson 1996})\}$	5, p.135) - 20.10		
	MJ/Kg x $(3.33 + 0.754)$ kg/ $\mathbf{m}^2 = 71$. Reuse materials and elements	content {34 MJ/Kg (Lawson 1996, p. 135) – 47 MJ/m² mand 2014) 40% x 4.084 kg/m2 x 34 MJ/K			
	- Reduce 20% steel use in design, 4.9	9 Kg x 34 MJ/Kg (Lawson 1996, p.135) x 20	$0\% = 33.32 \text{ MJ/m}^2$		
Building	- Use recycled thermal insulation, 49 (Steel Construction Information 2014	MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.551 4)	$kg/m^2 = 17.57 MJ/m^2$		
materials and elements	Green Star				
	 Steel from average recycled content Material-6 Steel, Green Star Technical Manual, is considered maximum 90%, therefore reduced embodied energy by this credit (Steel from 90% Recycled content) (Green building Council of Australia 2008) is: Steel sheet from average recycled content = 4.9 Kg x {38 MJ/Kg (Lawson 1996, p. 135) - 20.10 MJ/Kg} x 90% = 78.93 MJ/m² 				
	- Steel frame roofing from recycled content {38 MJ/Kg (Lawson 1996, p. 135) – 21.5 MJ/Kg} = 17.5 MJ/Kg x $(3.33 + 0.754)$ kg/m ² x 90% = 64.32 MJ/m²				
	Reduce 20% steel use in design, 4.9	Kg x 34 MJ/Kg (Lawson 1996, p. 135) x 209	$\% = 33.32 \text{ MJ/m}^2$		
Life Cycle Stages	Co	onstruction	Embodied Energy		
building	Pre-Construction	Construction	Basic		
		rbon emission (embodied energy)			
Measurable energy reduce in Building materials and	Steel frame from average recycled content 71.47 MJ/m² Steel Sheet from recycled	Use recycled trusses = 55.54 MJ/m^2 Use recycled insulation = 17.57 MJ/m^2	483 MJ / m ²		
elements	content 87.71 MJ/m²	Reduce steel in design 33.32 MJ/m^2			
Total Roof	159.18 MJ/m ²	73.11 MJ/m ²	483 MJ / m ²		
	232.29 MJ/m ²				

Table A.C.126: Green Star. Potential reduction in carbon emissions in a steel framed steel sheet roof (Lawson 1996, p. 135).

Life Cycle Stages of building	Construction			Embodied
	Pre-Construction	Construction		Energy
	Potential Carbon Emission (En	nbodied Energy) Reduction		Basic
Measurable energy to reduce in Implementation	Steel sheet from 90% Recycled content = 78.93 MJ/m² Steel frame from 90% Recycled content = 64.32 MJ/m²	Reduce steel in design 33.32 MJ/m ²		483 MJ/ m ²
Green Star, Total Roof	143.25 MJ/m ²	33.32 MJ/m ²		483 MJ / m ²
Green Star, Total Root	178.57 N	MJ/m ²		-105 1415/ 111

e. Timber Frame, Concrete Tile Roof

Table A.C.127: Potential carbon emission reductions in a timber framed concrete tile roof (Lawson 1996, p. 134).

Process	ses where carbon emissions	s (embodied energy) can be reduced			
Building	Reused materials and elements				
materials and	- Softwood Trusses from recycled trusses 40% x 43 (Design Coalition 2013) = 17.2 MJ/m^2				
elements	- Using recycled trusses = $60\% \text{ x}^2$	$13 \text{ MJ/m}^2 = 25.8 \text{ MJ/m}^2$			
	- Use insulation from recycled mat = 17.57 MJ/m ² (Steel Construction	terials, 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x n Information 2014)	0.6255kg/m ²		
	Being small and modular in nature crushed and recycled (LEED 2014	e, concrete roof tile is less prone to waste. Roof ti	iles can be		
	Use tiles from recycled roof tiles,	92 $MJ/m^2 x 13\%$ (LEED 2014) = 11.96 MJ/m^2			
	Use tiles from recycled roof tiles (Herbudiman & Saptaji 2013) from 45% recycled	l content		
	Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (44 concrete – 6.16 cement) Kg/m ² (Lawson 1996, p. 134) x 45% = 0.083 x 37.84 kg/m2 x 50% (Herbudiman & Saptaji 2013) = 1.57 MJ/m²				
		ents (local salvage/re-use centre) chnical Manual, 95% of all timber products re-us certified timber	ed, post-		
	- Softwood Trusses from recycled trusses 40% x 43 (Design Coalition 2013) = 17.2 MJ/m^2				
	- Using recycled trusses 55% x 43	$MJ/m^2 = 23.65 \ \mathbf{MJ/m^2}$			
Life Cycle Stages of		Construction	Embodied		
building	Pre-Construction	Construction	Energy		
	Potential Redu	action in Carbon Emissions	Basic		
Measurable energy to	Trusses from recycled trusses	Using recycled trusses 25.8 MJ/m ²			
reduce in Building	17.2 MJ/m²	Use recycled thermal insulation 17.57MJ/n	240MJ /m ²		
materials and elements	Use tiles with recycled contents 1.57 MJ/m ²	Use recycled roof tiles 13%, 11.96 MJ/m²	2401013/111		
	18.77 MJ/m ²	55.33 MJ/m ²	2403434		
Total Roof		74.1 MJ/m ²	240MJ/ m		

Table A.C.128: Green Star. Potential reduction in carbon emissions in a timber framed concrete tile roof (Lawson 1996, p. 134).

Green Star, Total Root	45.16 MJ/m ²		240 NJ/ III
Green Star, Total Roof	21.51 MJ/ m ²	23.65 MJ/m ²	240 MJ/ m ²
materials and clements			
materials and elements	2		
reduce in Building	recycled trusses 17.2 MJ/m²		240 MJ/m ²
Measurable energy to	Softwood Trusses from	Using recycled trusses 23.65 MJ/m ²	
	Potential Carbon Emission	(Embodied Energy) Reduction	Basic
building	Pre-Construction	Construction	Energy
Life Cycle Stages of	Cor	Embodied	

f. Steel Frame, Concrete Tile Roof

Table A.C.129: Potential reduction in carbon emissions in a steel framed concrete tile roof (Lawson 1996, p. 134).

	Processes where carbon en	nissions (embodied energy) can b	e reduced	
	$ MJ/Kg \ge (3.33 + 0.754) kg/m^2 = 71. $ Reuse materials and elements - Use 40% recycled trusses (UK Inde Reduce 20% steel use in design, 4.9	ontent {38 MJ/Kg (Lawson 1996, p. 135) – 47 MJ/m² mand 2014) 40% x 4.084 kg/m2 x 34 MJ/K Kg x 34 MJ/Kg (Lawson 1996, p. 135) x 20	$g = 55.54 \text{ MJ/m}^2$ $9\% = 33.32 \text{ MJ/m}^2$	
	(Steel Construction Information 2014	,	C	
	Use tiles from recycled roof tiles, 92	$MJ/m^2 \ge 13\%$ (LEED 2014) = 11.96 MJ/m^2	2	
	Use tiles from recycled roof tiles (He	rbudiman & Saptaji 2013) from 45% recycl	ed content	
Building materials and elements	Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (44 concrete – 6.16 cement) Kg/m ² (Lawson 1996, p. 134) x 45% = 0.083 x 37.84 kg/m2 x 50% (Herbudiman & Saptaji 2013) = 1.57 MJ/m²			
	Steel from average recycled contentMaterial-6 Steel, Green Star Technical Manual, is considered maximum 90%, therefore reduced embodied energy by this credit (Steel from 90% Recycled contents) (Green building Council of Australia 2008) is:- Steel sheet from average recycled content = 4.9 Kg x {38 MJ/Kg (Lawson 1996, p. 135) - 20.10 MJ/Kg} x 90% = 78.93 MJ/m ²			
	MJ/Kg x (3.33 + 0.754) kg/ m ² x 90%	ontent {38 MJ/Kg (Lawson 1996, p. 135) – 6 = 64.32 MJ/m ² Kg x 34 MJ/Kg (Lawson 1996, p.135) x 209	-	
	Co	onstruction	Embodied Energy	
Life Cycle Stages of building	Pre-Construction	Construction	Basic	
2		tion in carbon emissions		
Measurable energy reduce in Building materials and elements	 Steel frame from average recycled content 71.47 MJ/m² Recycled tiles used 11.96 MJ/m² Tiles from recycled content 1.57 MJ/m² 			
Total Roof	85 MJ/m ²	106.43 MJ/m ²	450 MJ / m ²	

Table A.C.130: Green Star. Potential reduction in carbon emissions in a steel framed concrete tile roof (Lawson 1996, p. 135).

Life Cycle Stages of building	Construc	Embodied	
	Pre-Construction Construction		Energy
	Potential Carbon Emission (En	nbodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation	Steel frame from 90% recycled content = 64.32 MJ/m ² Reduce steel use in design 33.32 MJ/m ²		450 MJ/ m ²
Green Star, Total Roof	64.32 MJ/m ²	33.32 MJ/m ²	450 MJ / m ²
Green Star, 10tal Root	97.64 N	IJ/m ²	430 WJ/ III

g. Timber Frame, Terracotta Tile Roof

Table A.C.131: Potential reduction in carbon emissions in a timber framed terracotta tile roof (Lawson 1996, p. 134).

Process	ses where carbon emissions	s (embodied energy) can be reduced			
Building	Reused materials and elem	nents			
materials and	- Softwood Trusses from recycled	trusses 40% x 43 (Design Coalition 2013) = 17.2	2 MJ/m ²		
elements	- Using recycled trusses = $60\% x^2$	$43 \text{ MJ/m}^2 = 25.8 \text{ MJ/m}^2$			
	- Use insulation from recycled mat = 17.57 MJ/m ² (Steel Construction	terials, 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x n Information 2014)	0.6255kg/m ²		
	Being small and modular in nature crushed and recycled, (LEED 2014	e, concrete roof tile is less prone to waste. Roof ti 4)	les can be		
	Use tiles from recycled roof tiles,	123 $MJ/m^2 \ge 13\%$ (LEED 2014) = 15.99 MJ/m^2			
	Use tile from recycled tiles (Herbu	udiman & Saptaji 2013) from 45% recycled conte	ent		
	Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (49 concrete) Kg/m ² (Lawson 1996, p. 134) x 50% = 0.083 x 49 kg/m2 x 50% (Herbudiman & Saptaji 2013) = 2.033 MJ/m^2				
	Material-8 Timber, Green Star Tec consumer recycled timber or FSC	trusses 40% x 43 (Design Coalition 2013) = 17.2			
Life Cycle Stages of		Construction	Embodied		
building	Pre-Construction	Construction	Energy		
· ·	Potential Redu	iction in Carbon Emissions	Basic		
Measurable energy to reduce in Building materials and elements	Trusses from recycled trusses 17.2 MJ/m ²	Using recycled trusses 25.8 MJ/m² Use recycled thermal insulation 17.57MJ/n Use recycled tiles 13%, 15.99 MJ/m² Tile from recycled content 2.033 MJ/m²	271MJ /m ²		
Total Roof	17.20 MJ/m²	61.39 MJ/m ²	271MJ/ m		
1 0tai Kooi		78.59 MJ/m ²	2/11VIJ/ M		

Table A.C.132: Green Star. Potential reduction in carbon emissions in a timber framed terracotta tile roof (Lawson 1996, p. 134).

Life Cycle Stages of	Con	Embodied	
building	Pre-Construction	Energy	
	Potential Carbon Emission	n (Embodied Energy) Reduction	Basic
Measurable energy to reduce in Building materials and elements	Softwood Trusses from recycled trusses 17.2 MJ/m ²	Using recycled trusses 23.65 MJ/m ²	271 MJ/m ²
	21.51 MJ/ m ²	23.65 MJ/m ²	
Green Star, Total Roof		.16 MJ/m ²	271 MJ/ m ²

h. Timber Frame, Synthetic Rubber Membrane Roof

Table A.C.133: Potential reduction in carbon emissions in a timber framed synthetic rubber membrane roof (Lawson 1996, p. 134).

Process	ses where carbon emissions	s (embodied energy) can be reduc	ed
Building materials and elements	- Using recycled trusses = $60\% x^2$	trusses 40% x 43 (Design Coalition 2013) = $43 \text{ MJ/m}^2 = 25.8 \text{ MJ/m}^2$ terials, 49MJ/kg (Lawson 1996) - 20.90 MJ/	
	Material-8 Timber, Green Star Tec consumer recycled timber or FSC	trusses 40% x 43 (Design Coalition 2013) =	
Life Cycle Stages of	Construction		Embodied
building	Pre-Construction	Construction	Energy
	Potential Reduction in Carbon Emissions		Basic
Measurable energy to reduce in Building materials and elements	Trusses from recycled trusses 17.2 MJ/m ²	Using recycled trusses 25.8 MJ/m² Use recycled thermal insulation 17.57MJ/m²	386MJ /m ²
	17.20 MJ/m ²	43.37 MJ/m ²	
Total Roof	60.57 MJ/m ²		386MJ/ m ²

Table A.C.134: Green Star. Potential reduction in carbon emissions in a timber framed synthetic rubber membrane roof (Lawson 1996, p. 134).

Life Cycle Stages of	Cor	Embodied	
building	Pre-Construction	Construction	Energy
	Potential Carbon Emission	Basic	
Measurable energy to	Softwood Trusses from	Using recycled trusses 23.65 MJ/m ²	
reduce in Building	recycled trusses 17.2 MJ/m ²		386 MJ/m ²
materials and elements			
Green Star, Total Roof	21.51 MJ/ m ²	23.65 MJ/m ²	386 MJ/ m ²
Green Star, Total Roof 45.16 MJ/m ²			JOU NIJ/ III

i. Concrete Slab, Synthetic Rubber Membrane Roof

Table A.C.135: Potential reduction in carbon emissions in a concrete slab synthetic rubber membrane roof (Lawson 1996, p. 135)

Proc	esses where carbon emissions (embodied energy) can be reduced	1		
	Reused recycled aggregate for concrete			
	 Concrete from 80% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (360 concrete Kg (Lawson 1996, p. 125) x 80% = 19.97 MJ/m² Steel from average recycled content 	00 0		
	- Steel mesh +Edge beams from average recycled content = 7.153 Kg x {34 MJ/Kg (La - 20.10 MJ/Kg} = $99.42 MJ/m^2$	wson 1996, p. 13		
Building materials and elements	 - 20.10 MJ/Kg } = 99.42MJ/m² Green Star Reused recycled aggregate for concrete Material-5 Green Star Technical Manual, is considered maximum 20%, therefore reduced embodied energy by this credit (Concrete from 20% Recycled aggregate) (Green building Council of Australia 2008) is: - Concrete from 20% Recycled aggregate (Uche 2008; PCA 2014), embodied energy of aggregate is 0.083 MJ/Kg Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (360 concrete –59.14 cement) Kg (Lawson 1996, p.125) x 20% = 4.99 MJ/m² Steel from average recycled content Material-6 Green Star Technical Manual, Steel is considered maximum 90%, therefore reduced embodied energy by this credit (Steel from Recycled content) (Green building Council of Australia 2008) is: 7.153 Kg x 90% {34 MJ/Kg (Lawson 1996, p. 13) - 20.10 MJ/Kg} = 89.48 MJ/m² 			
Implementation	Decreased and Replaced energy in process Replaced cement Geopolymer Concrete or 100% replacing with recycled cement (Nath & Sarker 2 reduction in GHG (McLellan et al. 2011) 360 kg/m ² (Lawson 1996, p. 124) x 14% Cement (Lawson1996, p. 41) = 48.88 kg replain concrete 48.88 kg Cement/m ² x 5.6 MJ/kg (Lawson 1996, p. 13) = 273.72 MJ/ m ² Green Star Replacing maximum 60% of cement (Green building Council of Australia 2008)	,		
	360 kg/m ² (Lawson 1996, p. 124) x 14% Cement (Lawson 1996, p. 41) = 29.33 kg repl in concrete 29.33 kg Cement/m ² x 5.6 MJ/kg (Lawson 1996, p. 13) x 60% = 164.24 MJ/ m²	aced cement/ m ²		
Life cycle stages of buil	ding Construction	Embodied		
	Pre-Construction Construction	Energy		
	Potential Carbon Emission (Embodied Energy) Reduction	Basic		
Measurable energy to re in Building materials a elements		645MJ/m		

Measurable energy to reduce in Implementation		Geopolymer replacing 100% of cement = 273.72 MJ/ m²	
Total Floor	19.97 MJ/m ²	373.14 MJ/m ²	645MJ / m ²
	393	.11 MJ/m ²	

Table A.C.136: Green star. Potential reduction in carbon emissions in a concrete slab synthetic rubber membrane roof (Lawson 1996, p. 135).

Life Cycle Stages of building	Cor	Embodied	
	Pre-Construction	Construction	Energy
	Potential Carbon Emission	n (Embodied Energy) Reduction	Basic
Measurable energy to		90% Steel mesh from average recycled	645 MJ/m ²
reduce in Implementation	ce in Implementation concrete = 4.99 MJ/m^2 content 89.48MJ/m^2		010 1010/11
Measurable energy to reduce		Geopolymer 60% Cement Replacement	
in Implementation		164.24 MJ/m ²	
Cusan Stan Tatal Flagn	4.99 MJ/m ²	253.72 MJ/m ²	645MJ/ m ²
Green Star, Total Floor	258.71 MJ/m ²		6451VIJ/ m ⁻

j. Steel Frame, Fibre Cement Sheet Roof

Table A.C.137: Potential reduction in carbon emissions in a steel framed fibre cement sheet roof (Lawson 1996, p. 135).

	Processes where carbo	n emissions (embodied energy) can	be reduced		
	MJ/Kg x (3.384 + 0.35) kg/ m ² = Reuse materials and elements	eled content {38 MJ/Kg (Lawson 1996, p. 135)			
	- Use recycled thermal insulation (Steel Construction Information	n, 49MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0. 2014)	$55 \text{kg/m}^2 = 17.57 \text{ MJ/m}^2$		
	Use fibre cement from recycled	contents, 106 $MJ/m^2 \times 13\%$ (LEED 2014) = 1	3.78MJ/m ²		
Building	Use fibre cement from recycled	contents (Herbudiman & Saptaji 2013) from 4	5% recycled content		
materials and elements		Saved embodied energy = embodied energy of aggregate 0.083 MJ/Kg x (44 concrete $- 6.16$ cement) Kg/m ² (Lawson 1996, p. 134) x 45% = 0.083 x 14 kg/m ² x 50% (Herbudiman & Saptaji 2013) = 5.81 MJ/m ²			
	embodied energy by this credit (Australia 2008) is:	chnical Manual, is considered maximum 90%, Steel from 90% Recycled contents) (Green bu cled content {38 MJ/Kg (Lawson 1996, p. 135)	ilding Council of		
		Construction Emb			
Life Cycle Stages building	of Pre-Construction	Construction	Basic		
		eduction in carbon emissions			
Measurable energy reduce in Building materials and elements		/m ² Use recycled trusses = 50.78 MJ/m ² Use recycled insulation = 17.57 MJ/m ² Fiber cement sheet from recycled contents 5.81 MJ/m ²	337 MJ / m ²		
Total Roof	75.39 MJ/m ²	74.16 MJ/m ²	227341/ 2		
		149.55 MJ/m ²	- 337MJ/ m ²		

Table A.C.138: Green Star. Potential reduction in carbon emissions in a steel framed fibre cement sheet roof (Lawson 1996, p, 135).

Life Cycle Stages of building	Construction		Embodied
	Pre-Construction Construction		Energy
	Potential Carbon Emission (En	nbodied Energy) Reduction	Basic
Measurable energy to reduce	Steel frame from 90% recycled		337 MJ/m ²
in Implementation	$content = 55.44 \text{ MJ/m}^2$		557 MJ/III
Crean Stan Tatal Deaf	55.44 MJ/m ²		337 MJ/ m ²
Green Star, Total Roof	55.44 MJ/m ²		557 MJ/ m

k. Steel Frame, Steel Sheet Roof (commercial)

Table A.C.139: Potential reduction in carbon emissions in a steel framed steel sheet roof (commercial) (Lawson 1996, p. 135).

	Р	rocesses where carbon em	ussions (embodied energy) can l	be reduced	
	Ste	Steel from average recycled content			
		eel sheet from average recycled co /Kg} = 100.24 MJ/m^2	$tent = 5.6 \text{ Kg x} \{38 \text{ MJ/Kg} (Lawson 199)\}$	96, p.135) - 20.10	
	MJ/ Ret	/Kg x $(3.384 + 0.35)$ kg/ $m^2 = 61.6$ use materials and elements	ontent {38 MJ/Kg (Lawson 1996, p. 135) 51 MJ/m² mand 2014) 40% x 3.734 kg/m2 x 34 MJ/	0,	
Building materials and	- U:	•	MJ/kg (Lawson 1996) - 20.90 MJ/kg x 0.5	6	
elements	Mat emb Aus - St MJ/ - St	Green Star Steel from average recycled content Material-6 Steel, Green Star Technical Manual, is considered maximum 90%, therefore reduced embodied energy by this credit (Steel from 90% Recycled content) (Green building Council of Australia 2008) is: - Steel sheet from average recycled content = 5.6 Kg x {38 MJ/Kg (Lawson 1996, p.135) - 20.10 MJ/Kg} x 90% = 90.21 MJ/m ² - Steel frame roofing from recycled content {38 MJ/Kg (Lawson 1996, p. 135) - 21.5 MJ/Kg} = 17.5 MJ/Kg x (3.384 + 0.35) kg/m ² x 90% = 55.44 MJ/m ²			
Life Coule Steres			nstruction	Embodied Energy	
Life Cycle Stages building	5 01	Pre-Construction	Construction	Basic	
		Potential reduction in carbon emissions			
Measurable energy to reduce in Building materials and elements		Steel frame from average recycled content 61.61 MJ/m² Steel Sheet from recycled content 100.24 MJ/m²	Use recycled trusses = 50.78 MJ/m ² Use recycled insulation = 17.57 MJ/m ²	401 MJ/ m ²	
Total Roof		161.85 MJ/m ²	68.35 MJ/m ²		
I OTAL ROOL			08.35 MJ/m ²	401 MJ/ m ²	

Table A.C.140: Green Star. Potential reduction in carbon emissions in a steel framed steel sheet roof (commercial) (Lawson 1996, p. 135).

Life Cycle Stages of building	Construction		Embodied
	Pre-Construction Construction		Energy
	Potential Carbon Emission (En	nbodied Energy) Reduction	Basic
Measurable energy to reduce in Implementation	Steel sheet from 90% Recycled content = 90.21 MJ/m² Steel frame from 90% Recycled content = 55.44 MJ/m²		401 MJ/m ²
Green Star, Total Roof	145.65 MJ/m ²		401 MJ/ m ²
Green Star, Totai Kooi	145.65 MJ/m ²		401 MJ/ III

APPENDIX D

DATA RELATING TO CHAPTER FIVE

References, specifications and detailed information in these tables relates to data in Chapter Five.

Appendix D

Table A.D.1: Bioclimatic condi	ions - current; from best practice with green tools (Green Star, LEED and BREEAM); from this research	h model; and from research and lab

Bioclimatic Design Principles Criteria	Current conditions, Implemented	Conditions with Green tools G.S., LEED, BREEAM	Conditions in this research	Conditions in research and lab
Concrete from recycled aggregates	In Australia, there are a number of manufactured and recycled aggregates readily available in certain localities ¹	G.S. and LEED 1-3 points 20-30% RA for structural purpose; BRE 25-50% in 20-40 MPa - no restriction, 100% non-structural 2,18,36	Fully RA for non-structural purpose; 100% RA for non-structural; 80 % RA for structural purpose ⁶	ADAA, ASA, UNSW, Standards Australia; ⁴ , fully RA for non-structural; 30-75-80 % RA for structural ^{13,11}
Concrete block from recycled aggregate	24% recycled content of an aggregate concrete block ⁸	G.S., BRE, 40%; US 25% RA structural; 100%, on no natural aggregates in non-structural ^{18,23,36}	Aggregate for concrete block fully from recycled aggregate ¹³	UK, USA, AUS; ¹¹ , fully RA for concrete block ¹³
Brick from recycled aggregates	Current level of recycled material content in brick is 11% ^{14,41}	G.S., 30% ; ^{16, 23} ; LEED 20%; BRE 11% ISO, up to 10 points for 10% Recycled aggregate ^{14,16,36}	Reuse the recycled aggregate for brick, 67% ¹⁹	US; UK, Reuse fully recycled aggregate for brick, 6 points ^{11, 17}
Steel from average recycled content	Primary typically 10-15% of scrap steel, Secondary 100% scrap based production 25, 34	G.S. Mat-6, 60%; LEED 65-97.5%; BRE, Mat-6, 60%; -97.5% beams, plates; 65% bars; 66% steel deck post-consumer recycled content ^{23,16,38}	Steel from fully post-consumer recycled contents	Steel from 65-97.5% post-consumer recycled contents ^{22, 39}
Reuse recycled and post- consumer structural and non- structural steel	Scaffolding, formwork, sheet piles, etc., London Olympic Stadium ^{32, 34}	G.S., 95% Joinery, 50% structural framing, roofing; LEED 75-100% existing wall, floor, roof; BRE, Mat-6, 60% recycled content ^{3,5,23,24}	Use 40% recycled and post- consumer steel elements	Steel products are re-usable, steel piles, hollow sections; gauge, purlins, rails ^{32,31}
Reduce material use in steel structural design 10-20%	Some current green projects have reduced materials use in design 10-20% 23	G.S., Mat-6, 10-20% one point; LEED, eliminating need for materials in the design stage; BRE reduced, avoiding over-design ^{23,21,10,7,32}	Reduced materials use in structural design 10-20%	Integrative Design Process (IDP) Linear design; the London Olympics structure 1/10 ^{32,42}
Reuse recycled timber and post-consumer FSC timber	FSC works in 80 countries, 24000 FSC chain of custody certificates are active in 107 countries ^{23,}	G.S. 95% re-used, post-consumer; FSC certified timber; up to 3 points; LEED, 50% FSC; BRE, 3 points, post-consumer waste stream ^{22, 23, 32,24,29}	60% of all timber products re-used, post-consumer recycled timber; FSC certified timber	AUS; fully timber products re-used, post-consumer, recycled or are FSC certified timber ⁴³
Roof tile from recycled tiles	In some countries materials such as concrete roof tiles, removed separated and recycled ^{44, 45}	G.S. Mat-5, 1 point, no natural aggregates are used; LEED, from the waste, up to 3.5 points, BRE, M03, from the waste stream ^{20,21,23,36}	50% Roof tile from recycled aggregate ²¹	US; UK; AUS,50% Roof tile from recycled aggregate RA; roof tiles are 100% recoverable ^{21,45}
Thermal insulation from recycled content		G.S. 80% advised; LEED MR4 20%, ¹ / ₂ point, BRE 80%, 1 point, responsibly sourced ^{12.7,27,37}	Thermal insulation from fully recycled waste ²⁵	US; UK; Thermal insulation 100% from recycled waste ²⁵
Portland cement replaced with geopolymer based cement	Geopolymer has been used in structural, non-structural, e.g. GCI in Qld, Wellcamp Airport ^{46,47,48}	G.S. 60% In situ concrete; 40% precast 30% stressed concrete; LEED, 30% structural; no limit others, BRE, responsibly sourced cement ^{23,26,7}	Geopolymer based cement fully replaces Portland cement arranged for non-structural, structural	Geopolymer based cement fully replaces Portland cement, arranged for non- structural and structural ^{13, 28}
Reduce transportation by reusing and recycled materials	National Waste Policy Australia advice to reduce waste, re-use to reduce environmental impact ³⁵	Green tools credit reusing and recycling up to 40% of materials, not directly credited; obtained from 30km radius of the site 2,15,35,37	Reuse has been considered in material production and building elements	Transportation reduction by increasing reuse and recycling is considered in current study in UK ³²
Transportation by water or rail not truck, Reduce transportation by localizing	15% of bricks are transported to distributor's yard or jobsite by rail and 85% by truck ^{19, 30}	LEED, Regional Materials, up to 2 points ¹⁴ tools advise localizing, using water and rail instead of road ^{2,15}	Localizing has been considered	Transport of construction materials in UK has been examined in London Olympics ³⁰

Sources: 1-(Cement Concrete & Aggregates Australia 2015; Gonzalez-Fonteboa 2005) 2-(Green building Council of Australia GBCA 2008) 3-(Subasic 2016) 4-(Ash Development Association of Australia 2013; Low carbon living CRC 2015) 5-(Green Building Council of Australia 2012) 6-Chapter Seven 7-(US Green Building Council 2010) 8.(Concrete Block Association 2013) 9-(GBCA 2016) 10- (LEED 2016)); 11-(Poon, Kou & Lam 2002; Concrete Block Association 2013) 13-(Uche 2008; PCA 2014) 14-(Brick Development Association 2009); 15-(LEED 2014) 16-(Kang and Kren 2007) 17-(Volz and Stovner 2010) 18-(Obla, Kim & Lobo. 2010) 19-(Brick Development Association 2014) 21-(LEED 2014) 22-(Steel Construction Information 2014) 23-(GBCA 2008; US Green Building Council 2011) 24-(LEED US Green Building Council 2005) 25-(Steel Construction Information 2014; Greenspec 2015) 26-(Ash Development Association of Australia 2013) 27-(US Green Building Council 2011) 28-(Geopolymer House 2011; Nath & Sarker 2014) 29- (Forest Stewardship Council 2010) 30-(Learning Legacy 2012; Benn, Dunphy & Griffiths 2014) 31-(Ecospecifier Global 2016) 32-(Allwood et al. 2012; UK Indemand 2014, 2015) 34-(Learning Legacy 2012; Inhabitat 2014; Steel Construction Information 2014) 35-(DEE 2012) 36-(Chisholm 2011) 37- (BREEAM 2014b); 38-(Dowling 2010) 39-(Kang & Kren 2007) 41-(Brick Industry Association 2016) 42- (CNN 2012) 43- (FSC 2015) 44-(Tam, Gao & Tam 2005) 45-(NSW Government 2010) 46-(Zeobond Group 2014) 47-(Geopolymer Institute 2014) 48-(Wellcamp 2014) | Table prepared by Author

Appendix D

Table A.D.2: Bioclimatic conditions of the research considered in current practice; green tools (Green Star, LEED and BREEAM); and from research and lab

Bioclimatic Design Principles Criteria	Current conditions	Australian Tool Green Star (GBCA)	US Green Tool LEED	UK Green Tool BREEAM	Research and Lab
Concrete from recycled aggregates	In Australia, there are a number of manufactured and recycled aggregates readily available in certain localities ¹	Green Star, one point, 20% of aggregate for structural purpose; no natural aggregate used in non-structural purposes ²	LEED, recycled content, 10-20% of aggregate up to 3 points; ^{2, 24} ; 20-30% of aggregate for structural 100% non-structural purposes, US ^{18,36}	BREEAM, 25-50% RA; no restriction in 16 MPa and 40 MPa; 20% Designated concrete 20-40 MPa ^{2, 36}	ADAA, ASA, UNSW, Standards Australia; ⁴ , fully RA for non- structural; 30-75-80 % RA for structural ^{13,11}
Concrete block from recycled aggregate	24% recycled content of an aggregate concrete block ⁸	Green Star, 40% RA; no natural aggregates in non-structural ^{23,33}	ASTM, structural 20-25% coarse aggregate; 100% up to 20 MPa ^{18, 36}	BREEAM, no restriction in 16 MPa and 40 for Concrete block ³⁶	UK, USA, AUS; ¹¹ , fully RA for concrete block ¹³
Brick from recycled aggregates	Current level of recycled material content in brick is 11% 14,41	Green Star, not directly credit, Mat-3, 80% reused material ^{2,9, 16}	LEED, recycled content in brick 10-20%, MR 4, 2 points, 2 ½ point ¹⁴	BREEAM; all waste reused; recycled content is 11% ¹⁴	US, UK reuse fully recycled aggregate for brick, 6 points ^{11,14}
Steel from average recycled content	Primary typically 10-15% of scrap steel, Secondary 100% scrap based production ^{25, 34}	Green Star, Mat-6; maximum 60% post-consumer recycled content ²³	LEED, 65-97.5% post-consumer recycled content ^{23, 16}	BREEAM, Mat-6;60% recycled content; ³⁸ 97.5% beams, plates; 65% bars; 66% steel deck, ¹⁶	Steel from 65-97.5% post- consumer recycled content ^{22, 16}
Reuse recycled and post- consumer steel in structural & non-structural	Scaffolding, formwork, sheet piles, etc., London Olympic Stadium ^{32, 34}	95% of joinery; 50% of structural framing, roofing, designed to be disassembled ⁵	LEED, 1-2 points to 75-100% reuse of existing walls, floors and roof. ^{24, 3}	BREEAM, Mat-6; maximum 60% recycled content ²³	Steel products are re-usable, steel piles, hollow sections; gauge, purlins, rails ^{32,31}
Reduce material use in steel structural design	Some current green projects have reduced materials use in design 10-20% ²³	Green Star, Mat-6, grade reduced materials in design,10-20%, ²³ Mat-10, one point for 20% reduce	LEED, eliminating the need for materials in the planning and design phases, ^{10, 7}	BREEAM, grade reduced materials in design ²¹ avoiding over-design, material reuse ³⁹	Integrative Design Process (IDP) Linear design; the London Olympics structure 1/10 ^{32,42}
Reuse recycled timber and post-consumer FSC timber	FSC works in 80 countries, 24000 FSC chain of custody certificates are active in 107 countries ^{23,}	Green Star 95% of all timber products re-used, post-consumer; FSC certified timber ^{22, 23}	LEED, timber products re-used, post- consumer; 50% FSC certified timber, up to 1 point ^{32, 29, 24}	BREEAM; up to three points where timber is part of a pre-or post-consumer waste stream ³⁶	AUS; fully timber products re- used, post-consumer, recycled or are FSC certified timber ⁴³
Roof tiles from recycled tiles	In some countries materials such as concrete roof tiles, removed separated and recycled ^{44, 45}	Green Star, Mat-5 one point, where no natural aggregates are used in non-structural uses ²³	LEED credits; produced from postconsumer recycled content, from the waste, up to3.5 points ^{20,21}	BREEAM; M03, roof tiles can be extracted from the waste stream ³⁶	US; UK; AUS,50% Roof tile from recycled aggregate RA; roof tiles are 100% recoverable ^{21,45}
Thermal insulation from recycled content	Thermal insulation is fully recyclable, i.e. wool content, ³¹	Green Star, not directly credit but 80% recycled content advised ^{27,}	LEED, MR4, 20% or more recycled thermal insulation, one point ^{12, 7}	80% thermal insulation must be responsibly sourced 1 point ³⁷	US; UK; Thermal insulation 100% from recycled content; ^{25,}
Portland cement replaced with Geopolymer based cement	Geopolymer has been used in structural, non-structural, e.g. GCI in Qld, Wellcamp Airport ^{46,47,48}	Green Star; Maximum 60% In situ concrete 40% precast and 30% for stressed concrete; 30% for 1 point and 40% for 2 points ^{23, 26}	LEED Concrete consists of at least 30% fly ash; 50% recycled content or reclaimed aggregate; 90% recycled content or reclaimed aggregate ^{23, 12,7}	One point awarded where cement used to make cement as the supply chain process and must be responsibly sourced ⁴⁰	Geopolymer cement fully replaces Portland cement, arranged for non-structural and structural purposes ^{13, 28}
Reduce transportation by reusing and recycling materials	National Waste Policy Australia advice to reduce waste, re-use to reduce environmental impact ³⁵	Green tools credit the reusing and recycling up to 40% of materials, not directly credited ^{2, 15, 35}	Green tools credit the reusing and recycling up to 40% of materials, not directly credited ^{2, 15}	One credit where obtained from waste processing site(s) within a 30km radius of the site, ³⁷	Transportation reduction by increasing reusing, recycling is considered in current study, UK ³⁹
Transportation by water or rail not truck, Reduce transportation by localizing	15% of bricks are transported to distributor's yard or jobsite by rail and 85% by truck ^{19, 30}	Green Star, advise localizing, using water and rail instead of road ^{2,15}	LEED, Regional Materials, up to 4 points; ¹⁴ tools advise localizing, using water and rail instead of road ^{2,15}	Regional Materials, localizing, using water and rail instead of road ^{2,15}	Transport construction materials in UK has already examined in London Olympics ³⁰

Sources: 1-(Cement Concrete & Aggregates Australia 2015; Gonzalez-Fonteboa 2005) 2-(Green building Council of Australia GBCA 2008) 3-(Subasic 2016) 4-(Ash Development Association of Australia 2013; Low carbon living CRC 2015) 5-(Green Building Council of Australia 2012) 6-Chapter Seven 7-(US Green Building Council 2010) 8.(Concrete Block Association 2013) 9-(GBCA 2016) 10- (LEED 2016); 11-(Poon, Kou & Lam 2002; Concrete Block Association 2013) 12- (LEED 2016)13-(Uche 2008; PCA 2014) 14-(Brick Development Association 2009); 15-(LEED 2014) 16-(Kang and Kren 2007) 17-(Volz and Stovner 2010) 18-(Obla, Kim & Lobo. 2010) 19-(Brick Development Association 2014); Tyrell & Goode 2014) 20-(Boral 2014) 21-(LEED 2014); 22-(Steel Construction Information 2014) 23-(GBCA 2008; US Green Building Council 2011) 24-(LEED US Green Building Council 2005) 25-(Steel Construction Information 2014; Greenspec 2015) 26-(Ash Development Association of Australia 2013) 27-(US Green Building Council 2011) 28-(Geopolymer House 2011; Nath & Sarker 2014) 29- (Forest Stewardship Council 2010) 30-(Learning Legacy 2012; Benn, Dunphy & Griffiths 2014) 31-(Inhabitat 2014; Learning Legacy 2014; Steel Construction Information 2014) 32- (Ecospecifier Global 2016) 33 (CBA Concrete Block Association 2013) 34- (Onesteel 2016) 35- (DEE 2012); 36- (Chisholm 2011) 37- (BREEAM 2014)); 38-(Dowling 2010) 39-(UK Indemand 2014, 2015); 40-(BREEAM BRE 2014) 41-(Brick Industry Association 2016) 42- (CNN 2012) 43- (FSC 2015) 44-(Tam, Gao & Tam 2005) 45-(NSW Government 2010) 46- (Zeobond Group 2014) 47-(Geopolymer Institute 2014) 48-(Wellcamp 2014) | Table prepared by Author

Appendix D

Table A.D.3: Bioclimatic conditions – current; from best practice with green tools (Green Star, LEED and BREEAM); from this research model; and from research and lab + Percentage carbon reductions.

Bioclimatic Design Principles (BDP) Criteria	Current conditions, Implemented	Conditions with Green tools G.S., LEED, BREEAM	Conditions in this research	Conditions in research and lab.
Concrete from recycled aggregates	In Australia, there are a number of manufactured and recycled aggregates readily available in certain localities ¹	G.S. and LEED 1-3 points 20-30% RA for structural purpose; BRE 25-50% in 20-40 MPa - no restriction, 100% non-structural ^{2, 18, 36}	Fully RA for non-structural purpose; 100% RA for non-structural; 80 % RA for structural purpose ⁶	ADAA, ASA, UNSW, Standards Australia; ⁴ , fully RA for non-structural; 30-75-80 % RA for structural; ^{13,11}
Concrete block from recycled aggregate	24% recycled content of an aggregate concrete block ⁸	G.S., BRE, 40%; US 25% RA structural; 100%, or no natural aggregates in non-structural ^{18,23,36}	Aggregate for concrete block fully from recycled aggregate ¹³	UK, USA, AUS; ¹¹ , fully RA for concrete block; ¹³
Brick from recycled aggregates	Current level of recycled material content in brick is 11% ^{14,41}	G.S., 30% ; ^{16, 23} ; LEED 20%; BRE 11% ISO, up to 10 points for 10% Recycled aggregate ^{14,16,36}	Reuse the recycled aggregate for brick, 67% ¹⁹	US; UK, Reuse fully the recycled aggregate for brick, 6 points; ^{11, 17}
Steel from average recycled content	Primary typically 10-15% of scrap steel, Secondary 100% scrap based production 25, 34	G.S. Mat-6, 60%; LEED 65-97.5%; BRE, Mat-6, 60%; -97.5% beams, plates; 65% bars; 66% steel deck post-consumer recycled content ^{23,16,38}	Steel from fully post-consumer recycled contents	Steel from 65-97.5% post-consumer recycled contents; ^{22, 39}
Reuse recycled and post- consumer structural and non- structural steel	Scaffolding, formwork, sheet piles, etc., London Olympic Stadium ^{32, 34}	G.S., 95% Joinery, 50% structural framing, roofing; LEED 75-100% existing wall, floor, roof; BRE, Mat-6, 60% recycled content ^{3,5,23,24}	Use 40% recycled and post- consumer steel elements	Steel products are re-usable, steel piles, hollow sections; gauge, purlins, rails ^{32,3}
Reduce material use in steel structural design 10-20%	Some current green projects have reduced materials use in design 10-20% 23	G.S., Mat-6, 10-20% one point; LEED, eliminating need for materials in the design stage; BRE reduced, avoiding over-design ^{23,21,10,7,32}	Reduced materials use in structural design 10-20%	Integrative Design Process (IDP) Linear design; the London Olympics' structure 1/10, ^{32, 42}
Reuse the recycled timber and post-consumer FSC timber	FSC works in 80 countries, 24000 FSC chain of custody certificates are active in 107 countries ^{23,}	G.S. 95% re-used, post-consumer; FSC certified timber; up to 3 points; LEED, 50% FSC; BRE, 3 points, post-consumer waste stream ^{22, 23, 32,24,29}	60% of all timber products re-used, post-consumer recycled timber; FSC certified timber	AUS; fully timber products re-used, post-consumer, recycled or are FSC certified timber ⁴³
Roof tile from recycled tile	In some countries materials such as concrete roof tiles, removed separated and recycled ^{44, 45}	G.S. Mat-5, 1 point, no natural aggregates are used; LEED, from the waste, up to 3.5 points, BRE, M03, from the waste stream ^{20,21,23,36}	50% Roof tile from recycled aggregate ²¹	US; UK; AUS,50% Roof tile from recycled aggregate RA; roof tiles are 100% recoverable ^{21,45}
Thermal insulation from recycled content	Thermal insulation is fully recyclable, i.e. wool content, ³¹	G.S. 80% advised; LEED MR4 20%, ½ point, BRE 80%, 1 point, responsibly sourced ^{12.7,27,37}	Thermal insulation from fully recycled waste ²⁵	US; UK; Thermal insulation 100% from recycled waste; ²⁵
Portland cement replaced with Geopolymer based cement	Geopolymer has been used in structural, non-structural, e.g. GCI in Qld, Wellcamp Airport ^{46,47,48}	G.S. 60% In situ concrete; 40% precast 30% stressed concrete; LEED, 30% structural; no limit others, BRE, responsibly sourced cement ^{23,26,7}	Geopolymer based cement fully replaces Portland cement arranged for non-structural, structural	Geopolymer based cement fully replace with Portland cement, arranged for non- structural and structural; ^{13, 28}
Reduce transportation by reusing and recycled materials	National Waste Policy Australia advice to reduce waste, re-use to reduce environmental impact ³⁵	Green tools credit reusing and recycling up to 40% of materials, not directly credited; obtained from30km radius of the site ^{2,15,35,37}	Reuse has been considered in material production and building elements	Transportation reduction by increasing reusing and recycling is considered in current study in UK; ³²
Transportation by water or rail not truck, Reduce transportation by localizing	15% of bricks are transported to distributor's yard or jobsite by rail and 85% by truck ^{19, 30}	LEED, Regional Materials, up to 2 points ¹⁴ tools advise localizing, using water and rail instead of road ^{2,15}	Localizing has been considered	Transport the construction materials in UK has already examined in London Olympics; ³⁰
Carbon Emissions	Six case studies Current Implementation	Examine the six case studies with Green Tool	The six case studies with Research Model	UK Government has funded UK- Indemand Center ³²

Sources: 1-(Cement Concrete & Agregates Australia 2015; Gonzalez-Fonteboa 2005) 2-(Green building Council of Australia GBCA 2008) 3-(Subasic 2016) 4-(Ash Development Association of Australia 2013; Low carbon living CRC 2015) 5-(Green Building Council of Australia 2012) 6-Chapter Seven 7-(US Green Building Council 2010) 8.(Concrete Block Association 2013) 9-(GBCA 2016) 10- (LEED 2016); 11-(Poon, Kou & Lam 2002; Concrete Block Association 2013) 13-(Uche 2008; PCA 2014) 14-(Brick Development Association 2009); 15-(LEED 2014) 16-(Kang and Kren 2007) 17-(Volz and Stovner 2010) 18-(Obla, Kim & Lobo. 2010) 19-(Brick Development Association 2019); 15-(LEED 2014) 20-(Boral 2014) 21-(LEED 2014); 22-(Steel Construction Information 2014) 23-(GBCA 2008; US Green Building Council 2011) 24-(LEED US Green Building Council 2005) 25-(Steel Construction Information 2014; Greenspec 2015) 26-(Ash Development Association of Australia 2013) 27-(US Green Building Council 2011) 28-(Geopolymer House 2011; Nath & Sarker 2014) 29- (Forest Stewardship Council 2010) 30-(Learning Legacy 2012; Benn, Dunphy & Griffiths 2014) 31-(Ecospecifier Global 2016) 32-(Allwood et al. 2012; UK Indemand 2014, 2015) 34-(Learning Legacy 2012; Inhabitat 2014; Steel Construction Information 2014) 35-(DEE 2012) 36-(Chisholm 2011) 37- (BREEAM 2014b); 38-(Dowling 2010) 39-(Kang & Kren 2007) 41-(Brick Industry Association 2016) 42- (CNN 2012) 43- (FSC 2015) 44-(Tam, Gao & Tam 2005) 45-(NSW Government 2010) 46-(Zeobond Group 2014) 47-(Geopolymer Institute 2014) 17 able prepared by Author

Between 17 to 32 %

Between -23 % to 57 %

Between 50 to 65 %

Proposes 80 %

Reduction

Bioclimatic criteria		A.1 Floor construction systems	A.2. Wall construction systems	A.3. Roof construction systems
Concrete from recycled aggregates	Study	80% RA for fixing posts in the ground 1	80 % RA for concrete slab on ground ¹	80 % RA for concrete slab on ground $^{\rm 1}$
	Green Star	20% RA for fixing posts in the ground 2	20 % RA for fixing posts in the ground $^{\rm 2}$	20 % RA for fixing posts in the ground $^{\rm 2}$
Concrete block and brick from recycled	Study	-	Concrete block wall from (67-100%) RA ³	-
aggregate	Green Star	-	Concrete block wall from 20% RA ³	-
Brick from recycled aggregate	Study	Brick from 67% RA for posts Use recycled bricks 60% ⁴	Brick wall from 67% RA ⁴	_
	Green Star	-	-	-
Steel from average recycled content	Study	Use steel produced with 100% recycled content ^{8,13}	Use steel produced with 100% recycled content ^{8,13}	Use steel produced with 100% recycled content ^{8,13}
	Green Star	Use steel produced with 90% recycled content ^{6,7}	Use steel produced with 90% recycled content ^{6,7}	Use steel produced with 90% recycled content ^{6,7}
Reuse recycled and post-consumer structural and non- structural steel	Study	Reuse 40% recycled steel in structural and non-structural elements ^{31,32}	Reuse 40% recycled steel in structural and non-structural elements ^{31,32}	Reuse 40% recycled steel in th structural and non-structural elements ^{31,32}
	Green Star	-	-	-
Reduce material (steel) use in design 10-20%	Study	Reduced 20% steel use in design ^{12, 14}	Reduced 20% steel use in design ^{12, 14}	Reduced 20% steel use in design ^{12, 14}
		Reduced 20% steel use in design ^{, 15,16, 5, 6, 12}	Reduced 20% steel use in design ^{, 15,16, 5, 6, 12}	Reduced 20% steel use in design ^{15,16, 5, 6, 12}
Reuse recycled timber and post-consumer FSC certified timber	Study	Use 100%, recycled timber or FSC certified timber, reuse ⁶ .	Use 100%, recycled timber or FSC certified timber, reuse ⁶ .	Use 100%, recycled timber or FSC certified timber, reuse ⁶ .
	Green Star	Use 100%, recycled timber or FSC certified timber, reuse ⁶ , 7, 12, 18, 19	Use 100%, recycled timber or FSC certified timber, reuse ^{6,} 7, 12, 18, 19	Use 100%, recycled timber on FSC certified timber, reuse ⁶ , ¹² , ¹⁸ , ¹⁹
Roof tile from recycled tiles	Study	-	-	Use 13% recycled tile, tiles with 45% recycled content ^{5, 2}
	Green Star	-	-	-
Thermal insulation from recycled content	Study	-	Thermal insulation 100% from recycled content ⁸	Thermal insulation 100% from recycled content ⁸
	Green Star	-	-	-
Replaced Portland cement with	Study	Replace 100% of Portland cement with geopolymer ^{12, 21}	Replace 100% of Portland cement with geopolymer ^{12, 21}	Replace 100% of Portland cement with geopolymer ^{12, 21}
geopolymer cement	Green Star	Replace 60% of Portland cement with geopolymer ⁶ ,9, 22	Replace 60% of Portland cement with geopolymer ⁶ ,9, ²²	Replace 60% of Portland cement with geopolymer ⁶ ,9,2

Table A.D.4: Bioclimatic criteria examined in general Australian floor, wall and roof construction systems using the research model and the Green Star rating tool

Sources: 1-(CCAA) 2015; Gonzalez-Fonteboa 2005) 2-(Green building Council of Australia 2008) 6-Chapter Seven 3-(Uche 2008; PCA 2014) 4-(Brick Development Association 2014; Tyrell & Goode 2014) 5-(LEED 2014) 6-(GBCA 2008; US Green Building Council 2011) 7-(LEED US Green Building Council 2005) 8-(Steel Construction.Information 2014; Greenspec 2015) 9-(Ash Development Association of Australia 2013) 10-(Ecospecifier Global 2016) 12-(Allwood et al. 2012; UK Indemand 2014), 2015) 13-(Inhabitat 2014; Steel Construction.Information 2014) 14-(CNN 2012) 15-(US Green Building Council 2010) 16-(LEED 2016) 17-(FSC 2015) 18-(Steel Construction Information 2014) 19-(FSC 2010) 20-(NSW Government 2010) 21-(DEE 2012) 22-(US Green Building Council 2010) | (RA = Recycled Aggregate, PC = Portland cement, GC = Geopolymer Cement.| Table Prepared by Author,

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