

A Critical Review on Structural Health Monitoring: Definitions, Methods, and Perspectives

Vahid Reza Gharehbaghi¹, Ehsan Noroozinejad Farsangi^{2*}, Mohammad Noori³, T.Y. Yang⁴,
Shaofan Li⁵, Andy Nguyen⁶, Ch. Málaga-Chuquitaype⁷, Paolo Gardoni⁸, Seyedali Mirjalili^{9,10}

¹ Adjunct Associate Research Fellow, School of Civil Engineering and Surveying, University of Southern Queensland, Springfield Campus, Queensland, Australia
Email: Vahidreza.Gharehbaghi@usq.edu.au

 <https://orcid.org/0000-0002-6831-313X>

² A/Professor, Faculty of Civil and Surveying Engineering, Graduate University of Advanced Technology, Kerman, Iran

*Corresponding Author Email: noroozinejad@kgut.ac.ir ; e.noroozinejad@alumni.ubc.ca

 <https://orcid.org/0000-0002-2790-526X>

³ Professor, Department of Mechanical Engineering, California Polytechnic State University, CA, United States (ASME Fellow)

Email: mnoori@calpoly.edu

 <https://orcid.org/0000-0002-2793-5194>

⁴ Professor, Department of Civil Engineering, University of British Columbia, Vancouver, Canada

Email: yang@civil.ubc.ca

⁵ Professor, Dept of Civil and Environmental Engineering, University of California-Berkeley, CA, United States

Email: shaofan@berkeley.edu

 <https://orcid.org/0000-0002-6950-1474>

⁶ A/Professor, School of Civil Engineering and Surveying, University of Southern Queensland, Springfield Campus, Queensland, Australia

Email: Andy.Nguyen@usq.edu.au

⁷ A/Professor, Department of Civil and Environmental Engineering, Imperial College London, London, UK

Email: c.malaga@imperial.ac.uk

 <https://orcid.org/0000-0002-2538-7374>

⁸ Professor, Civil and Environmental Engineering Department, University of Illinois at Urbana-Champaign, Urbana, IL 61801, United States

(Director of Mid-America Earthquake Center (MAE))

Email: gardoni@illinois.edu

⁹ Centre for Artificial Intelligence Research and Optimisation, Torrens University, Adelaide, SA 5000, Australia

¹⁰ YFL (Yonsei Frontier Lab), Yonsei University, Seoul 03722, Republic of Korea

Email: ali.mirjalili@laureate.edu.au

 <https://orcid.org/0000-0002-1443-9458>

39 A Critical Review on Structural Health Monitoring: 40 Definitions, Methods, and Perspectives

41

42

43 Abstract 44

45 The benefits of tracking, identifying, measuring features of interest from structure responses have
46 endless applications for saving cost, time and improving safety. To date, structural health
47 monitoring (SHM) has been extensively applied in several fields, such as aerospace, automotive,
48 and mechanical engineering. However, the focus of this paper is to provide a comprehensive up-
49 to-date review of civil engineering structures such as buildings, bridges, and other infrastructures.
50 For this reason, this article commences with a concise introduction to the fundamental definitions
51 of SHM. The next section presents the general concepts and factors that determine the best strategy
52 to be employed for SHM. Afterward, a thorough review of the most prevalent anomaly detection
53 approaches, from classic techniques to advanced methods, is presented. Subsequently, some
54 popular benchmarks, including laboratory specimens and real structures for validating the
55 proposed methodologies, are demonstrated and discussed. Finally, the advantages and
56 disadvantages of each method are summarized, which can be helpful in future studies.

57 **Keywords:** Structural Health Monitoring (SHM); Damage Detection Methods; SHM
58 Benchmarks; Anomaly Detection; Structural Safety; Reliability

59

60 1 Introduction

61 In general, ‘damage’ is defined as a significant factor influencing the structural behaviour in such
62 a way that leads to degradation in the current or future performance of a structure. Therefore, a
63 clear description of damage requires comparing two distinct conditions of a structure: the status of
64 being either ‘healthy’ or ‘damaged’[\(1\)](#). The former describes the base or ‘healthy’ condition of the
65 structure, and the latter indicates the current or the deteriorated state. As a definition, a healthy
66 structure functions efficiently and preserves its integrity throughout its lifetime [\(2\)](#). On the other
67 hand, in the field of structural identification, damage is associated with changes first in the material
68 and then in the geometry and topology of the structure, e.g., changes to the boundary conditions
69 and connections [\(3\)](#).

70 Existing techniques for identifying damage cover a wide range, from conventional inspection
71 methods carried out by experts to cutting-edge automated techniques using smart sensors and
72 Artificial Intelligence (AI). The latter identification procedure integrates different fields, namely
73 computer science, data science, electronics, mechanics, material sciences, and civil engineering,
74 which shape the foundation of the interdisciplinary field called Structural Health Monitoring
75 (SHM).

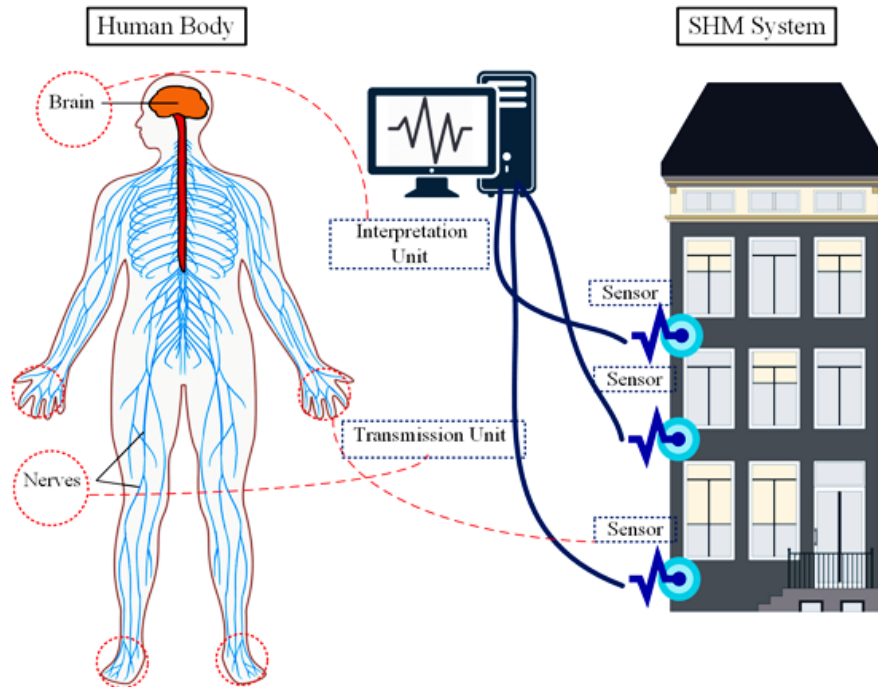
76 From a general perspective, monitoring the response of structures and detecting probable damages
77 to enhance their performance level and reduce upkeep costs are considered the prime target in
78 SHM. Consequently, structures that benefit from an SHM system commonly experience prolonged
79 service life. In contrast, those that have no such system in place face notably higher risks of
80 structural failures. SHM also guarantees the system's integrity to some extent and can prevent
81 possible failures in the future by sounding a pre-emptive alarm regarding abnormal behaviors.

82 Over the past two decades, a wide array of inspection approaches have been examined, developed,
83 and established by scientists and engineers to identify, locate, and assess different types of damage.
84 Accordingly, researchers have published many papers to shed light on the fundamentals and
85 applications of those methods. Herein, the authors have attempted to provide a comprehensive
86 perspective on definitions of SHM and damage detection techniques that are described in the
87 following four sections. First, the SHM is defined briefly and its principal objectives are explained.
88 Second, the general concepts within this scope are summarized. In the third part, several damage
89 detection approaches are discussed, and the last section highlights some important SHM
90 benchmarks. Subsequently, conclusions, recommendations, and prospects are provided for future
91 use.

92 **2 Structural Health Monitoring (SHM)**

93 Structural Health Monitoring (SHM) yields precious details regarding a system's behavior by
94 analyzing its responses and evaluating its current mechanical state. A system may include a high-
95 rise building, a bridge, an infrastructure system, or a simple beam. Initially, SHM was employed
96 for damage identification of aircraft in the realm of aerospace engineering and industry. In the late
97 1970s (4), however, it was implemented to investigate offshore platforms. At the beginning of the
98 1990s, SHM was extended to civil engineering and infrastructure systems. Just to name some of
99 its applications in this particular field, Beck and Katafyglotis (5) designated a probabilistic
100 identification approach for global health monitoring of a structure by detecting any significant
101 changes in its stiffness distribution. Additionally, Mita (6) presented an overview of the rapidly
102 emerging SHM in Japan's civil engineering in late 1999. In 1997, Al-Khalidy et al. (7) presented
103 one of the earliest studies on the health monitoring of linear systems using wavelets; they discussed
104 the need for promoting SHM for damage detection in infrastructure systems.

105 With the emergence of new Sensing Technologies, significant breakthroughs in computers, and
106 incorporating structural control methods(8, 9), SHM has expanded extensively in the past two
107 decades. The general idea of SHM can be described through an analogy with the human nervous
108 system (Figure 1) (10). In an intelligent structure embedded with a network of sensors, the sensing
109 function is similar to the nervous system. Also, sensors receive various signals such as vibration,
110 strain, stress, or temperature similar to the human nervous system, which forms a transmission unit
111 that sends different signals to the brain, functioning as a processing and interpretation/diagnostic
112 unit.



114 Figure 1 Comparison between the human body and the SHM system (adopted from (10))

115 By and large, a conventional SHM system consists of three major elements (11):

- 116
- Contact or non-contact sensors
 - 117 • Processing unit (composed of data acquisition, transmission, and storage)
 - 118 • Data interpretation system (made of diagnostic methods and information management)

119 Interpretation includes diagnosis (assessment) and prognosis (prediction) of structural changes.
 120 The diagnosis notifies the onset of damage, its location, or its severity. This procedure is conducted
 121 either by passive diagnosis (i.e., by a passive sensor such as strain gauges) or by active diagnosis
 122 (i.e., by an actuator and intelligent sensors) (12). The fusion of these components leads to a fitting
 123 SHM system in a particular civil engineering project.

124 SHM is considered as an inverse problem wherein the structural defects are recognized through
 125 the measured data of known inputs. Also, this process is a system identification problem (12).
 126 Based on research by Rytter (13), damage identification levels in SHM can be categorized into the
 127 following levels according to the extent/scope of the information acquired from the structure:

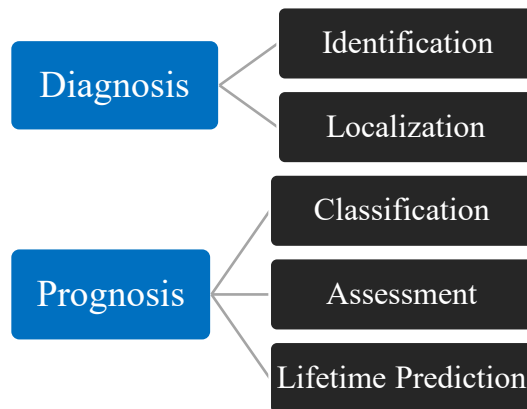
- 128
- **Level 1:** Identification: determining the existence of a defect on a global scale.
 - 129 • **Level 2:** Localization: determining the location and coordinates of the damage.
 - 130 • **Level 3:** Assessment: determining the intensity of damage in various components.
 - 131 • **Level 4:** Lifetime prediction: estimating the structure's remaining life.

132 Specifically, the first stage involves monitoring the desired properties of the structure over time,
 133 and it provides answers regarding the overall presence of damage in a structure. Comparatively,
 134 the second level appears to be more complicated as it requires determining the location of damage
 135 and its orientation(12).

136 In general, the first two levels are defined as diagnosis steps and the next ones as prognosis levels.
137 Importantly, levels 1 and 2 can be evaluated without using any model, but level 3 requires
138 numerical modeling. The last level requires using processes such as breakdown mechanics,
139 fatigue-life analysis, reliability analysis, or structural design assessment (14). In addition, level 4
140 stems from level 3, wherein the assessment of fracture parameters is utilized to achieve fatigue life
141 analysis to specify the structure’s remaining life (12).

142 It seems that among a large number of publications, a significant portion of studies found in the
143 existing literature is targeted at levels 1-3 (15-17), and relatively small number of papers seek to
144 address level 4 (18, 19). Herein, most of the existing research is concerned with applying damage
145 detection strategies to either laboratory tests or analytical models, not real structures (20). A
146 growing number of researchers have concluded that to assess the risk and the severity of the
147 damage as the necessary information for making a proper decision about the safety of the structure
148 and prevent potential catastrophic failure, there is a need to recognize the type of damage. For
149 instance, in the case of a building under fire, it is crucial to have an SHM system that can detect
150 the severity of existing damage and hence determine if the plan for emergency evacuation is safe
151 to be carried out. Consequently, a new level called ‘classification’ has been recently presented,
152 aiming to designate the type of damage and bridge the existing gap (21) (See Figure 2).

153



154

155

Figure 2 Damage identification levels

156

157 3 General Concepts for SHM

158 The development of a methodology or a technique for structural health monitoring depends on
159 several factors. They include the complexity of the dynamic response, whether the system behaves
160 linearly or nonlinearly, the scale and dimension of the structure, how easily the physical system
161 can be modeled or its behavior be simulated, the nature of the excitation, or how easily a feedback
162 mechanism can be identified to assess the behavior. Some of the crucial factors determining the
163 effective strategy for SHM are depicted in Figure 3 and are elaborated in the following paragraphs.



Figure 3 Common concepts for SHM

164

165 **3.1 Inspection Scale: Global or Local**

166 According to prior research by Doebling et al. (22), detecting damage is performed by global or
 167 local methodologies. Global methods are used to spot the existence of damage and assess the state
 168 of the entire structure. In contrast, local methods assist in locating damage or monitoring a specific
 169 relevant parameter/metric in the system (23). Visual inspection or non-destructive tests, including
 170 ultrasonic, radiography, and acoustic emission, are some practical tools for pinpointing the
 171 damage. Since minor faults, such as cracks and delamination, may not show up in global
 172 measurements unless they are large, localized measurements are also necessary (24).

173 Generally, local methods are more common for small and non-complex structures since data is
 174 required about the initial state of the structure and such methods designate the vicinity of the
 175 damaged member (18). Hence, they are time-consuming and, most likely, quite expensive (25).
 176 Consequently, to overcome those limitations, specialists take advantage of global methods, which
 177 provide valuable information based on vibration characteristics, such as natural frequencies and
 178 mode shapes, especially in complicated structures. Notably, an efficient strategy is applied to
 179 identify the structural characteristics of a small area by using global methods, then implementing
 180 the local damage assessment methods to zoom in on the damage location (24).

181 **3.2 Response type: Static or Dynamic**

182 A vast majority of damage detection methods are based on assessing the response of the structure
 183 due to an excitation source. In this respect, these strategies form two main groups: static response
 184 assessment (strain or stress) and dynamic responses (frequencies, mode shapes, or modal
 185 damping). Compared to dynamic measurements, measuring static responses is more
 186 straightforward but less sensitive to changes resulting from damages (22). Accordingly, using
 187 dynamic responses is more efficient for detecting both abrupt and gradual changes, such as

188 detecting deterioration. Nonetheless, dynamic measurement of responses requires controlling
189 environmental and operational effects to attain accurate data. In earlier research in this area,
190 dynamic-based methods relied on frequency measurements., This was principally due to the
191 greater accuracy of devices measuring frequency compared to devices measuring mode shape or
192 geometrical shape. With the advancement of instrumentation, other methods, such as vibration-
193 based methods, were also considered.

194 Since measuring static responses is more reliable than measuring dynamic ones, some researchers
195 deployed static data in their study cases (displacement and strain) for damage detection (26-30).
196 The occurrence of measurement errors in damage detection data by static response measurement
197 is relatively negligible compared with dynamic responses. While the dynamic matrix requires
198 stiffness, mass, and damping matrixes, the structure's stiffness matrix is solely needed in static
199 concepts. For this reason, static methods generally have simpler equations.

200 **3.3 Behaviour: Linear or nonlinear**

201 The presence of damage induces more complex behavior and causes nonlinear changes. Moreover,
202 damage may cause a structure with a typically linear behaviour to develop nonlinear reactions such
203 as cracking, impacts and/or rattling, delamination, stick/slip, rub, or loosened connections (31, 32).
204 To illustrate these phenomena, Gudmundson (33) proved via experimental tests on a cantilever
205 beam that natural frequencies may increase instead of decline due to breathing phenomena. This
206 behavior confirms the fact that the crack alternately opens and closes during experimental tests.
207 There are different methods for considering nonlinear effects, for instance, nonlinear output
208 frequency response functions (NOFRFs) and/or Higher-Order Frequency Response Functions
209 (HOFRF). In this regard, Sinou (34) classified and reviewed linear and nonlinear methods
210 comprehensively.

211 **3.4 Computation: Model-based or Signal-based**

212 Anomaly identification can be conducted using a model (also called physics-based approaches),
213 or by signal-based methods (also called data-driven approaches). In the former concept, the
214 damage is recognized through tracking variations in the simulated measurements from the
215 structural model (24). Basically, a model is a mathematical abstraction that connects and correlates
216 the input and the output parameters of a structure using (known or assumed) properties (35). In
217 some cases, it requires a post-process response to predict the damage location and severity. For
218 this reason, various mathematical models have been established, such as finite difference methods
219 (FDMs), finite element methods (FEMs), spectral finite element methods (SFEMs), and boundary
220 element methods (BEMs). In particular, FEM is the most widely used approach due to its
221 versatility in modeling of complex geometries (12).

222 When utilizing the model-based approach, specific parameters of a finite element model simulating
223 the system are updated under the system's responses by studying the dynamic behavior of the FEM
224 model (36-41). Through that process, the FEM model needs to be updated to account for the
225 system changes that occur due to the damage. Model updating includes the optimization of
226 problem solution to seek the optimum set of matrices (mass, stiffness, and damping), leading to
227 the minimization of variances between empirical and computed responses (24). These approaches
228 have some drawbacks because they require prior knowledge of the boundary conditions, damage

229 location, and material properties (14). Moreover, an optimization problem faces challenging issues
230 such as ill-conditioning, which affects the existence, uniqueness, and stability of a solution of an
231 inverse problem, i.e., it is not possible to fully guarantee the determination of the system
232 characteristics based on the given response. Hence, incorporating uncertainty quantification
233 measures such as probabilistic, non-probabilistic, and hybrid methods would be an appropriate
234 alternative (35).

235 It is also important to point out that FEM methods are not quite suitable when dealing with minor
236 or invisible damages. The preferred mathematical model seems to be relying on wave propagation
237 techniques such as SFEM (42). In contrast, signal-based methods rely on statistical analysis and
238 assess the system's response independently; therefore, they do not require additional information
239 concerning the structure's physical properties and parameters (43-47).

240 **3.5 Feedback: Active or Passive**

241 As for the diagnosis, procedures include two classes; passive and active diagnosis (12). Active
242 schemes excite the structures with a guided-wave (GW) or various ultrasonic waves, Lamb waves,
243 shakers, or piezoelectric transducers (32). Piezoelectric materials and devices can be employed as
244 both actuators and sensors (48).

245 On the other hand, when measuring input signals is complicated, passive approaches are employed
246 instead. Passive SHM means embedding various types of passive sensors such as stress, strain,
247 loading, environmental condition, or temperature measurement sensors, which are tracked over
248 time, and the collected data is fed back into a structural model. To put it simply, passive SHM
249 systems 'listen' to the responses yet do not engage with the structure, nor does it affect its dynamic
250 behavior (49). A promising passive method is Acoustic Emission (AE), which uncovers acoustic
251 events associated with the occurrence and extension of defects. Other passive techniques include
252 pieces of equipment that are placed in contact with the structure or on the ground to analyze the
253 dynamic response under ambient excitations, such as the dynamic response of a bridge structure
254 under passing traffic or due to wind and ground motions (42).

255

256 **3.6 Excitation: Forced or Ambient excitation**

257 Dynamic responses of any structure are usually due to two types of excitations; ambient and forced
258 vibrations (50). Ambient excitations are described as stochastic processes such as random white
259 noise. Herein, Random Decrement Technique (RDT) as an effective signal processing method is
260 utilized to measure crosscorrelation functions and free-response decays (51). It is important to note
261 that the use of forced vibration for seismic assessment requires special equipment like eccentric
262 mass shakers to generate the required response magnitude (14). Moreover, using forced vibration
263 testing on existing structures should be done through a well-controlled process as it may cause
264 damage to the structure. Thus, the use of ambient vibration tests as a practical and relatively
265 inexpensive way has increased over the past few years (52-55).

266 **3.7 Domain: Time, Frequency or Time-Frequency**

267 Signal processing techniques have been carried out in different domains, namely time, frequency,
268 or time-frequency domains. Practical vibration analysis begins with acquiring an accurate time-

269 varying signal from vibrometers or accelerometers. Various options and procedures are available
270 to analyze the signal to extract the desired dynamic characteristics that have the potential to
271 illuminate the nature of changes in a structure. Restoring force curves and autoregressive moving
272 average (ARMA) models are a few examples of time-domain methods. In ARMA models, time
273 histories of structural responses are fitted to a model, then the coefficients and residual errors are
274 evaluated as damage-sensitive characteristics.

275 The most commonly used tool for signal processing in the frequency domain is the Fourier
276 Transform (FT) that takes a real-world time-varying signal and splits it into its harmonic
277 components to deliver information about their amplitude, phase, and frequency. By associating the
278 frequencies with the system characteristics and looking at the amplitudes, it is possible to pinpoint
279 changes caused by incurred damages with relative accuracy. This transformation is carried out
280 using Fast Fourier Transform (FFT) algorithms, which are the most popular ones in practical SHM
281 analyses.

282 The time-frequency presentation of a signal makes it possible to recognize transient behaviors
283 induced either by damage (desired) or environmental noise (undesired) overlapping within the
284 frequency of the original signal (56). In contrast to FT, abrupt changes due to damages can be
285 identified with the aid of zooming and focusing on the characteristics of wavelets. Wavelet
286 transforms (WTs), Wigner-Ville distribution (WVD), short-time Fourier transform (STFT),
287 pseudo-WVD (PWVD), empirical mode decomposition (EMD) or ensemble empirical mode
288 decomposition (EEMD), as well as Hilbert-Huang transform (HHT) are some of the common
289 approaches (57, 58).

290 **3.8 Solution: Forward (Direct) or Inverse (Indirect)**

291 Parameter estimation solutions, or system identification, are inverse problems since they focus on
292 inverting the standard ‘forward’ relationship between the parameters and output of a model; the
293 target is to obtain the parameters generating a specific output. Practically, deterministic parameter
294 estimation aims to extract the optimal mathematical model parameters so that the most feasible fit
295 is obtained between the model output and the observed data (35).

296 **4 Traditional Inspection**

297 Traditional inspections can be conducted depending on the value and importance of a structure,
298 repair costs, and failure consequences (12). The most preliminary approach is visual inspections
299 conducted by experienced technical specialists (Figure 4). It is noteworthy to point out, however,
300 that visual inspection is not necessarily the most economical solution. For example, in 2004,
301 bridge inspection expenses were roughly 20M Australian Dollars (AUD) annually in the state of
302 Queensland, Australia (14). Moreover, a visual inspection cannot be practically used in some
303 conventional, especially large and complex structures.

304 Visual inspection techniques can be combined with different types of experimental tests, which
305 are typically categorized as either destructive testing (DTs), primarily used to determine the
306 material properties, or Non-destructive testing (NDT). NDTs aim to inspect the nature of the
307 damage or control its propagation in a member, joint, or various connections. As a result, NDTs
308 mainly point out the variation of physical values of defects and are deployed for Quality-Control

309 (QC), material properties determination, and damage detection (59). There are some differences
 310 between NDTs and SHM. First, regarding the sensing methodology, in SHM, the sensors are
 311 permanent and in fixed positions, while in NDTs, they are brought to the point of investigation.
 312 Secondly, some specialists articulate that SHM should be carried out online or in an automated
 313 fashion, while NDT is conducted via another inspection (60).

314 Although using NDTs may seem feasible for inspecting small structures, they have some
 315 drawbacks. First, employing these techniques usually involves a temporary interruption of the
 316 functionality of the structure. This problem makes them time-consuming and costly. Additionally,
 317 on many occasions, due to the inaccessibility or the invisibility of the location of the damaged area
 318 for the inspector, it may be difficult or impractical to perform a satisfactory damage inspection
 319 (61). Lastly, the characteristics of the material also affect the results. Table 1 summarizes several
 320 NDTs and the principal characteristics of the material that should be measured (62).

321 Overall, these methods are appropriate when the initial information about the vicinity of the failure
 322 is available. Likewise, they are not practical if the member is not accessible or is covered by other
 323 structural components (14). Accordingly, most of these methods are limited to only simple
 324 members such as beams, columns, or plates; and they are not practical in detecting damage in
 325 complex structures, such as multi-story buildings or large bridges (63). A list of commonly used
 326 non-destructive methods is provided in the ASM Handbook (62).

327

Table 1. NDTs and their relative material characteristics (62)

Method	Important Characteristics
Liquid penetrant	Defects must intercept surface
Magnetic particle	Requiring magnetic materials
Eddy current	Requiring conductive or magnetic materials
Radiography and x-ray	Changes in thickness, density, or elemental composition
Neutron radiography	Changes in thickness, density, or elemental composition
Optical holography	Surface optical properties

328

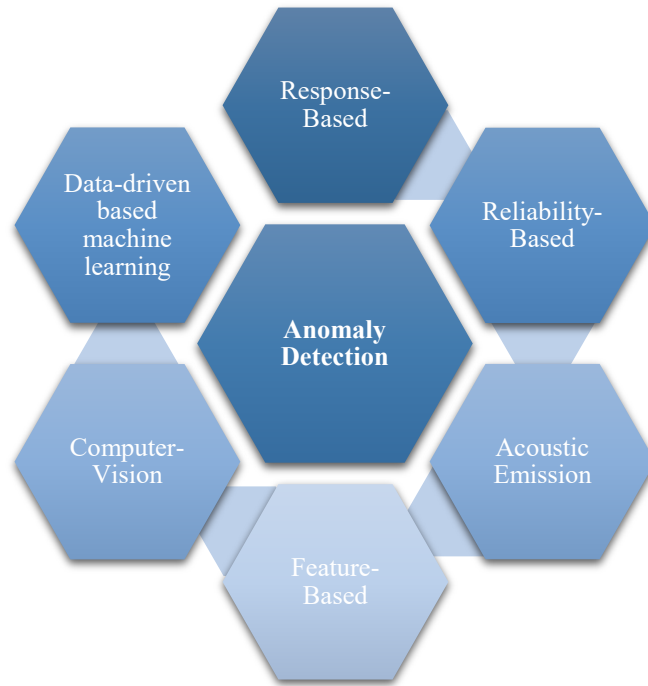


Figure 4 Visual inspection on a bridge girder (64)

329 **5 Anomaly Detection Methods**

330 The SHM literature shows six commonly used structural assessment methods (Figure 5), namely,
331 response-based techniques, reliability-based methods, Acoustic Emission (AE), feature extraction
332 methods, computer vision, and machine learning in data-driven methods. In the following, each
333 technique and its subcategories are described, and relevant papers are reviewed.

334



335

336

Figure 5 Anomaly detection approaches in SHM

337

338 **5.1 Response-Based Techniques**

339 **5.1.1 Displacement-based approach**

340 Measuring static responses is easier and more reliable in comparison with dynamic response
341 measurements. Therefore it is the interest of a large proportion of researchers. For example, Xu et
342 al. (65) deployed non-contact laser displacement sensors to measure dynamic displacements on a
343 frame structure model, searching for baseline states and joint connection defects. They utilized
344 displacement time series with two neural networks to find damage and assess its extent.

345 Huang et al. (66) proposed a displacement-based damage assessment method that utilized nodal
346 displacements on a steel beam that combined analytical and numerical models with some
347 experiments. Their methodology was practical since it required a few sensors, and there was no
348 need to have a baseline condition assessment of the structure.

349 Ono et al. (67) used influence lines of the road to detect damage on a full-scale finite element
350 bridge slab. Different parameters, such as damaged positions and boundary conditions, were
351 examined to investigate their impacts on the performance of the presented methodology.

352 Huseynov et al. (68) studied numerical analysis to find an index on the basis of rotation
353 measurements. To this end, they proposed a sensitive index using the difference in rotation
354 influence lines of damage and healthy states. It was concluded that this parameter could
355 successfully identify damages on an experimental bridge model.

356 **5.1.2 Strain-based approach**

357 Monitoring strain is possible by employing Fiber-optic strain gauges, Fiber Bragg grating (FBG)
358 sensors, and piezoresistive sensors such as microelectromechanical systems (MEMS) (69, 70).
359 Usually, a large number of sensors are needed for measuring strain because the strain is a localized
360 quantity. Thus, piezoelectric polymers, polyvinylidene fluoride (PVDF) patches (71, 72) are more
361 recent tools that are suggested to measure strain (32).

362 Jang et al. (73) employed the damage locating vector (DLV) method with static strain
363 measurements to localize damage on 2D and 3D planar truss models. It was shown that the
364 proposed method required fewer strain sensors without needing to measure the damaged members.
365 In this context, Zhao et al. (74) introduced the basic theory of modal macro strain-based using long
366 gauge distributed sensing technology and deep learning theory for the first time.

367 Rageh et al. (75) utilized strain outputs induced by unknown, nonstationary external inputs on a
368 steel railway bridge. A coupled Proper Orthogonal Modes (POM) and ANN methodology were
369 used to assess stringer–floor beam connection deterioration on the bridge in a noisy environment.

370 **5.1.3 Vibration-based methods**

371 Structures are subjected to a variety of loading types during their lifetime. Forced or ambient
372 vibrations might generate these excitations. Regardless of the type of excitation, when the
373 vibratory motion threshold exceeds a certain level, it might cause damages such as structural
374 fatigue damage, cracks, strength or stiffness degradation, and other types of deformations.
375 Environmental loads may also induce noise, which adversely affects the signals (76). Ambient
376 excitations seem less risky and may not cause severe damage. Furthermore, the evaluation of
377 structural response under ambient excitations is more straightforward.

378 The response of a system is related to its inherent dynamic characteristic, namely inertia (mass),
379 damping, and stiffness. These dynamic characteristics are unique for each structure and can change
380 as a result of damage. Accordingly, any structural damage can be traced and correlated with the
381 subsequent changes in these dynamic structural characteristics (stiffness, mass, or energy
382 dissipation). In that case, changes in natural frequencies, mode shapes, and damping properties
383 inherently related to stiffness, mass, and damping indicate the incurred structural damages (14,
384 77). Vibration-based methods aim to incorporate and integrate the experimental vibration data,
385 e.g., acceleration, velocity, or displacement, with vibration models for damage evaluation and
386 develop damage models for prediction. These models range from pure lumped parameter models
387 to complex finite element models (32).

388 It is important to note that the low-frequency examination carried out by these techniques typically
389 involves the structural components throughout, along with boundary conditions. Consequently,
390 these methodologies usually are considered global diagnostic tools (12). Therefore, they are
391 commonly integrated with the sensitivity of local tools such as Scanning Laser Doppler

392 Vibrometers (SLDVs), guided waves, or Ultrasonic methods with the frequency range of kHz to
393 MHz. A summary review of vibration-based methods can be found in (35, 78, 79). In the following
394 sub-sections, the most commonly used vibration-based, namely Modal Based approaches, are
395 discussed.

396 5.1.3.1 *Natural frequencies*

397 Monitoring changes of natural frequencies was among the earliest work carried out by researchers
398 for damage detection, and numerous attempts have been made in this regard (32). Generally,
399 frequency-based techniques are based on the fact that when a structure undergoes any type of
400 damage, this damage results in a change in the structure's natural frequencies. These approaches
401 are practical and helpful only when a global assessment is needed.

402 Tracing shifts of frequencies cannot provide detailed information about damage characteristics
403 (80, 81). Therefore, techniques solely dependent on changes in frequency are usually limited to
404 the first level of damage identification and, as stated, are considered as global detection methods.
405 What's more, most frequency-based techniques, which can identify and localize defects, are
406 heavily dependent on the existence of a precise FEM model of the actual structure (82).
407 Furthermore, frequency information by itself is not practical since several combinations of damage
408 phenomena, such as cracks in different locations, can produce the same changes in the natural
409 frequencies (20). Hence, the implementation of natural frequencies as the sole technique for
410 anomaly identification can lead to unrealistic damage assessments and evaluations (83).

411 Many researchers have deployed frequency approaches on simple structures like beams or plates
412 (84-88). For instance, Kim et al. (89) compared frequency-based damage detection (FBDD) vs.
413 mode-shape-based damage detection (MBDD) on a simple beam and two sets of modal
414 parameters. They concluded that through FBDD, the damage could be identified with a much
415 smaller error, and by applying the MBDD, the damage could be located more accurately. More
416 recently, Nguyen et al. (90) employed a vector of first few frequencies as the multivariate input of
417 a statistical distance-based damage identification study using experimental data from two real
418 benchmark structures.

419 Mohan et al. (91) designated a frequency change correlation for detecting damage in a cantilever
420 beam. They studied four different damage scenarios and located the corresponding damages by
421 Damage Location Assurance Criterion (DLAC), based on Modal Assurance Criterion (MAC)
422 established by Messina et al. (92). The DLAC measures the correlation of a vector of experimental
423 natural frequency change ratios instead of mode shapes (23). However, few researchers have
424 applied the frequency method to complex structures such as space frame structures (93). In order
425 to cope with the obstacles mentioned above, research studies have exhibited inclinations towards
426 concentrating on the implementation of mode shapes (94-96) and derivatives (97) since changes
427 in these parameters are more sensitive to local damage than changes in natural frequencies (98). A
428 concise review of these methods is noted in (99, 100).

429

430 5.1.3.2 *Mode-shapes*

431 Measuring mode shapes is more laborious than measuring frequencies, and also, a significant
432 number of sensors is required to specify mode shape vectors accurately (101). This technique
433 typically utilizes mode shapes and compares the measured mode shapes either directly or the
434 various features of mode shapes, such as curvature or modal strain energy, to improve the
435 sensitivity (20). The occurrence of singularities in the mode shape due to the existence of defects
436 is the critical factor that reveals damage. In other words, the higher the extent of damage, the more
437 singularities in the mode shape (102).

438 Mode shape methods primarily required both data from the intact and damaged structure. The
439 baseline data is obtained from either an experimental test or a finite element analysis. Broadly,
440 these methods are sensitive only to limited areas within a structure (e.g., mid-span of a clamped
441 beam), and the reported work in this area has been mainly limited to laboratory experiments.
442 Furthermore, reported cases indicate that the approach has been more effective for preliminary
443 damage localization than more accurate localization (103).

444 Nevertheless, recently developed model-based methods have shown promising prospects for either
445 mode shape data or mode shape changes identification of damaged structures. The most popular
446 technique in this regard is MAC (104-107), a statistical index that is more sensitive to substantial
447 variations while relatively insensitive to slight differences in the mode shapes, taking values
448 between 0 (i.e., uncorrelated) and 1 (i.e., perfect correlation). Values larger than 0.9 indicate
449 correspondence, whereas small values signify low similarity between the two shapes. (108). Some
450 of the popular mode shape-based techniques are compiled in (100, 109).

451

452 5.1.3.3 *Modal curvature*

453 Derivatives of mode shapes appear more sensitive to defects since the reduction in stiffness causes
454 an abrupt change in the mode shape's first or second derivatives (slope, curvature, or strain) (25,
455 110). In short, occurrence of damage leads to a decline in stiffness that subsequently causes an
456 increase in curvature. Thus, damage identification is performed by comparing differences in the
457 pre and post-damage curvature mode shapes near the vicinity of the damaged region. This
458 procedure implements multiple modes and is summed up in a damage parameter for a particular
459 location (23).

460 Pandey et al. (111) presented mode shape curvature methods for detecting and localizing damage
461 in a cantilever and a simply supported beam. They employed a central difference estimation to
462 derive the curvature mode shapes from the displacement mode shapes using a numerical equation.
463 It was concluded that changes in the displacement of mode shapes were unable to locate the
464 damage region. In addition, it was proved that MAC and coordinate modal assurance criteria
465 (COMAC) were not sensitive enough for detecting slighter damages.

466 Wahab et al. (112) confirmed that detection is possible using multiple modes in the case of multiple
467 damages. Therefore, they presented the Curvature Damage Factor (CFD), providing clear
468 identification of multiple damages occurring and using classical mode shape curvature obtained
469 from only one mode. They also applied modal curvature techniques to measured data on a concrete

470 bridge and achieved promising results in terms of damage identification and localization. In
471 addition, by using measured data on the aforementioned bridge, it was demonstrated that the modal
472 curvatures of the lower modes were more precise compared to those of the higher ones.

473 Roy and Chaudhuri (113) found that variation in the fundamental mode shape and derivatives were
474 associated with the location of the defect. Thereby, mode shapes might not indicate damage in
475 contrast with mode shape derivatives in some cases. Roy (114) put forward a robust localization
476 technique through the derivatives of mode shapes related to undamaged and damaged states of a
477 structure. He noted that the difference in mode shape slopes resulted in a Dirac delta function for
478 damage location. It was observed that the difference in mode shape curvature was discontinuous
479 at the position of the defect. Accordingly, that approach was effective in identifying and localizing
480 damage due to slight changes despite the existence of noise-contaminated data.

481 Janeliukstis et al.(115) developed a square curvature procedure to measure the damage on pre-
482 stressed railway sleepers. Although their method revealed efficiency in detecting damage on the
483 mid-span of the rail, no accuracy was noted in finding damages on the edges. The effects of
484 environmental conditions, including temperature and humidity, on the dynamic properties (natural
485 frequencies, mode shapes, and mode shape curvature) for a wind turbine blade were investigated
486 by Ou et al. (116). The authors offered thorough documentation regarding the configuration of the
487 experimental benchmark, sensor types, and the nature of excitations.

488 5.1.3.4 Modal strain energy

489 Shi et al. (117) proposed Modal Strain Energy (MSE) in damage localization for the first time.
490 Therein, Modal Strain Energy Change Ratio (MSECR) was established as an indicator of damage
491 location. This approach was verified through a numerical model and an experimental specimen
492 with a two-story portal steel frame. The results revealed that the method was efficient in the single
493 damage quantification with a 7% noise. However, in the case of multiple damages, results were
494 not satisfactory at the same noise level.

495 Cornwell et al. (118) implemented a strain energy approach on a beam and a plate. The authors
496 proposed fractional strain energy for the healthy and damaged beam, which required the structure's
497 mode shapes in damage and baseline condition. Although this approach showed some errors near
498 the nodes, it was advantageous while using ambient excitation. In addition, the algorithm was
499 able to locate even slightly damaged areas employing a few modes. Hu et al. (119) extended the
500 previous work by developing a non-iterative exact solution methodology called cross-modal strain
501 energy (CMSE), which used only a few modes of damaged structure for estimating damage
502 severity. The method was verified on a three-dimensional five-story structure by assessing single-
503 damage and multiple-damage scenarios under an ordinary noise environment. In a recent study,
504 Nguyen et al. (120) proposed a correlation method using change in the ratio of modal strain energy
505 to eigenvalue directly estimated from the experimental modal information, which is powered by a
506 sensitivity-weighted search space scheme incorporated with genetic algorithm to overcome the ill-
507 posed problem that causes false detection errors. The improved method is shown to be effective
508 in locating and assessing damage in a complex steel truss structure.

509 Wahalathantri et al. (121) proposed a modification function according to mode shape curvature,
510 which could enhance the previous approach and qualify damage to some extent. Tan et al. (122)
511 presented a modal strain energy damage index as the input of an Artificial Neural Network (ANN).
512 This method simply used the first mode of vibration and was preferable in detecting, locating, and
513 quantifying single and multiple damage scenarios on steel beams. In an effort to extend to large-
514 scale building structures, Wang et al. (123) proposed a component-based MSE damage index
515 method and combined it with the modal flexibility method to locate damage in three-dimensional
516 asymmetrical building frames. On the side of bridges, Jayasundara et al. (124) studied modified
517 modal flexibility and strain energy indices as the input of an ANN to assess deficiencies on full-
518 scale arch-type bridges. The proposed strategy was promising, even in the presence of noise-
519 contaminated data along with the accumulation of multiple damages. The modified indices are
520 formulated by decomposing the traditional modal flexibility and strain energy into vertical and
521 lateral indices, extracting the larger values for each type and normalizing them to get a fix on the
522 location of the damage very effectively (125).

523 5.1.3.5 Damping

524 Arising damage in a structure can cause an increase in damping. However, this structural
525 characteristic is not sensitive enough to indicate damage. As a case in point, Hearn and Testa (126)
526 explored the use of modal parameters, including frequency, mode shape, and damping values, for
527 detecting damages in a welded steel frame subjected to cyclic load. It was observed that after the
528 accumulation of damage, the damping level might decrease due to cumulative deterioration.

529 Salawu and Williams (127) conducted a full-scale test on a concrete bridge prior to repairing
530 actions. It was demonstrated that the repairs led to a slight change in the natural frequencies, but
531 no identifiable trend could be established in the modal damping ratio.

532 Frizzarin et al. (128) recommended applying the nonlinear damping ratio as a damage index for
533 reinforced concrete structures. By that, they were able to identify anomalies without any reference
534 to the baseline condition. Moreover, they observed a significant correlation between the increase
535 in the nonlinear damping and a decrease in the structural stiffness connected with the escalation in
536 seismic damage intensity.

537 Montalvão et al. (129) developed a modal damping factor to identify delamination on composite
538 materials such as Carbon Fiber Reinforced Plastics (CFRP). This low-cost method required either
539 FEM or experimentally measured mode shapes and presented a geometrical probability definition
540 of the damage vicinity for any bi-dimensional structure. Similar researches on the application of
541 damping ratio as a damage index are compiled in (130, 131).

542 5.1.3.6 Frequency response functions (FRFs)

543 In essence, a frequency response function is defined as a mathematical representation between
544 input and output of a system derived from the Fourier transform (132). Having the general
545 equation of motion, the displacement response in the frequency domain is given by

$$X(\omega) = (-\omega^2 M + j\omega C + K)^{-1} F(\omega) = H_d(\omega) F(\omega) \quad (1)$$

$$\dot{X}(\omega) = \omega X(\omega) = H_v(\omega) F(\omega) \quad (2)$$

$$\ddot{X}(\omega) = -\omega^2 X(\omega) = H_d(\omega)F(\omega) \quad (3)$$

546 where $H_d(\omega)$ indicates the displacement Frequency Response Function (FRF) matrix and $j =$
547 $\sqrt{-1}$ (132). FRFs require installing a smaller number of sensors, and the corresponding
548 measurements efficiently fulfill local detection (133). Among the different dynamic characteristics
549 of the structure, it is relatively easier to obtain the structure's frequency response. Furthermore,
550 since these data can be, for instance, derived from seismic tests on a structure, FRFs express the
551 actual behavior of the structure and can be more reliable. Consequently, different FRF-based
552 damage detection techniques can be obtained using displacement frequency response (DFRF),
553 velocity frequency response (VFRF), or acceleration frequency response (AFRF), as presented by
554 equations (1-3) (134).

555 Esfandiari et al. (135, 136) established an FRF-based parameter assessment approach using
556 incomplete measured responses derived through a quasi-linear sensitivity equation. To cater to this
557 need (employing incomplete measurements in the derivation of the sensitivity equation), they
558 proposed an approximation of the damaged structure's transfer function via the measured
559 frequencies coupled with modal damping ratios of the damaged structure and the analytical mode
560 shapes of the healthy structure. Likewise, numerical simulations were adopted to validate the
561 robustness of the model updating for extended damage scenarios through highly noise-
562 contaminated data. The authors also formulated methodologies in terms of picking subsets of
563 measured responses and suitable weighting of sensitivity equations. Staszewski and Wallace (137)
564 concluded that the wavelet ridge algorithm could effectively derive and visualize data out of
565 wavelet-based FRFs.

566 Bandara et al. (138) used DFRF along with an ANN pattern recognition for localization and
567 quantification of damage in a frame. In that research, the authors deployed a finite element model
568 of a two-story frame structure to train the neural network, which could identify even slight damages
569 with reasonable accuracy under 10% noise. Liu-Sheng and Jun (139) used AFRF for detecting and
570 localization of damage in a planar truss. They demonstrated that the method made accurate
571 predictions about the damaged member but could not exclude the damage probability of
572 circumference members.

573 The accuracy of FRF methods depends on using raw data in measuring frequencies. However, a
574 massive amount of data leads to more significant data processing demands. To deal with this
575 problem, data compressing methods such as fuzzy clustering algorithms or principal component
576 analysis (PCA) could be practical in this scope. Data compression methods can also reduce
577 environmental effects (140, 141). Moreover, in a complex structure, variations in natural
578 frequencies are the same for both damaged and undamaged cases (141). Hence, the solution is
579 reading damage and healthy data simultaneously (142).

580 5.1.3.7 Matrix-based (stiffness and flexibility)

581 Changing the stiffness and flexibility matrices induced by damage and comparing them with the
582 undamaged state devises another damage identification strategy. Zimmerman and Kaouk (143)
583 considered damage as changes in stiffness using an eigenvalue problem derived from a general
584 equation of motion for a finite element model. Sivico et al. (144) proposed a method considering

585 changes in stiffness and damping parameters in the time domain. It was observed that higher modes
586 contribute more than lower ones to the structure stiffness (145, 146). Accordingly, a precise
587 estimation of the stiffness matrix needs to measure all modes of the structure. However, measuring
588 higher frequencies is quite tricky due to the apparent limitations of the experimental apparatus. To
589 this end, the flexibility matrix method was proposed for estimating the changes in system stiffness
590 by means of first mode shapes and modal frequencies, which have the most significant influences
591 on the structure's response (147). In this aspect, Pandey and Biswas (147) developed a novel
592 algorithm that was capable of localizing damage in three types of beams using the first several
593 modes and measuring flexibility changes. Reich and Park (148) utilized strain-based sub-structural
594 flexibility matrices for detecting damage in a reinforced concrete model.

595 Park et al. (149) compared the predicted position of damage obtained via damage index methods
596 with visual inspection results in a reinforced concrete box-girder bridge. They proved that
597 environmental conditions, such as the atmospheric moisture and the dry summer months in the
598 region, could affect the damage index results.

599 Tomaszewska (150) attempted to detect damage on a simple beam and a FEM model of a real-
600 world tower through structural flexibility and mode shape curvature. He tested the modal
601 identification errors by an absolute damage index. It was pointed that ignoring modal errors in the
602 damage detection process could distort results. Additionally, using the flexibility and curvature
603 indices improved the accuracy of detection when erroneous modal data was collected.

604 Grande and Imbimbo (151) put forward a new technique by combining the classical flexibility
605 method and a multi-stage procedure relying on Dempster's rule discussed in (152, 153). That
606 approach was applied to two case studies, including a fixed-end beam and a three-dimensional
607 structure benchmark model. Overall, the method effectively detected damage in both cases, even
608 with a limited number of parameters and noise measurements.

609 Wickramasinghe et al. (154) confirmed the applicability of modal flexibility to detect and locate
610 single, multiple, and complex damage scenarios. The authors developed two damage indices that
611 used only the first four modes to detect defects on a real suspension bridge simulated using a FEM.

612 **5.2 Reliability-based Methods**

613 Engineers have always tended to use SHM for optimizing the cost of maintenance based on the
614 remaining service life of a structure. However, numerous uncertainties exist in current procedures.
615 Thus, to consider these uncertainties, a probabilistic approach, such as reliability-based methods,
616 is used to overcome existing gaps. Many researchers have developed reliability-based methods as
617 a quantitative tool to scan the health state of the structure for deterioration or damage (17, 155-
618 157)

619 Soyoz et al. (158) deployed structural parameters, stiffness, and damping values according to
620 seismic response measurements obtained from shaking table tests as indexes. Some scholars have
621 also introduced a probability-based framework for estimating the performance of the structure.
622 Others developed reliability-based assessment methods using strain-monitoring data to develop
623 deterioration indices (159, 160). Notably, those methods have also been investigated for damage
624 detection in various infrastructures (17, 161-163). Nonetheless, some limitations cast doubts on

625 practical implementation (164). A large number of methods mentioned above that are based on the
626 reliability approach have solely utilized strain as input data (159, 160). Strain measurements have
627 some drawbacks; for instance, they might not be stable, especially over a long time. This approach
628 may also be expensive and require complex signal processing systems (165).

629 In addition, recent studies have revealed that reliability-based procedures are prone to an
630 inaccurate estimation of the structural failure probability due to the sensitivity of the results to the
631 accuracy of the input data and require making assumptions for numerous input parameters (165,
632 166).

633 5.3 Acoustic Emission (AE)

634 Acoustic emission (AE) has been studied as a non-destructive evaluation (NDE) and structural
635 health monitoring method over the last six decades (167). It is defined as propagating transient
636 elastic waves in the materials, which are generally propagated from internal energy sources due to
637 damage initiation (168). The primary components consist of the structure, AE sensors, amplifiers,
638 acquisition, and recording unit coupled with the data processing system (169). Signal
639 characteristics that are commonly utilized include rise time, peak frequency (PF) or average
640 frequency (AF), duration, and ringdown count (4).

641 In practice, AE is helpful for global monitoring, real-time assessment, and remote monitoring to
642 discriminate different sources of damages (170). AE has been deployed broadly to assess fracture
643 mechanisms and characterize structural damages, especially for composite materials and for
644 complex damage mechanisms such as matrix cracking, delamination, fiber fracture, pull-out, and
645 gross material faults (171). Moreover, a large percentage of the papers that have reported this
646 approach concern concrete material and structures (172).

647 Hamdi et al. (173) introduced a real-time method through random AE signals obtained from a
648 static bending test on a cross-ply Glass Fiber Reinforced Plastic (GFRP) composite material. They
649 concluded that the Hilbert–Huang transform (HHT) was efficient for nonstationary AE signals
650 feature extraction. Moreover, instant frequencies could provide applicable descriptors in terms of
651 in-situ health monitoring.

652 Behnia et al. (168) investigated steel fiber reinforced concrete beams under pure torsional loading
653 to find different damage mechanisms, including micro and macro-cracking and fiber tension
654 softening. They introduced an unsupervised pattern recognition approach and a novel technique,
655 referred to as Spatial Intelligent b-value Analysis, to quantify fault levels for each loading state.
656 Some practical reviews regarding AE damage detection are available in (169, 174, 175)

657 5.4 Feature-Based

658 The analysis of measured signals searching to reveal hidden features related to the structure's
659 condition has recently attracted a lot of interest. Signal processing techniques derive features from
660 time, frequency, or time-frequency (176). Some of the most practical tools for extracting
661 information from each domain are presented in the following sub-sections.

662 5.4.1 Time-domain

663 Time series is a statistical tool for creating mathematical models that simulate the dynamic
664 characteristics using measured data, divided into two categories, namely parametric and
665 nonparametric time series. In the first group, the observation is simulated using nonparametric
666 time series such as frequency response function (FRF), binned power spectral density (PSD), etc.
667 In this approach, dynamic variations caused by damage are recognized through changes in
668 statistical parameter characteristics (14). In the second group, the input-output relationship of a
669 system is presented through an Average model with exogenous inputs (ARMAX) with the
670 following equation:

$$671 \quad A(q)y(t) = B(q)u(t) + D(q)\varepsilon(t) \quad (4)$$

672 where $y(t)$ denotes the response of the system to the input excitation $u(t)$ and $\varepsilon(t)$ is the residual
673 term. The terms A , B , and C are the coefficients or parameters in polynomials with the delay
674 operator q . The polynomial order defines the time-series model order, which is an unknown term
675 and is determined through different techniques, namely Akaike's information criterion (AIC),
676 Minimum description length (MDL), Root Mean Squared Error (RMSE), and best model order
677 (BMO) (14)(177). Skewness, crest factor, kurtosis analysis, and RMS amplitudes are some of the
678 popular features that apply to time series (178).

679 In a general sense, changes in a system lead to changes in the coefficients and residuals of the time
680 series, which form the main criteria for damage diagnosis in the parametric time series. Since
681 measuring input vibrations is challenging, and it is costly to apply this approach to real-world
682 structures, output-only time-series, which utilize ambient excitation, are more desirable and
683 practical. Thus, various types of output-only parametric time-series have been established in the
684 realm of SHM, including but not limited to AR, ARMA, Vector Autoregressive (VAR), and Vector
685 Autoregressive Moving Average (VARMA) (14).

686 Monavari et al. (179) proposed a signal-based approach utilizing autoregressive (AR) time-series
687 residuals. In this paper, a novel AR model order estimation algorithm was established that was
688 capable of enhancing the sensitivity of the AR model prediction concerning deterioration. As a
689 result, the authors were successful in qualifying slight changes like deterioration on a high-rise
690 FEM concrete building excited by real ambient excitations. AR model residuals can also be
691 combined with test statistics such as the T -values of statistical hypothesis of chi-square variance
692 test to locate crack-induced deterioration in a complex lab test of a box girder structure (54)

693 Time series is one of the tools implemented in statistical pattern recognition applications for SHM
694 (180). Since the method is based on a partial structural dynamics model, it can identify even a
695 small number of variations (181). As an illustration, Gharehbaghi et al. (55) employed AR time-
696 series along with a robust algorithm that was able to select sensitive uncorrelated features.
697 Afterward, they established a pattern, which they then employed in a super vector machine (SVM)
698 algorithm to classify different deterioration scenarios within an analytical model. Following this
699 approach, they could locate and qualify deterioration under the effect of environmental
700 variabilities, such as high noise and operational errors.

701

702 **5.4.2 Frequency-domain**

703 Fourier spectra, cepstrum analysis, difference frequency analysis, and the high-frequency
704 resonance technique are appropriate tools for damage identification, especially for gear faults and
705 roller bearings (182). Fourier transform (FT) and fast Fourier transform (FFT) are considered the
706 principal anomaly detection concepts. As a case in point, in a study conducted by Melhem and
707 Kim (183), FFT and CWT were compared for detecting damage in real prestressed concrete beams
708 and concrete slabs. Results proved that FFT could identify the progression of damage in the beam
709 but not in the slab. Contrarily, CWT could differentiate the initial and damaged states for both
710 structures.

711 Ngo et al. (184) developed an FFT-based correlation coefficient approach to evaluate damages on
712 a beam and bridge. It was deduced that FFT used fewer calculation steps than FT, and the proposed
713 method could locate structural decline through crosscorrelation matrices.

714 **5.4.3 Time-Frequency domain**

715 The time-frequency presentation of a signal allows for the recognition of transient behaviors
716 induced either by damage (desired) or environmental noise (undesired) overlapping with frequency
717 within the original signal (56). The capability of wavelets through multi-scale analysis of transient
718 events induced by damage (desired) or environmental noise (undesired) generated considerable
719 attention for SHM. In contrast to Fourier Transform, wavelet analysis can describe any type of
720 signal both in time and frequency domain simultaneously, while FT can map a signal from the
721 time domain to the frequency domain. Moreover, through a flexible window location and scale,
722 wavelets can identify abrupt changes due to damage with the aid of zooming and focusing. This
723 can be achieved through multiresolution analysis (MRA) from discrete wavelet transform (DWT)
724 and Wavelet packet transform (WPT) or the wavelet spectra from continuous wavelet transform
725 (CWT) (58, 185).

726 Noori et al. (186) applied data obtained via long-gage FBG strain sensors into a modified wavelet
727 packet energy rate index to quantify damage in a steel bridge under a noisy environment. Zhao et
728 al. (187) used the structural mode shapes extracted from the finite element model of a simply
729 supported reinforced concrete beam that is employed for damage identification using different
730 types of wavelets. They concluded that the maximum curve reaches a peak value at a specific scale
731 for a specific case, based upon which a new mode shape-based algorithm and damage index were
732 proposed for damage identification. Haq et al. (188) investigated the use of DWT and CWT for
733 Fatigue damage mounting and estimating the residual life of RC frames.

734 Huang et al. (189) established a new local and adaptive method for analyzing stationary and
735 nonstationary signals called the Hilbert–Huang transform (HHT). HHT relies on empirical mode
736 decomposition (EMD) and can decompose the original signals into a series of basic functions and
737 almost mono-component called implicit mode functions (IMFs). Through IMFs, one can identify
738 all the instantaneous frequencies, which are then utilized to calculate the Hilbert spectrum and
739 enlighten distinctive chrematistics of the original signal (190). Sanchez et al. used empirical

740 wavelet transform and HHT to calculate the three structures' natural frequencies and damping
741 ratios ([191](#)).

742 Yang et al. ([192](#)) proposed a modified EMD for the identification of modal parameters on a four-
743 story steel frame. AE signals of 3D braiding composite shafts under tensile and torsion were
744 analyzed by HHT in ([193](#)). It was shown that HHT could do modal separation of AE signals to
745 identify matrix damage types on composite materials.

746 Babajanian et al. ([176](#)) analyzed cable-bridge responses and extracted features using STFT. A
747 support vector machine (SVM) and a filter-method approach called 'ReliefF' were used to find the
748 sensitive subset of features for detecting damage.

749

750 **5.5 Computer Vision**

751 Computer vision is a sub-set of artificial intelligence that tries to derive information from digital
752 data, including images or videos, by pairing computers and machines ([194](#)). The ultimate target of
753 this methodology is to automatically convert the image or video data into inferable information
754 ([195](#)). Computer vision consists of a vision system, a computer, and an image processing software
755 platform (see Figure 6) ([196](#)). Vision sensors typically include digital cameras, smartphones,
756 infrared cameras, optical lenses, and laser scanners. In addition, image acquisition utilizes
757 customary cameras, camera tracking vehicles, and robotic systems such as UAVs and drones. In
758 this regard, displacement, temperature field distribution, and superficial defects are the most
759 common data recorded by non-contact vision cameras. The processing unit includes image
760 processing techniques that extract features from digital data. In this regard, various types of low-
761 level and high-level features such as shape, texture lines, pixel intensity are utilized in image
762 processing algorithms.

763 Computer vision is mainly deployed for assessing damages on surfaces and visible parts of
764 structures, including different types of cracks, steel corrosion, or concrete spalling. It consists of
765 two main groups, including image processing-based and deep learning-based approaches. Various
766 image/video processing techniques that use features extracted from acquired images are utilized
767 regarding the first group. These consist of edge detection filters ([197](#), [198](#)), morphological features
768 ([199](#)), and bottom-hat transform ([200](#)). Herein, different machine learning classification methods
769 are used, such as SVMs, Naive-Bayes, and K-Nearest Neighbors (KNN). Moreover, in the case
770 of big data, deep learning techniques can be applied to image features.

771 With respect to the first group, Shan et al. ([201](#)) used two cameras to retrieve coordinates of the
772 crack edge using the Canny-Zernike algorithm. The width of the crack was identified via a minimal
773 edge detection approach. Qiang et al. ([202](#)) proposed an adaptive canny edge detection algorithm
774 for crack identification using a Gauss filter and Otsu method. They segmented cracks from the
775 background by applying an iterative threshold algorithm. Sari et al. ([203](#)) classified and segmented
776 asphalt pavements by deploying the SVM and Otsu methods, respectively. Some of the popular
777 crack detection algorithms are reviewed in ([204](#)).

778 Motion magnification is another trending technique that deploys high-speed cameras to amplify
779 small displacements and lead to model identification in structures. As a case in point, Chen et al.
780 (205) calculated the mode-shaped curvature of a beam to identify damage. Accelerometer and laser
781 vibrometer measurements were deployed for validation of the technique. In a paper by Sarrafi et
782 al. (206), phase-based motion estimation (PME) and video motion magnification were employed
783 to perform operational analysis on a wind turbine blade and extract resonant frequencies and
784 operating deflections. A single camera captured the sequential images, and the MAC criterion
785 detected damage scenarios applied to the blade. It was concluded that the use of phase-based
786 motion could be efficient in a noisy environment. PME was applied on a laboratory and real bridge
787 by Cabo et al. (207). The results indicated that PME had a good performance in comparison to
788 traditional sensing methods (e.g., LVDT). Furthermore, natural frequencies are not enough for
789 classifying damage, and other information regarding mode shapes is required.

790 Regarding the learning-based methods, it should be noted that they have broadly improved the first
791 group's ability via different detection approaches, including image classification, object detection,
792 and semantic segmentation (195). Furthermore, thanks to the rapid developments of technology,
793 graphics processing units (GPUs) paired with Field Programmable Gate Arrays (FPGAs) as fine-
794 grained programmable devices are the most suitable platforms for implementing convolutional
795 neural networks (CNNs) since they offer super performance for the sake of pure computation
796 (194).

797 German et al. (208) proposed a damage index for concrete columns to quantify the damage, such
798 as cracks and spalling, based on computer vision for rapid inspection after earthquakes. Chen et
799 al. (209) used aerial images captured by UAVs to evaluate the degrees of damage to buildings after
800 earthquakes. Various image texture features were used to identify ground targets (building, road,
801 mountain, riverway, and vegetation). An SVM classifier was used to evaluate the extent of the
802 damage, and a new damage degree evaluation (DDE) index to identify the damage potential and
803 intensity of the earthquake was devised..

804 Zhang et al. (210) established a CNN called CrackNet, able to classify different cracks on 3D
805 asphalt surfaces, with the explicit objective of pixel-perfect accuracy. For training, two GPU
806 devices were deployed on 1800 images of asphalts.

807 Liang (211) exploited deep learning and Bayesian optimization by examining a reinforced concrete
808 (RC) bridge after an earthquake on three sequential stages, including the system stage, component
809 stage, and damage localization. Yang et al. (212) deployed thermal imaging to combine a rolling
810 electric heating rod with a horizontal thermal excitation methodology to generate a temperature
811 gradient on the side of the crack. An improved Fast R-CNN was implemented to learn temperature
812 gradient and to detect cracks of different depths on a steel plate.

813 Oudah and El-Hacha (213) conducted damage and deformation evaluation of a large-scale that
814 was tested on two new RC connection systems using digital image correlation (DIC). Ni et al.
815 (214) proposed a deep-learning-enabled data compression and reconstruction framework, divided
816 into two phases: (a) a one-dimensional CNN; (b) a new SHM data compression and reconstruction
817 method based on Autoencoder structure. To validate the approach, acceleration data from the SHM

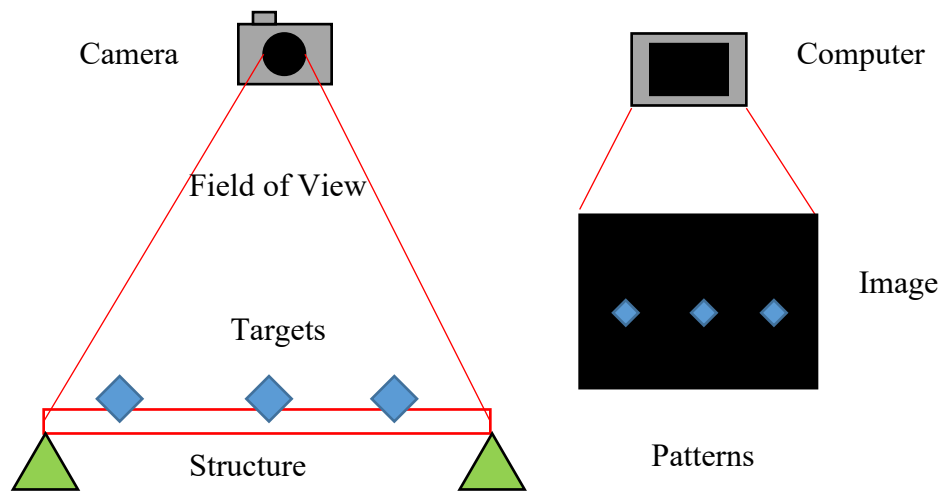
818 system of a long-span bridge in China was employed. In the abnormal data detection phase, the
819 results showed that the proposed method could detect anomalies with high accuracy.

820 Chen and Jahanshahi (215) proposed a method for detecting cracks on the pixel level. In this study,
821 a rotation-invariant fully convolutional network (FCN) called ARF-Crack was established that
822 explicitly used the rotation-invariant characteristic of cracks. The architecture of the FCN named
823 DeepCrack for pixel-level crack detection was adopted and revised where active rotating filters
824 (ARFs) were utilized for encoding the rotation-invariant characteristic into the network.

825 Comprehensive reviews on new advances and computer vision applications for SHM are available
826 in (195, 196).

827

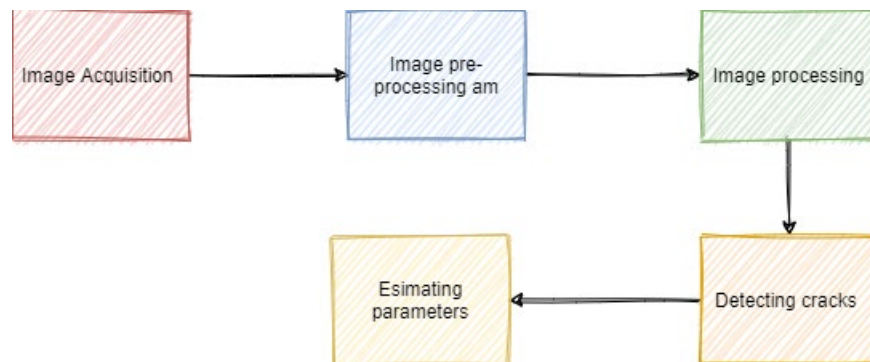
828



829

830

Figure 6 Schematic of computer vision SHM(196)



832

Figure 7 Image processing based architecture (204)

833

834 **5.6 Data-driven based machine learning**

835 As mentioned, signal-based (or data-driven) methods utilize the information obtained from
836 monitored structures in order to reveal features reflecting the state of a system without any
837 knowledge of the physical properties of the structure. These approaches are practical when (216):

- 838 • Sufficient numbers of sensors are available.
- 839 • Computational operations are costly in the SHM project
- 840 • Physical properties of the structure are unknown or complicated to be modeled.

841 It should be noted that methods based on extraction of features can identify damages independently
842 via using different damages indices directly (54, 217-219) or by combining them with machine
843 learning techniques for the purpose of pattern recognition (55). Herein, machine learning methods
844 are applied to the features extracted from measured data to classify and predict the structural
845 patterns obtained from sensors. Supervised, semi-supervised, and unsupervised are the categories
846 for the different learning schemes in this scope. Three major issues are considered in the scope of
847 machine learning, namely classification, regressions, and density estimation (60).

848 Kim and Philen (220) developed a machine learning algorithm called Adaboost that had the
849 potential to identify corrosion and cracks on metals. Four signal processing techniques were
850 examined, and the spectrogram based on short-time Fourier transform was chosen as the reliable
851 damage diagnosis approach. They used the FE model of damages as training samples and
852 examined the performance of the Adaboost on experimental specimens.

853 Three sets of experimental steel pipelines were investigated through 365 features extracted from
854 ultrasonic signals in a study carried out by Ying et al. (221). Two feature selection methods using
855 adaptive boosting algorithms automatically recognized suitable features for damage identification.
856 Five classifications, namely adaptive boosting, modified adaptive boosting, SVM, and two
857 methods combining adaptive boosting and SVMs, showed good performance for determining
858 different damage scenarios.

859 A supervised method based on redundant information of the structure was introduced by Smarsly
860 et al. (216). The algorithm used the inherent correlations among the amplitudes at peaks of the
861 frequency spectra of accelerations from different sensors and deployed an ANN to map the
862 relationship between the modal peak amplitudes of correlated sensors.

863 In a study done by Gui et al. (222), three optimization-based machine learning methods, including
864 grid-search, partial swarm optimization, and the genetic algorithm were used for optimizing the
865 penalty coefficient and kernel function parameter for the SVMs. Two damage features detected
866 the damage scenarios of a scaled metal building model. They concluded that the genetic algorithm
867 had better performance compared to the other optimization techniques. In a more recent study, Yu
868 et al. (223) employed five different machine learning techniques, namely SVM, ANN, adaptive
869 neuro-fuzzy inference system, regression tree model called MSP, and genetic expression
870 programming to quantify Alkali-Silica Reaction (ASR)-induced elastic modulus degradation of
871 unrestrained concrete. The study shows the proposed methods outperform three commonly-used
872 empirical models in a wide range of statistical indices.

873
874

875 Gharehbaghi et al. (55) applied the AR time-series on acceleration signals for extracting sensitive
876 features. In addition, an SVM algorithm was used in order to classify the different conditions of
877 two specimens under environmental variations. The authors extracted features through statistical
878 indices that were applied on coefficients and residuals of AR models then deployed a novel
879 algorithm to find the sensitive features relating to deterioration and damage.

880

881 **6 Popular SHM Benchmarks:**

882 In a broad sense, a laboratory benchmark model provides an experimental study platform to
883 validate the proposed methodology for anomaly detection (224). For expository reasons, SHM
884 benchmark structures are divided into four regions of Europe, North America, East Asia, and
885 Australia in this paper.

886 The majority of research projects in the USA, in this regard, have been supported by National
887 Science Foundation (NSF), the Federal Highway Administration (FHWA), or other universities
888 and laboratories such as LANL (Los Alamos National Laboratory), National Aeronautics, and
889 Space Administration (NASA), United States Air Force (USAF), California Department of
890 Transportation (CALTRANS), and Pacific Earthquake Engineering Research Center (PEER)
891 among others.

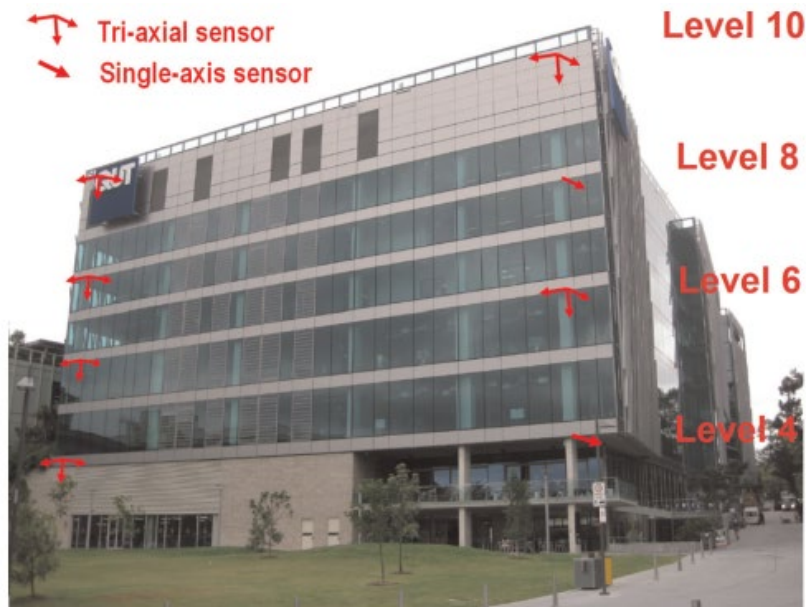
892 In Europe, some collaborative projects on SHM have been organized. For instance, by the Ministry
893 of Scientific Research and Technology (MURST) in Italy, and the Department of Trade and
894 Industry (DTI) and Engineering and Physical Sciences Research Council (EPSRC), in the UK
895 (225). Two primary schemes for cooperative research are the EC Framework Program projects
896 and the EUREKA projects.

897 The Australian Network of Structural Health Monitoring (ANSHM) executes SHM projects in
898 Australia on three projects: ARC Discovery, ARC Linkage, and CRC/CSIRO Projects. In the
899 following sub-section, some of the important benchmark studies conducted around the world are
900 summarized. A comprehensive review of SHM benchmarks is provided in (226).

901 **6.1.1 P-block building**

902 The P-block building is located at the Queensland University of Technology (QUT). It has been
903 recently constructed at the Gardens Point campus of QUT, Australia, costing around AU\$230M.
904 The P-block has been awarded a 5-star Green Star rating from the Green Building Council of
905 Australia (14). This concrete structure has ten floors equipped with accelerometers across four of
906 its six above-ground stories (227). The most important part is that this benchmark utilizes an
907 integrated vibration-sensing concept that has a software-based synchronization method, and it
908 appears to be a promising choice for deployment in vibration monitoring of civil engineering
909 structures.

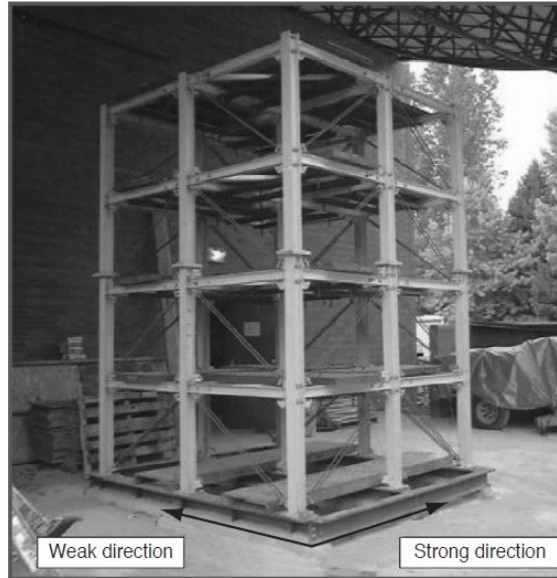
910 On the first instrumented floor of this structure (i.e., level 4), six analog tri-axial sensors coupled
911 with two single-axis accelerometers have been installed to record the vibration signals. As depicted
912 in Figure 8, the sensors are positioned on the upper part of the structure (i.e., at levels 4, 6, 8, and
913 10) that appear to be more sensitive to the ambient vibrations originating from occupants' activities
914 or environmental loads, such as wind load (228). Known as the testbed of Australia's first-ever
915 long-term full-scale SHM system, P block building has interestingly hosted the 8th International
916 Conference on Structural Health Monitoring of Intelligent Infrastructures (SHMII-8) on the first
917 time this prestigious conference in the SHM field was organised in Oceania (229). More details
918 regarding the P-block are presented in (230, 231)



920 Figure 8 P-block building(227)

921 6.1.2 ASCE SHM Benchmark

922 Ventura (232) introduced this 4-story laboratory model at the 15th International Modal Analysis
923 Conference. This structure is placed in the Earthquake Engineering Research Laboratory at the
924 University of British Columbia (UBC) and is 2.5 meters wide and 3.6 meters high. Each level of
925 this structure has two diagonal braces on each exterior face, as shown in Figure 9. The mass of
926 each story is simulated with steel plates of various weights. Some of the braces can be removed to
927 model different damage scenarios, and the connections between columns and beams can be
928 loosened (224).



930

Figure 9 ASCE SHM Benchmark ([224](#))

931 **6.1.3 Bookshelf Frame Structure**

932 The Los Alamos National Laboratory (LANL) has provided some experimental data sets, such as
933 datasets, for bridges and buildings in the public domain ([233](#)). A bookshelf is one of the most
934 popular datasets that is used as a damage detection testbed. This model is a three-story bookshelf
935 with bolted joints and is constructed of metal columns and aluminum floor plates, as depicted in
936 Figure 10 ([233](#)) ([234](#)). Moreover, four isolators allow the structure to sway in horizontal directions
937 with the aid of a hydraulic shaker. Piezoelectric single-axis accelerometers equip the structure.
938 Different damage simulations can be conducted by replacing the masses and changing the stiffness
939 of the columns.

940

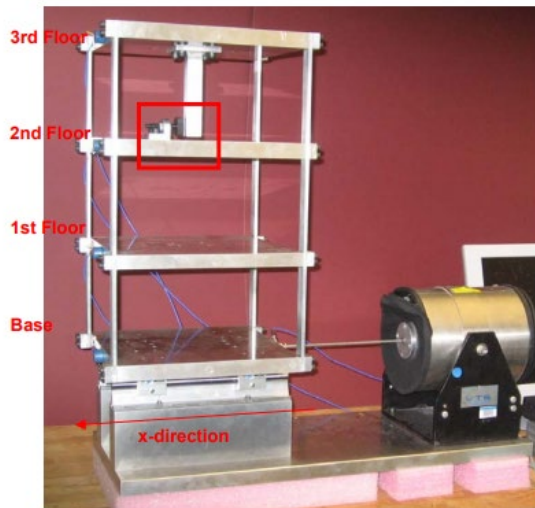


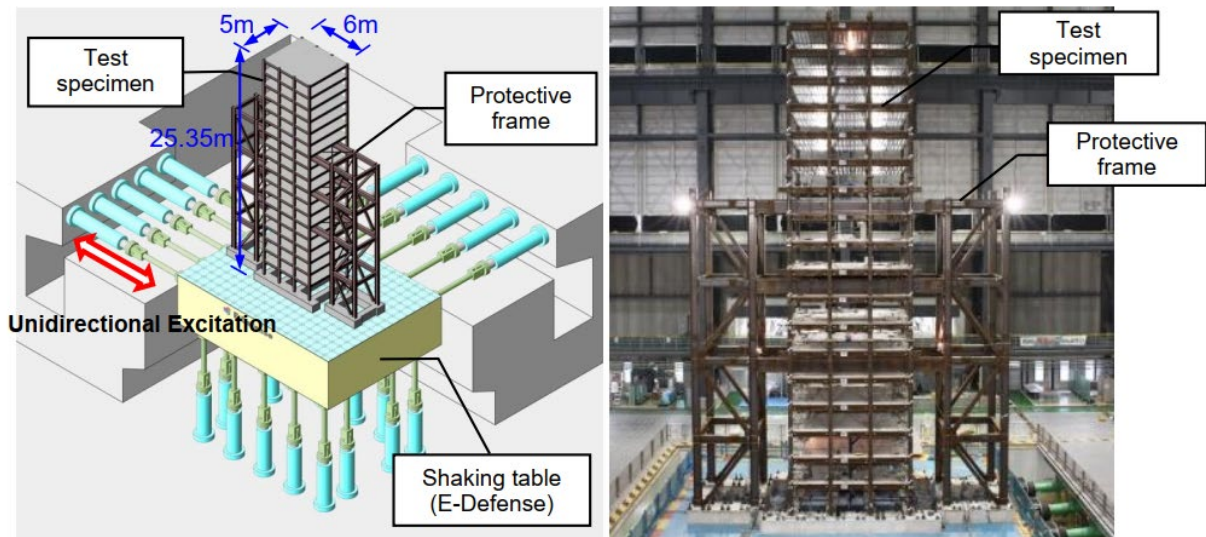
Figure 10 Bookshelf Frame Structure ([233](#))

941

942 **6.1.4 18-Story Steel Moment Frame**

943 A one-third scale model of an 18-story steel high-rise and a protective frame was built and installed
944 on the E-Defense shake table (Figure 11) (235). The model shows the behavior of a typical steel
945 high-rise and responds to the earthquake as a steel moment-resisting frame. The model is similar
946 to steel high-rise buildings constructed in the 1980s to 90s, where the column-to-beam strength
947 ratio of 1.5 is provided to simulate a weak-beam strong-column mechanism. The building can be
948 excited in one direction solely. The input ground excitation is a simulated ground vibration with
949 long-period properties for a Tokai-Tonankai-Nankai subduction-zone earthquake.

950 Moreover, different types of sensors have been installed, and 879 data channels are recorded.
951 Acquired signals of all channels can be obtained for all loading cases, composed of primary
952 earthquake loadings and white-noise vibration. Notably, images from digital cameras record the
953 overall model's condition vividly and the fracture at the beam ends.



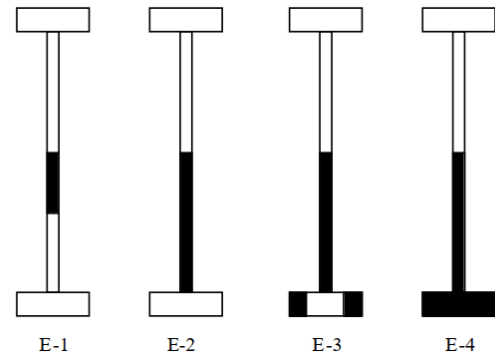
955

Figure 11 18-Story Steel Moment Frame(235)

956

957 **6.1.5 I-40 bridge**

958 This bridge was constructed over a highway in the Rio Grande River in Albuquerque, New Mexico
959 (see Figure 12 a). The concrete deck was about 13.3 m wide and 18 cm thick, supported by two
960 steel plate girders with a 3.05 m height (224). A number of modal tests were conducted after it had
961 been closed in 1993. To this end, 13 accelerometers were installed to each of the two plate girders
962 of the three spans and recorded 26 response measurements. The bridge was excited via a hydraulic
963 actuator placed on the deck of the middle span closest to the abutment. Four levels of damages
964 were introduced so as to simulate fatigue cracking by cutting the web and flange of the girder, as
965 shown in Figure 12 b. More elaborated information on the modal experimental of this bridge is
966 explained in (236).



a) Picture of the bridge

b) damage scenarios

967

Figure 12 I-40 Bridge in New Mexico. (224)

968 6.1.6 Z24 bridge:

969 This bridge was located in Canton Bern, Switzerland, as shown in Figure 13. It was a prestressed
 970 two-span bridged with two lanes and approximately 60m in length (237). In 1998, different
 971 progressive damages scenarios were implemented on this bridge, including settlement of piers,
 972 spalling of concrete, cutting of concrete hinges, landslide, ruptures of tendons, and failure of anchor
 973 bolts. However, the settlement was the central scenario that significantly impacted on the
 974 degradation of bending stiffness. The settlement was simulated by cutting the Koppigen pier and
 975 removing 0.4m of concrete to use six hydraulic jacks. Full details regarding this benchmark are
 976 illustrated in (238)



a) Overall view of the bridge

b) Pier settlement using hydraulic jacks

977

Figure 13 Z24 bridge benchmark (237)

978 6.1.7 Tamar bridge:

979 The bridge is situated in the United Kingdom and used to be one of the longest suspended
 980 structures in England (239) (Figure 14). Firstly, in 1961 the structure had a 335 m span and a side

981 span of 114 m. The anchorage and approach together amount to the total length of 643 m. Two
 982 concrete towers with a height of 73 m support the bridge. After a significant upgrade in the 1990s,
 983 several sensors were installed to assess the bridge's performance. These sensors recorded the data
 984 regarding cable tensions, wind velocity, temperature, and deflections. After years, in 2006, the
 985 engineers from the University of Sheffield installed an additional set of sensors consisting of eight
 986 accelerometers on orthogonal pairs to four cables and three sensors on the deck to extract
 987 vibrational data. The data had a 64 Hz sampling frequency at 10 minutes intervals. More details
 988 about this benchmark are provided in ([240](#)).



Figure 14 The Tamar suspended bridge

989 7 Conclusions

990 This paper has presented a review of the most promising and significant work reported in the
 991 literature regarding SHM and related methodologies developed over the past three decades.
 992 Additionally, a comprehensive categorization for anomaly detection was presented, and related
 993 studies in each subset were summarized and discussed. Moreover, the most widely studied SHM
 994 benchmarks were introduced at the end. The key findings of the literature review regarding the
 995 advantages and disadvantages of each anomaly detection method, as discussed in this paper, are
 996 summarized below:

Method	Pros.	Cons.
Displacement	<ul style="list-style-type: none"> • Detecting damage up to level 3 • Requiring a few sensors 	<ul style="list-style-type: none"> • Insensitive to minor damage • Difficult to measure bridge structures over water using traditional displacement transducers.
Strain	<ul style="list-style-type: none"> • Detecting damage at levels 1 and 2 	<ul style="list-style-type: none"> • Requiring large numbers of sensors

	<ul style="list-style-type: none"> • Capable of detecting damage in the presence of noise 	<ul style="list-style-type: none"> • Strains are not reliable for long periods
Natural Frequencies	<ul style="list-style-type: none"> • Easy implementation • Relatively low cost • Require a limited number of sensors 	<ul style="list-style-type: none"> • Sensitive to noise and vicinity of sensor or actuator • Usually limited to level 1 • Detect severe and single damage only
Mode-Shape	<ul style="list-style-type: none"> • More sensitive to damage than the natural frequency • More effective in noisy environments than frequencies 	<ul style="list-style-type: none"> • Requiring large numbers of sensors • Having errors in locating damages in some areas • Insensitive to minor damage such as concrete cracks
Modal Curvature	<ul style="list-style-type: none"> • Able to detect slight damages 	<ul style="list-style-type: none"> • Requiring many sensors • Existing errors in central difference approximation
MSE	<ul style="list-style-type: none"> • Requiring first few modes • Addresses the levels 2 and 3 damage detection • Detecting multiple damages • Effective in noisy environments 	<ul style="list-style-type: none"> • Accuracy decreases as the mode shape complexity increases
Damping	<ul style="list-style-type: none"> • Relatively low cost 	<ul style="list-style-type: none"> • Having large standard deviations • Can be affected by operational effects • Damping levels may rise or fall depending on the damage
FRF	<ul style="list-style-type: none"> • Easy implementation • Relatively low cost • Multi damage case detection • Efficient in the existence of noise 	<ul style="list-style-type: none"> • Mainly limited to level 2 • Sensitivity to numbers of modes • Sensitivity to frequency ranges
Matrix-based	<ul style="list-style-type: none"> • Addresses the levels 2 and 3 • Requiring few modes • Sensitive to faults through incomplete modal measurements • Sensitive to local defects 	<ul style="list-style-type: none"> • Not sensitive to slight damages • Requiring well-distributed sensors • Requiring mass normalized mode shapes • Affecting the performance by using incomplete modal measurements

		<ul style="list-style-type: none"> • The precision relies on the mode shape data • Requiring higher-order modes for precise damage detection
Reliability	<ul style="list-style-type: none"> • Can be applied to complex structures 	<ul style="list-style-type: none"> • The sensitivity of the results depend on the accuracy of the input data
AE	<ul style="list-style-type: none"> • Practical for complex damage mechanisms like composite materials • Can be deployed for real-time damage detection • Effective for global monitoring • Sensitive to slight damages 	<ul style="list-style-type: none"> • Expensive • Requires skillful operator
Time-domain	<ul style="list-style-type: none"> • Detecting damage at levels 1 and 2 • Capable of detecting damage in the presence of noise • Sensitive to local damage • Not require a solving system of equations in finite element method • Capable of solving complex systems hard to model operating on partial models with a limited number of measurable excitation and/or response signals <ul style="list-style-type: none"> • Identifying dynamic characteristics of a system under ambient vibration • Inherent accounting for uncertainty through statistical tools 	<ul style="list-style-type: none"> • Limit information about the location and severity of damage in the presence of noise • False-positive/negative results
Time-Frequency domain	<ul style="list-style-type: none"> • Effective in noisy environments • Addresses the levels 2 and 3 	<ul style="list-style-type: none"> • Computationally expensive
Computer Vision	<ul style="list-style-type: none"> • Easy implementation • Low cost • Addresses the levels 2 and 3 • Ability to be automated 	<ul style="list-style-type: none"> • Computationally expensive • Images quality degrades by environmental conditions

Data-Driven based Machine learning	<ul style="list-style-type: none">• Ability to be automated• Addresses the levels 2 and 3	<ul style="list-style-type: none">• Computationally expensive

997

998

999 **Compliance with Ethical Standards**

1000 **Conflict of Interest:** On behalf of all authors, the corresponding author states that there is no
1001 conflict of interest.

1002 **Funding:** The authors received no specific funding for this work.

1003

1004

1005

1006

1007

1008

1009

1010

1011

1012

1013

1014

1015

1016

1017

1018

1019

1020

1021

1022 **8 References**

- 1023 1. Inman DJ, Farrar CR, Junior VL, Junior VS. Damage prognosis: for aerospace, civil and
1024 mechanical systems: John Wiley & Sons; 2005.
- 1025 2. Staszewski WJ, Worden K. Signal Processing for Damage Detection. Encyclopedia of
1026 Structural Health Monitoring: John Wiley & Sons, Ltd; 2009.
- 1027 3. Farrar CRaKW. An Introduction to Structural Health Monitoring. Philosophical
1028 Transactions of The Royal Society. 2006:PP 303-15.
- 1029 4. Farrar CR, Worden K. Structural health monitoring: a machine learning perspective: John
1030 Wiley & Sons; 2012.
- 1031 5. Beck, J. L. and Katafygiotis, L. S. Probabilistic System Identification and Health
1032 Monitoring of Structures. Proceedings of the Tenth World Conference on Earthquake Engineering
1033 July 1992, Madrid, Spain.
- 1034 6. Mita A. Emerging Needs in Japan for Health Monitoring Technologies in Civil and
1035 Building Structures. 2nd International Workshop on Structural Health Monitoring, Stanford
1036 University. 1999
- 1037 7. A. Al-Khalidy MN, Z. Hou, R. Carmona, S. Yamamoto, A. Masuda, A. Sone. A study of
1038 health monitoring systems of linear structures using wavelet analysis. ASME J on Pressure Vessels
1039 and Piping. 1997;347:49-58.
- 1040 8. Basu B, Bursi OS, Casciati F, Casciati S, Del Grosso AE, Domaneschi M, et al. A European
1041 Association for the Control of Structures joint perspective. Recent studies in civil structural control
1042 across Europe. Structural Control and Health Monitoring. 2014;21(12):1414-36.
- 1043 9. Aydin E, Ozturk B, Noroozinejad Farsangi E, Bogdanovic A. Editorial: New Trends and
1044 Developments on Structural Control & Health Monitoring. Frontiers in Built Environment.
1045 2020;6(53).
- 1046 10. Speckmann H, Henrich R, editors. Structural health monitoring (SHM)–overview on
1047 technologies under development. Proc of the World Conference on NDT, Montreal-Canada; 2004.
- 1048 11. Amezquita-Sanchez JP, Adeli H. Signal processing techniques for vibration-based health
1049 monitoring of smart structures. Archives of Computational Methods in Engineering. 2016;23(1):1-
1050 15.
- 1051 12. Gopalakrishnan S, Ruzzene M, Hanagud S. Computational techniques for structural health
1052 monitoring: Springer Science & Business Media; 2011.
- 1053 13. Rytter A. Vibrational-based inspection of civil engineering structures. 1993.
- 1054 14. Monavari B. SHM-based Structural Deterioration Assessment [Ph.D. thesis]: Queensland
1055 University of Technology, 2019.
- 1056 15. Nie Z, Hao H, Ma H. Using vibration phase space topology changes for structural damage
1057 detection. Structural Health Monitoring. 2012;11(5):538-57.
- 1058 16. Rodrigues C, Félix C, Lage A, Figueiras J. Development of a long-term monitoring system
1059 based on FBG sensors applied to concrete bridges. Engineering Structures. 2010;32(8):1993-2002.
- 1060 17. Hosser D, Klinzmann C, Schnetgöke R. A framework for reliability-based system
1061 assessment based on structural health monitoring. Structure and Infrastructure Engineering.
1062 2008;4(4):271-85.
- 1063 18. Shih HW, Thambiratnam DP, Chan TH. Vibration based structural damage detection in
1064 flexural members using multi-criteria approach. Journal of Sound and Vibration. 2009;323(3):645-
1065 61.
- 1066 19. Guo T, Li A, Wang H. Influence of ambient temperature on the fatigue damage of welded
1067 bridge decks. International Journal of Fatigue. 2008;30(6):1092-102.

- 1068 20. Karbhari VM, Ansari F. Structural health monitoring of civil infrastructure systems:
1069 Elsevier; 2009.
- 1070 21. Worden K, Dulieu-Barton JM. An overview of intelligent fault detection in systems and
1071 structures. *Structural Health Monitoring*. 2004;3(1):85-98.
- 1072 22. Doebling SW, Farrar CR, Prime MB. A summary review of vibration-based damage
1073 identification methods. *Shock and vibration digest*. 1998;30(2):91-105.
- 1074 23. Shih HW. Damage assessment in structures using vibration characteristics: Queensland
1075 University of Technology; 2009.
- 1076 24. Pawar PM, Ganguli R. Structural health monitoring using genetic fuzzy systems: Springer
1077 Science & Business Media; 2011.
- 1078 25. Chang PC, Flatau A, Liu S. Health monitoring of civil infrastructure. *Structural health
1079 monitoring*. 2003;2(3):257-67.
- 1080 26. Viola E, Bocchini P. Non-destructive parametric system identification and damage
1081 detection in truss structures by static tests. *Structure and Infrastructure Engineering*.
1082 2013;9(5):384-402.
- 1083 27. Ugalde U, Anduaga J, Martinez F, Iturrospe A. A SHM method for detecting damage with
1084 incomplete observations based on VARX modelling and Granger causality. arXiv preprint
1085 arXiv:160200557. 2016.
- 1086 28. Martinez D, O'Brien EJ, Sevillano E, editors. Damage Detection by Drive-by Monitoring
1087 Using the Vertical Displacements of a Bridge. Sixth International Conference on Structural
1088 Engineering, Mechanics and Computation (SEMC 2016), Cape Town, South Africa, 5 to 7
1089 September 2016; 2016: CRC Press (Taylor & Francis).
- 1090 29. Hjelmstad KD, Shin S. Damage detection and assessment of structures from static
1091 response. *Journal of engineering mechanics*. 1997;123(6):568-76.
- 1092 30. Fei C, Wan-cheng Y, Jia-jun S. Damage detection of structures based on static response.
1093 *JOURNAL OF TONGJI UNIVERSITY NATURAL SCIENCE*. 2000;28(1).
- 1094 31. Nichols JM, Todd MD. Nonlinear features for SHM applications. *Encyclopedia of
1095 structural health monitoring*. 2009.
- 1096 32. Haroon M. Free and Forced Vibration Models. *Encyclopedia of Structural Health
1097 Monitoring*.
- 1098 33. Gudmundson P. The dynamic behaviour of slender structures with cross-sectional cracks.
1099 *Journal of the Mechanics and Physics of Solids*. 1983;31(4):329-45.
- 1100 34. Sinou J-J. A review of damage detection and health monitoring of mechanical systems
1101 from changes in the measurement of linear and non-linear vibrations. Nova Science Publishers,
1102 Inc.; 2009.
- 1103 35. Chatzi EN, Papadimitriou C. Identification Methods for Structural Health Monitoring:
1104 Springer; 2016.
- 1105 36. Jaishi B, Ren W-X. Damage detection by finite element model updating using modal
1106 flexibility residual. *Journal of Sound and Vibration*. 2006;290(1):369-87.
- 1107 37. Kim C-W, Kawatani M. Pseudo-static approach for damage identification of bridges based
1108 on coupling vibration with a moving vehicle. *Structure and infrastructure engineering*.
1109 2008;4(5):371-9.
- 1110 38. Moaveni B, Stavridis A, Lombaert G, Conte JP, Shing PB. Finite-element model updating
1111 for assessment of progressive damage in a 3-story infilled RC frame. *Journal of Structural
1112 Engineering*. 2012;139(10):1665-74.

- 1113 39. Weber B, Paultre P. Damage identification in a truss tower by regularized model updating.
1114 Journal of structural engineering. 2009;136(3):307-16.
- 1115 40. Huang Q, Gardoni P, Hurlbauss S. Assessment of modal parameters considering
1116 measurement and modeling errors. Smart Structures and Systems. 2015;15(3):717-33.
- 1117 41. You T, Gardoni P, Hurlbauss S. Iterative damage index method for structural health
1118 monitoring. Structural Monitoring and Maintenance. 2014;1(1):89.
- 1119 42. Gopalakrishnan S, Chakraborty A, Mahapatra DR. Spectral finite element method: wave
1120 propagation, diagnostics and control in anisotropic and inhomogeneous structures: Springer
1121 Science & Business Media; 2007.
- 1122 43. Bodeux J-B, Golinval J-C. Modal identification and damage detection using the data-
1123 driven stochastic subspace and ARMAV methods. Mechanical Systems and Signal Processing.
1124 2003;17(1):83-9.
- 1125 44. Deraemaeker A, Preumont A. Vibration-based damage detection using large array sensors
1126 and spatial filters. Mechanical systems and signal processing. 2006;20(7):1615-30.
- 1127 45. Kumar RP, Oshima T, Mikami S, Miyamori Y, Yamazaki T. Damage identification in a
1128 lightly reinforced concrete beam based on changes in the power spectral density. Structure and
1129 Infrastructure Engineering. 2012;8(8):715-27.
- 1130 46. Ay AM, Wang Y. Structural damage identification based on self-fitting ARMAX model
1131 and multi-sensor data fusion. Structural Health Monitoring. 2014;13(4):445-60.
- 1132 47. Lu Y, Gao F. A novel time-domain auto-regressive model for structural damage diagnosis.
1133 Journal of Sound and Vibration. 2005;283(3):1031-49.
- 1134 48. White J, Adams D, Jata K, editors. Damage Identification in a Sandwich Plate Using the
1135 Method of Virtual Forces. Proceeding of the International Modal Analysis Conference; 2006.
- 1136 49. Giurgiutiu V. Tuned Lamb wave excitation and detection with piezoelectric wafer active
1137 sensors for structural health monitoring. Journal of intelligent material systems and structures.
1138 2005;16(4):291-305.
- 1139 50. Ivanovic SS, Trifunac MD, Todorovska M. Ambient vibration tests of structures-a review.
1140 ISET Journal of Earthquake Technology. 2000;37(4):165-97.
- 1141 51. Lee J, Kim J, Yun C, Yi J, Shim J. Health-monitoring method for bridges under ordinary
1142 traffic loadings. Journal of Sound and Vibration. 2002;257(2):247-64.
- 1143 52. Nguyen V, Dackermann U, Alamdari MM, Li J, Runcie P, editors. Model Updating for
1144 Loading Capacity Estimation of Concrete Structures using Ambient Vibration. International
1145 Symposium Non-Destructive Testing in Civil Engineering (NDT-CE); 2015.
- 1146 53. Perez-Ramirez CA, Amezquita-Sanchez JP, Adeli H, Valtierra-Rodriguez M, Camarena-
1147 Martinez D, Romero-Troncoso RJ. New methodology for modal parameters identification of smart
1148 civil structures using ambient vibrations and synchrosqueezed wavelet transform. Engineering
1149 Applications of Artificial Intelligence. 2016;48:1-12.
- 1150 54. Monavari B, Chan TH, Nguyen A, Thambiratnam DP, Nguyen K-D. Structural
1151 Deterioration Localization Using Enhanced Autoregressive Time-Series Analysis. International
1152 Journal of Structural Stability and Dynamics. 2020;20(10):2042013.
- 1153 55. Gharehbaghi VR, Nguyen A, Farsangi EN, Yang T. Supervised damage and deterioration
1154 detection in building structures using an enhanced autoregressive time-series approach. Journal of
1155 Building Engineering. 2020;30:101292.
- 1156 56. Beale C, Niezrecki C, Inalpolat M. An adaptive wavelet packet denoising algorithm for
1157 enhanced active acoustic damage detection from wind turbine blades. Mechanical Systems and
1158 Signal Processing. 2020;142:106754.

- 1159 57. Nikkhoo A, Karegar H, Karami Mohammadi R, Hajirasouliha I. An acceleration-based
1160 approach for crack localization in beams subjected to moving oscillators. *Journal of Vibration and*
1161 *Control*. 2020;1077546320929821.
- 1162 58. Hou Z, Hera A, Noori M. Wavelet-based techniques for structural health monitoring.
1163 *Health Assessment of Engineered Structures: Bridges, Buildings and Other Infrastructures World*
1164 *Scientific*. 2013:179-202.
- 1165 59. Hillger W. Ultrasonic methods. *Encyclopedia of Structural Health Monitoring*. 2009.
- 1166 60. Gardner P, Fuentes R, Dervilis N, Mineo C, Pierce S, Cross E, et al. Machine learning at
1167 the interface of structural health monitoring and non-destructive evaluation. *Philosophical*
1168 *Transactions of the Royal Society A*. 2020;378(2182):20190581.
- 1169 61. Gangone MV, Whelan MJ, Janoyan KD. Wireless sensing system for bridge condition
1170 assessment and health monitoring. *Smart Sensor Phenomena, Technology, Networks, and*
1171 *Systems*. 2009;7293:72930M1-12.
- 1172 62. Volume AH. 17: Nondestructive evaluation and quality control. ASM International.
1173 1989;795.
- 1174 63. Liang WANG THTC. Review of Vibration-Based Damage Detection and Condition
1175 Assessment of Bridge Structures using Structural Health Monitoring. 2009.
- 1176 64. Washer GA. Developing NDE technologies for infrastructure assessment. *Public Roads*.
1177 2000;63(4).
- 1178 65. Xu B, Song G, Masri SF. Damage detection for a frame structure model using vibration
1179 displacement measurement. *Structural Health Monitoring*. 2012;11(3):281-92.
- 1180 66. Huang T, Chaves-Vargas M, Yang J, Schröder K-U. A baseline-free structural damage
1181 indicator based on node displacement of structural mode shapes. *Journal of Sound and Vibration*.
1182 2018;433:366-84.
- 1183 67. Ono R, Ha TM, Fukada S. Analytical study on damage detection method using
1184 displacement influence lines of road bridge slab. *Journal of Civil Structural Health Monitoring*.
1185 2019;9(4):565-77.
- 1186 68. Huseynov F, Kim C, OBrien E, Brownjohn J, Hester D, Chang K. Bridge damage detection
1187 using rotation measurements—Experimental validation. *Mechanical Systems and Signal*
1188 *Processing*. 2020;135:106380.
- 1189 69. Zhishen Wu JZaMN. *Fiber-Optic Sensors For Infrastructure Health Monitoring, Volume*
1190 *I: Introduction and Fundamental Concepts*: Momentum Press, New York, 2019.
- 1191 70. Zhishen Wu JZaMN. *Fiber-Optic Sensors For Infrastructure Health Monitoring, Volume*
1192 *II Methodology and Case Studies*: Momentum Press, New York; 2019.
- 1193 71. Luo H, Hanagud S. PVDF film sensor and its applications in damage detection. *Journal of*
1194 *Aerospace Engineering*. 1999;12(1):23-30.
- 1195 72. Kim D-H, Kim B, Kang H. Development of a piezoelectric polymer-based sensorized
1196 microgripper for micro-assembly and micromanipulation. *Microsystem Technologies*.
1197 2004;10(4):275-80.
- 1198 73. Jang S, Sim S, Spencer Jr B, editors. Structural damage detection using static strain data.
1199 *Proceedings of the World Forum on Smart Materials and Smart Structures Technology, China;*
1200 *2007*.
- 1201 74. Zhao Y, Noori M, Altabey WA, Ghiasi R, Wu Z. Deep learning-based damage, load and
1202 support identification for a composite pipeline by extracting modal macro strains from dynamic
1203 excitations. *Applied Sciences*. 2018;8(12):2564.

- 1204 75. Rageh A, Linzell DG, Azam SE. Automated, strain-based, output-only bridge damage
1205 detection. *Journal of Civil Structural Health Monitoring*. 2018;8(5):833-46.
- 1206 76. Junior VL, Steffen Jr V, Savi MA. *Dynamics of Smart Systems and Structures*.
- 1207 77. Farrar CR, Duffey T, Cornwell PJ, Doebling SW, editors. *Excitation methods for bridge*
1208 *structures*. Society for Experimental Mechanics, Inc, 17 th International Modal Analysis
1209 Conference; 1999.
- 1210 78. Goyal D, Pabla B. The vibration monitoring methods and signal processing techniques for
1211 structural health monitoring: A review. *Archives of Computational Methods in Engineering*.
1212 2016;23(4):585-94.
- 1213 79. Gomes GF, Mendez YAD, Alexandrino PdSL, da Cunha SS, Ancelotti ACJAoCMiE. A
1214 review of vibration-based inverse methods for damage detection and identification in mechanical
1215 structures using optimization algorithms and ANN. 2018:1-15.
- 1216 80. Karbhari V, Lee L. Vibration-based damage detection techniques for structural health
1217 monitoring of civil infrastructure systems. Chapter 6 in *Structural Health Monitoring of Civil*
1218 *Infrastructure Systems*. 2009:177-212.
- 1219 81. Farrar CR, Doebling SW, Nix DA. Vibration-based structural damage identification.
1220 *Philosophical Transactions of the Royal Society of London A: Mathematical, Physical and*
1221 *Engineering Sciences*. 2001;359(1778):131-49.
- 1222 82. Liang Y, Li D, Song G. Damage Identification of Shear Buildings Using Natural
1223 Frequency-Change Square Ratio Vector Based on Improved Restoring Force Technology. *Earth*
1224 *and Space*. 2016:998.
- 1225 83. Maeck J, De Roeck G, editors. *Damage assessment of a gradually damaged RC beam using*
1226 *dynamic system identification*. Proceedings of the 20th International Modal Analysis Conference
1227 (IMAC-XX)–CD-ROM, Los Angeles, California; 2002.
- 1228 84. Jeong M, Choi JH, Koh BH. Isomap-based damage classification of cantilevered beam
1229 using modal frequency changes. *Structural Control and Health Monitoring*. 2014;21(4):590-602.
- 1230 85. Zhang Z, Shankar K, Morozov EV, Tahtali M. Vibration-based delamination detection in
1231 composite beams through frequency changes. *Journal of Vibration and Control*. 2016;22(2):496-
1232 512.
- 1233 86. Gillich G, Ntakpe J, Abdel Wahab M, Praisach Z, Mimis M, editors. *Damage detection in*
1234 *multi-span beams based on the analysis of frequency changes*. 12th International Conference on
1235 *Damage Assessment of Structures*; 2017: IOP Publishing.
- 1236 87. Wang L, Lie ST, Zhang Y. Damage detection using frequency shift path. *Mechanical*
1237 *Systems and Signal Processing*. 2016;66:298-313.
- 1238 88. Sha G, Radziński M, Cao M, Ostachowicz W. A novel method for single and multiple
1239 damage detection in beams using relative natural frequency changes. *Mechanical Systems and*
1240 *Signal Processing*. 2019;132:335-52.
- 1241 89. Kim J-T, Ryu Y-S, Cho H-M, Stubbs N. Damage identification in beam-type structures:
1242 frequency-based method vs. mode-shape-based method. *Engineering structures*. 2003;25(1):57-
1243 67.
- 1244 90. Nguyen T, Chan TH, Thambiratnam DP. Field validation of controlled Monte Carlo data
1245 generation for statistical damage identification employing Mahalanobis squared distance.
1246 *Structural Health Monitoring*. 2014;13(4):473-88.
- 1247 91. Mohan V, Parivallal S, Kesavan K, Arunsundaram B, Ahmed AF, Ravisankar K. Studies
1248 on damage detection using frequency change correlation approach for health assessment. *Procedia*
1249 *Engineering*. 2014;86:503-10.

- 1250 92. Messina A, Jones I, Williams E, editors. Damage detection and localization using natural
1251 frequency changes. Proceedings of Conference on Identification in Engineering Systems; 1996.
- 1252 93. He K, Zhu W, editors. Structural damage detection using changes in natural frequencies:
1253 theory and applications. Journal of Physics: Conference Series; 2011: IOP Publishing.
- 1254 94. Xia Y, Hao H, Brownjohn JM, Xia PQ. Damage identification of structures with uncertain
1255 frequency and mode shape data. Earthquake engineering & structural dynamics. 2002;31(5):1053-
1256 66.
- 1257 95. Ndambi J-M, Vantomme J, Harri K. Damage assessment in reinforced concrete beams
1258 using eigenfrequencies and mode shape derivatives. Engineering Structures. 2002;24(4):501-15.
- 1259 96. Maia N, Silva J, Almas E, Sampaio R. Damage detection in structures: from mode shape
1260 to frequency response function methods. Mechanical systems and signal processing.
1261 2003;17(3):489-98.
- 1262 97. Ismail Z, Razak HA, Rahman AA. Determination of damage location in RC beams using
1263 mode shape derivatives. Engineering Structures. 2006;28(11):1566-73.
- 1264 98. J.-T. Kim, S. Jung, Y. Lee, J.-W. Yun less. Damage identification in bridges using
1265 vibration-based system identification scheme. SPIE proceedings series; 2000: Society of Photo-
1266 Optical Instrumentation Engineers.
- 1267 99. Salawu O. Detection of structural damage through changes in frequency: a review.
1268 Engineering structures. 1997;19(9):718-23.
- 1269 100. An Y, Chatzi E, Sim SH, Laflamme S, Blachowski B, Ou J. Recent progress and future
1270 trends on damage identification methods for bridge structures. Structural Control and Health
1271 Monitoring. 2019;26(10):e2416.
- 1272 101. Doebling SW, Farrar CR, Prime MB, Shevitz DW. Damage identification and health
1273 monitoring of structural and mechanical systems from changes in their vibration characteristics: a
1274 literature review. 1996.
- 1275 102. Sha G, Radzienski M, Soman R, Cao M, Ostachowicz W, Xu W. Multiple damage
1276 detection in laminated composite beams by data fusion of Teager energy operator-wavelet
1277 transform mode shapes. Composite Structures. 2020;235:111798.
- 1278 103. Fan W, Qiao P. Vibration-based damage identification methods: a review and comparative
1279 study. Structural Health Monitoring. 2011;10(1):83-111.
- 1280 104. Wolff T, Richardson M, editors. Fault detection in structures from changes in their modal
1281 parameters. Proceedings of the 7th international modal analysis conference; 1989.
- 1282 105. West WM. Illustration of the use of modal assurance criterion to detect structural changes
1283 in an orbiter test specimen. 1986.
- 1284 106. Haisty B, Springer W. A general beam element for use in damage assessment of complex
1285 structures. ASME, Transactions, Journal of Vibration, Acoustics, Stress, and Reliability in Design.
1286 1988;110:389-94.
- 1287 107. Marrongelli G, Gentile C, Saisi A, editors. Anomaly Detection Based on Automated OMA
1288 and Mode Shape Changes: Application on a Historic Arch Bridge. International Conference on
1289 Arch Bridges; 2019: Springer.
- 1290 108. Pastor M, Binda M, Harčarik T. Modal assurance criterion. Procedia Engineering.
1291 2012;48:543-8.
- 1292 109. Gandomi A, Sahab M, Rahaei A, Gorji MS. Development in mode shape-based structural
1293 fault identification technique. World Applied Sciences Journal. 2008;5(1):29-38.

- 1294 110. Chance J, Tomlinson G, Worden K, editors. A simplified approach to the numerical and
1295 experimental modeling of the dynamics of a cracked beam. Proceedings of 12th International
1296 Modal Analysis Conference; 1994: Citeseer.
- 1297 111. Pandey A, Biswas M, Samman M. Damage detection from changes in curvature mode
1298 shapes. *Journal of Sound and Vibration*. 1991;145(2):321-32.
- 1299 112. Wahab MA, De Roeck G. Damage detection in bridges using modal curvatures: application
1300 to a real damage scenario. *Journal of Sound and Vibration*. 1999;226(2):217-35.
- 1301 113. Roy K, Ray-Chaudhuri S. Fundamental mode shape and its derivatives in structural
1302 damage localization. *Journal of Sound and Vibration*. 2013;332(21):5584-93.
- 1303 114. Roy K. Structural Damage Identification Using Mode Shape Slope and Curvature. *Journal*
1304 *of Engineering Mechanics*. 2017;143(9):04017110.
- 1305 115. Janeliukstis R, Ručevskis S, Kaewunruen S. Mode shape curvature squares method for
1306 crack detection in railway prestressed concrete sleepers. *Engineering Failure Analysis*.
1307 2019;105:386-401.
- 1308 116. Ou Y, Tatsis KE, Dertimanis VK, Spiridonakos MD, Chatzi EN. Vibration-based
1309 monitoring of a small-scale wind turbine blade under varying climate conditions. Part I: An
1310 experimental benchmark. *Structural Control and Health Monitoring*. 2020:e2660.
- 1311 117. Shi Z, Law S, Zhang L. Structural damage localization from modal strain energy change.
1312 *Journal of Sound and Vibration*. 1998;218(5):825-44.
- 1313 118. Cornwell P, Doebling SW, Farrar CR. Application of the strain energy damage detection
1314 method to plate-like structures. *Journal of Sound and Vibration*. 1999;224(2):359-74.
- 1315 119. James Hu S-L, Wang S, Li H. Cross-modal strain energy method for estimating damage
1316 severity. *Journal of engineering mechanics*. 2006;132(4):429-37.
- 1317 120. Nguyen K-D, Chan TH, Thambiratnam DP, Nguyen A. Damage identification in a
1318 complex truss structure using modal characteristics correlation method and sensitivity-weighted
1319 search space. *Structural Health Monitoring*. 2019;18(1):49-65.
- 1320 121. Wahalathantri BL, Thambiratnam D, Chan TH, Fawzia S, editors. An improved modal
1321 strain energy method for damage assessment. Proceedings of the tenth international conference on
1322 computational structures technology; 2010: Civil-Comp Press.
- 1323 122. Tan ZX, Thambiratnam D, Chan T, Razak HA. Detecting damage in steel beams using
1324 modal strain energy-based damage index and Artificial Neural Network. *Engineering Failure*
1325 *Analysis*. 2017;79:253-62.
- 1326 123. Wang Y, Thambiratnam DP, Chan TH, Nguyen A. Method development of damage
1327 detection in asymmetric buildings. *Journal of Sound and Vibration*. 2018;413:41-56.
- 1328 124. Jayasundara N, Thambiratnam D, Chan T, Nguyen A. Damage detection and quantification
1329 in deck type arch bridges using vibration-based methods and artificial neural networks.
1330 *Engineering Failure Analysis*. 2020;109:104265.
- 1331 125. Jayasundara N, Thambiratnam D, Chan T, Nguyen A. Vibration-based dual-criteria
1332 approach for damage detection in arch bridges. *Structural Health Monitoring*. 2019;18(5-6):2004-
1333 19.
- 1334 126. Hearn G, Testa RB. Modal analysis for damage detection in structures. *Journal of*
1335 *Structural Engineering*. 1991;117(10):3042-63.
- 1336 127. Salawu OS, Williams C. Bridge assessment using forced-vibration testing. *Journal of*
1337 *structural engineering*. 1995;121(2):161-73.

1338 128. Frizzarin M, Feng MQ, Franchetti P, Soyoz S, Modena C. Damage detection based on
1339 damping analysis of ambient vibration data. *Structural Control and Health Monitoring*.
1340 2010;17(4):368-85.

1341 129. Montalvão D, Ribeiro A, Duarte-Silva J. A method for the localization of damage in a
1342 CFRP plate using damping. *Mechanical systems and signal processing*. 2009;23(6):1846-54.

1343 130. Razak HA, Choi F. The effect of corrosion on the natural frequency and modal damping
1344 of reinforced concrete beams. *Engineering Structures*. 2001;23(9):1126-33.

1345 131. Curadelli R, Riera J, Ambrosini D, Amani M. Damage detection by means of structural
1346 damping identification. *Engineering Structures*. 2008;30(12):3497-504.

1347 132. Law S, Li J, Ding Y. Structural response reconstruction with transmissibility concept in
1348 frequency domain. *Mechanical Systems and Signal Processing*. 2011;25(3):952-68.

1349 133. Fang X, Luo H, Tang J. Structural damage detection using neural network with learning
1350 rate improvement. *Computers & structures*. 2005;83(25):2150-61.

1351 134. Cao S, Ouyang H. Robust structural damage detection and localization based on joint
1352 approximate diagonalization technique in frequency domain. *Smart Materials and Structures*.
1353 2016;26(1):015005.

1354 135. Esfandiari A, Bakhtiari-Nejad F, Rahai A, Sanayei M. Structural model updating using
1355 frequency response function and quasi-linear sensitivity equation. *Journal of Sound and Vibration*.
1356 2009;326(3):557-73.

1357 136. Esfandiari A, Sanayei M, Bakhtiari-Nejad F, Rahai A. Finite element model updating using
1358 frequency response function of incomplete strain data. *AIAA journal*. 2010;48(7):1420.

1359 137. Staszewski WJ, Wallace DM. Wavelet-based frequency response function for time-variant
1360 systems—an exploratory study. *Mechanical Systems and Signal Processing*. 2014;47(1):35-49.

1361 138. Bandara RP, Chan TH, Thambiratnam DP. Frequency response function based damage
1362 identification using principal component analysis and pattern recognition technique. *Engineering*
1363 *Structures*. 2014;66:116-28.

1364 139. Jun LL-SaC. Structural Integrated State Evaluation Base on Acceleration Frequency
1365 Response Function. *Journal of Applied Sciences*. 2014;14(2):188-92.

1366 140. Ni Y, Zhou X, Ko J. Experimental investigation of seismic damage identification using
1367 PCA-compressed frequency response functions and neural networks. *Journal of Sound and*
1368 *Vibration*. 2006;290(1):242-63.

1369 141. Yu L, Zhu J-H, Yu L-L. Structural damage detection in a truss bridge model using fuzzy
1370 clustering and measured FRF data reduced by principal component projection. *Advances in*
1371 *Structural Engineering*. 2013;16(1):207-17.

1372 142. Askegaard V, Mossing P. Long term observation of RC-bridge using changes in natural
1373 frequency. *Nordic concrete research*. 1988(7):20-7.

1374 143. Zimmerman DC, Kaouk M. Structural damage detection using a minimum rank update
1375 theory. *TRANSACTIONS-AMERICAN SOCIETY OF MECHANICAL ENGINEERS*
1376 *JOURNAL OF VIBRATION AND ACOUSTICS*. 1994;116:222-.

1377 144. Valentin-Sivico J, Rao VS, Koval LR, editors. Health monitoring of bridgelike structures
1378 using state variable models. *Smart Structures and Materials' 97; 1997: International Society for*
1379 *Optics and Photonics*.

1380 145. LIN C. Location of modeling errors using modal test data. *AIAA journal*. 1990;28(9):1650-
1381 4.

1382 146. Berman A, Flannelly WG. Theory of incomplete models of dynamic structures. *AIAA*
1383 *journal*. 1971;9(8):1481-7.

1384 147. Pandey A, Biswas M. Damage detection in structures using changes in flexibility. *Journal*
1385 *of Sound and Vibration*. 1994;169(1):3-17.

1386 148. Reich GW, Park K, editors. Experimental application of a structural health monitoring
1387 methodology. SPIE's 7th Annual International Symposium on Smart Structures and Materials;
1388 2000: International Society for Optics and Photonics.

1389 149. Park S, Stubbs N, Bolton R, Choi S, Sikorsky C. Field Verification of the Damage Index
1390 Method in a Concrete Box-Girder Bridge via Visual Inspection. *Computer-Aided Civil and*
1391 *Infrastructure Engineering*. 2001;16(1):58-70.

1392 150. Tomaszewska A. Influence of statistical errors on damage detection based on structural
1393 flexibility and mode shape curvature. *Computers & structures*. 2010;88(3-4):154-64.

1394 151. Grande E, Imbimbo M. A multi-stage approach for damage detection in structural systems
1395 based on flexibility. *Mechanical Systems and Signal Processing*. 2016;76:455-75.

1396 152. Sentz K, Ferson S. Combination of evidence in Dempster-Shafer theory: Sandia National
1397 Laboratories Albuquerque; 2002.

1398 153. Shafer G. A (1976) *Mathematical theory of evidence*. Princeton: Princeton University
1399 Press. 1976.

1400 154. Wickramasinghe WR, Thambiratnam DP, Chan TH. Damage detection in a suspension
1401 bridge using modal flexibility method. *Engineering Failure Analysis*. 2020;107:104194.

1402 155. Tatsis K, Chatzi E, Lourens E-M, editors. Reliability prediction of fatigue damage
1403 accumulation on wind turbine support structures. *Proceedings of the 2nd International Conference*
1404 *on Uncertainty Quantification in Computational Sciences and Engineering*; 2017: National
1405 Technical University of Athens (NTUA).

1406 156. Dissanayake P, Karunananda P. Reliability index for structural health monitoring of aging
1407 bridges. *Structural Health Monitoring*. 2008;7(2):175-83.

1408 157. Jamali S, Chan TH, Nguyen A, Thambiratnam DP. Reliability-based load-carrying
1409 capacity assessment of bridges using structural health monitoring and nonlinear analysis.
1410 *Structural Health Monitoring*. 2019;18(1):20-34.

1411 158. Soyoz S, Feng MQ, Shinozuka M. Structural reliability estimation with vibration-based
1412 identified parameters. *Journal of engineering mechanics*. 2009;136(1):100-6.

1413 159. Frangopol DM, A. Strauss, and S. Kim. Bridge reliability assessment based on monitoring.
1414 *Journal of Bridge Engineering*. 2008:258-70.

1415 160. Catbas FN, Susoy M, Frangopol DM. Structural health monitoring and reliability
1416 estimation: Long span truss bridge application with environmental monitoring data. *Engineering*
1417 *Structures*. 2008;30(9):2347-59.

1418 161. Messervey TB, Frangopol DM, Casciati S. Application of the statistics of extremes to the
1419 reliability assessment and performance prediction of monitored highway bridges. *Structure and*
1420 *Infrastructure Engineering*. 2011;7(1-2):87-99.

1421 162. Rafiq MI, Onoufriou T, Chryssanthopoulos M. Sensitivity of uncertainties in performance
1422 prediction of deteriorating concrete structures. *Structure & Infrastructure Engineering*.
1423 2006;2(2):117-30.

1424 163. Peil U, Mehdiانpour M, Frenz M, Scharff R. Life time prediction of old bridges.
1425 *Materialwissenschaft und Werkstofftechnik*. 2005;36(11):715-21.

1426 164. Frangopol DM. Life-cycle performance, management, and optimisation of structural
1427 systems under uncertainty: accomplishments and challenges 1. *Structure and Infrastructure*
1428 *Engineering*. 2011;7(6):389-413.

1429 165. Aktan AE, et al. Development of a model health monitoring guide for major bridges. 2002.

- 1430 166. Gavin HPaSCY. High-order limit state functions in the response surface method for
1431 structural reliability analysis. *Structural Safety*. 2008: 162-79.
- 1432 167. Huang J. Non-destructive evaluation (NDE) of composites: acoustic emission (AE). *Non-*
1433 *Destructive Evaluation (NDE) of Polymer Matrix Composites*; Elsevier; 2013. p. 12-32.
- 1434 168. Behnia A, Chai HK, GhasemiGol M, Sepehrinezhad A, Mousa AA. Advanced damage
1435 detection technique by integration of unsupervised clustering into acoustic emission. *Engineering*
1436 *Fracture Mechanics*. 2019;210:212-27.
- 1437 169. Saeedifar M, Zarouchas D. Damage characterization of laminated composites using
1438 acoustic emission: A review. *Composites Part B: Engineering*. 2020:108039.
- 1439 170. Rizzo P. Sensing solutions for assessing and monitoring underwater systems. *Sensor*
1440 *Technologies for Civil Infrastructures*; Elsevier; 2014. p. 525-49.
- 1441 171. Carlsson L, Crane RL, Uchino K. Test Methods, Nondestructive Evaluation, and Smart
1442 Materials, vol. 5 of *Comprehensive Composite Material*. Elsevier, London, UK; 2006.
- 1443 172. Ida N, Meyendorf N. *Handbook of Advanced Nondestructive Evaluation*; Springer; 2019.
- 1444 173. Hamdi SE, Le Duff A, Simon L, Plantier G, Sourice A, Feuilloy M. Acoustic emission
1445 pattern recognition approach based on Hilbert–Huang transform for structural health monitoring
1446 in polymer-composite materials. *Applied Acoustics*. 2013;74(5):746-57.
- 1447 174. Nair A, Cai C. Acoustic emission monitoring of bridges: Review and case studies.
1448 *Engineering structures*. 2010;32(6):1704-14.
- 1449 175. Huang Z, Huang C, Zhang J, Jiang D, Ju S. Acoustic Emission Technique for Damage
1450 Detection and Failure Process Determination of Fiber-reinforced Polymer Composites: an
1451 Application Review. *Materials Review*. 2018(7):13.
- 1452 176. Babajanian Bisheh H, Ghodrati Amiri G, Nekooei M, Darvishan E. Damage detection of a
1453 cable-stayed bridge using feature extraction and selection methods. *Structure and Infrastructure*
1454 *Engineering*. 2019;15(9):1165-77.
- 1455 177. Monavari B, Chan TH, Nguyen A, Thambiratnam D, editors. Deterioration sensitive
1456 feature using enhanced AR model residuals. *Fourth Conference on Smart Monitoring, Assessment*
1457 *and Rehabilitation of Civil Structures*; 2017.
- 1458 178. Gharehbaghi VR, Farsangi EN, Yang T, Hajirasouliha I, editors. Deterioration and damage
1459 identification in building structures using a novel feature selection method. *Structures*; Elsevier.
- 1460 179. Monavari B, Chan TH, Nguyen A, Thambiratnam DPJJoSS, Dynamics. *Structural*
1461 *Deterioration Detection Using Enhanced Autoregressive Residuals*. 2018;18(12):1850160.
- 1462 180. Gul M, Catbas FN, Georgiopoulos M. Application of pattern recognition techniques to
1463 identify structural change in a laboratory specimen. *Sensors and Smart Structures Technologies*
1464 *for Civil, Mechanical and Aerospace Systems*. 2007:65291N1-N10.
- 1465 181. Das S, Saha P, Patro S. Vibration-based damage detection techniques used for health
1466 monitoring of structures: a review. *Journal of Civil Structural Health Monitoring*. 2016;6(3):477-
1467 507.
- 1468 182. Farrar CR, Duffey TA, Doebling SW, Nix DA. A statistical pattern recognition paradigm
1469 for vibration-based structural health monitoring. *Structural Health Monitoring*. 1999;2000:764-73.
- 1470 183. Melhem H, Kim H. Damage detection in concrete by Fourier and wavelet analyses. *Journal*
1471 *of Engineering Mechanics*. 2003;129(5):571-7.
- 1472 184. Ngo NK, Nguyen TQ, Vu TV, Nguyen-Xuan H. An fast Fourier transform–based
1473 correlation coefficient approach for structural damage diagnosis. *Structural Health Monitoring*.
1474 2020:1475921720949561.

- 1475 185. Asgarian B, Aghaeidoost V, Shokrgozar HRJMS. Damage detection of jacket type offshore
1476 platforms using rate of signal energy using wavelet packet transform. 2016;45:1-21.
- 1477 186. Noori M, Wang H, Altabey WA, Silik AI. A modified wavelet energy rate-based damage
1478 identification method for steel bridges. *Scientia Iranica Transaction B, Mechanical Engineering*.
1479 2018;25(6):3210-30.
- 1480 187. Zhao Y, Noori M, Altabey WA, Beheshti-Aval SB. Mode shape-based damage
1481 identification for a reinforced concrete beam using wavelet coefficient differences and
1482 multiresolution analysis. *Structural Control and Health Monitoring*. 2018;25(1):e2041.
- 1483 188. Haq M, Bhalla S, Naqvi T. Fatigue damage monitoring of reinforced concrete frames using
1484 wavelet transform energy of pzt-based admittance signals. *Measurement*. 2020:108033.
- 1485 189. Huang NE, Shen Z, Long SR, Wu MC, Shih HH, Zheng Q, et al. The empirical mode
1486 decomposition and the Hilbert spectrum for nonlinear and non-stationary time series analysis.
1487 *Proceedings of the Royal Society of London Series A: mathematical, physical and engineering*
1488 *sciences*. 1998;454(1971):903-95.
- 1489 190. Roveri N, Carcaterra A. Damage detection in structures under traveling loads by Hilbert–
1490 Huang transform. *Mechanical Systems and Signal Processing*. 2012;28:128-44.
- 1491 191. Amezcua-Sanchez JP, Park HS, Adeli H. A novel methodology for modal parameters
1492 identification of large smart structures using MUSIC, empirical wavelet transform, and Hilbert
1493 transform. *Engineering Structures*. 2017;147:148-59.
- 1494 192. Yang J, Li P, Yang Y, Xu D. An improved EMD method for modal identification and a
1495 combined static-dynamic method for damage detection. *Journal of Sound and Vibration*.
1496 2018;420:242-60.
- 1497 193. Zhao G, Zhang L, Wang B, Hao W, Luo Y. HHT-based AE characteristics of 3D braiding
1498 composite shafts. *Polymer Testing*. 2019;79:106019.
- 1499 194. Hassaballah M, Awad AI. *Deep Learning in Computer Vision: Principles and Applications*:
1500 CRC Press; 2020.
- 1501 195. Spencer Jr BF, Hoskere V, Narazaki Y. *Advances in computer vision-based civil*
1502 *infrastructure inspection and monitoring*. Engineering. 2019.
- 1503 196. Ye X-W, Dong C, Liu T. A review of machine vision-based structural health monitoring:
1504 methodologies and applications. *Journal of Sensors*. 2016;2016.
- 1505 197. Abdel-Qader I, Abudayyeh O, Kelly ME. Analysis of edge-detection techniques for crack
1506 identification in bridges. *Journal of Computing in Civil Engineering*. 2003;17(4):255-63.
- 1507 198. Nguyen H-N, Kam T-Y, Cheng P-Y. An automatic approach for accurate edge detection
1508 of concrete crack utilizing 2D geometric features of crack. *Journal of Signal Processing Systems*.
1509 2014;77(3):221-40.
- 1510 199. Choi K-Y, Kim S. Morphological analysis and classification of types of surface corrosion
1511 damage by digital image processing. *Corrosion Science*. 2005;47(1):1-15.
- 1512 200. Lyasheva S, Tregubov V, Shleymovich M, editors. *Detection and recognition of pavement*
1513 *cracks based on computer vision technology*. 2019 International Conference on Industrial
1514 Engineering, Applications and Manufacturing (ICIEAM); 2019: IEEE.
- 1515 201. Shan B, Zheng S, Ou J. A stereo vision-based crack width detection approach for concrete
1516 surface assessment. *KSCE Journal of Civil Engineering*. 2016;20(2):803-12.
- 1517 202. Qiang S, Guoying L, Jingqi M, Hongmei Z, editors. *An edge-detection method based on*
1518 *adaptive canny algorithm and iterative segmentation threshold*. 2016 2nd International Conference
1519 *on Control Science and Systems Engineering (ICCSSE)*; 2016: IEEE.

- 1520 203. Sari Y, Prakoso PB, Baskara AR, editors. Road Crack Detection using Support Vector
1521 Machine (SVM) and OTSU Algorithm. 2019 6th International Conference on Electric Vehicular
1522 Technology (ICEVT); 2019: IEEE.
- 1523 204. Mohan A, Poobal S. Crack detection using image processing: A critical review and
1524 analysis. Alexandria Engineering Journal. 2018;57(2):787-98.
- 1525 205. Chen JG, Wadhwa N, Cha Y-J, Durand F, Freeman WT, Buyukozturk O. Structural modal
1526 identification through high speed camera video: Motion magnification. Topics in Modal Analysis
1527 I, Volume 7: Springer; 2014. p. 191-7.
- 1528 206. Sarrafi A, Mao Z, Niezrecki C, Poozesh P. Vibration-based damage detection in wind
1529 turbine blades using Phase-based Motion Estimation and motion magnification. Journal of Sound
1530 and Vibration. 2018;421:300-18.
- 1531 207. do Cabo CT, Valente NA, Mao Z, editors. Motion magnification for optical-based
1532 structural health monitoring. Health Monitoring of Structural and Biological Systems IX; 2020:
1533 International Society for Optics and Photonics.
- 1534 208. German S, Jeon J-S, Zhu Z, Bearman C, Brilakis I, DesRoches R, et al. Machine vision-
1535 enhanced postearthquake inspection. Journal of Computing in Civil Engineering. 2013;27(6):622-
1536 34.
- 1537 209. Chen J, Liu H, Zheng J, Lv M, Yan B, Hu X, et al. Damage degree evaluation of earthquake
1538 area using UAV aerial image. International Journal of Aerospace Engineering. 2016;2016.
- 1539 210. Zhang A, Wang KC, Li B, Yang E, Dai X, Peng Y, et al. Automated pixel-level pavement
1540 crack detection on 3D asphalt surfaces using a deep-learning network. Computer-Aided Civil and
1541 Infrastructure Engineering. 2017;32(10):805-19.
- 1542 211. Liang X. Image-based post-disaster inspection of reinforced concrete bridge systems using
1543 deep learning with Bayesian optimization. Computer-Aided Civil and Infrastructure Engineering.
1544 2019;34(5):415-30.
- 1545 212. Yang J, Wang W, Lin G, Li Q, Sun Y, Sun Y. Infrared Thermal Imaging-Based Crack
1546 Detection Using Deep Learning. IEEE Access. 2019;7:182060-77.
- 1547 213. Oudah F, El-Hacha R. Damage and deformation assessment of earthquake-resistant RC
1548 slotted beam-column connections using digital image correlation technique. Engineering
1549 Structures. 2020;215:110442.
- 1550 214. Ni F, Zhang J, Noori MN. Deep learning for data anomaly detection and data compression
1551 of a long-span suspension bridge. Computer-Aided Civil and Infrastructure Engineering.
1552 2020;35(7):685-700.
- 1553 215. Chen F-C, Jahanshahi MR. ARF-Crack: rotation invariant deep fully convolutional
1554 network for pixel-level crack detection. Machine Vision and Applications. 2020;31(6):1-12.
- 1555 216. Smarsly K, Dragos K, Wiggenbrock J, editors. Machine learning techniques for structural
1556 health monitoring. Proceedings of the 8th European Workshop on Structural Health Monitoring
1557 (EWSHM 2016), Bilbao, Spain; 2016.
- 1558 217. Monavari B, Chan T, Nguyen A, Thambiratnam D, editors. Time-series coefficient-based
1559 deterioration detection algorithm. Proceedings of the 8th International Conference on Structural
1560 Health Monitoring of Intelligent Infrastructure (SHMII 2017); 2018: Curran Associates, Inc.
- 1561 218. Bogoevska S, Chatzi E, Dumova-Jovanoska E, Höffer R. Data-driven structural health
1562 monitoring and diagnosis of operating wind turbines. 2019.
- 1563 219. Limongelli MP, Chatzi E, Döhler M, Lombaert G, Reynders E, editors. Towards extraction
1564 of vibration-based damage indicators 2016.

1565 220. Kim D, Philen M, editors. Damage classification using Adaboost machine learning for
1566 structural health monitoring. Sensors and Smart Structures Technologies for Civil, Mechanical,
1567 and Aerospace Systems 2011; 2011: International Society for Optics and Photonics.

1568 221. Ying Y, Garrett Jr JH, Oppenheim IJ, Soibelman L, Harley JB, Shi J, et al. Toward data-
1569 driven structural health monitoring: application of machine learning and signal processing to
1570 damage detection. Journal of Computing in Civil Engineering. 2013;27(6):667-80.

1571 222. Gui G, Pan H, Lin Z, Li Y, Yuan Z. Data-driven support vector machine with optimization
1572 techniques for structural health monitoring and damage detection. KSCE Journal of Civil
1573 Engineering. 2017;21(2):523-34.

1574 223. Yu Y, Nguyen TN, Li J, Sanchez LF, Nguyen A. Predicting elastic modulus degradation
1575 of alkali-silica reaction affected concrete using soft computing techniques: A comparative study.
1576 Construction and Building Materials. 2021;274:122024.

1577 224. Zhou L, Yan G, Wang L, Ou J. Review of benchmark studies and guidelines for structural
1578 health monitoring. Advances in Structural Engineering. 2013;16(7):1187-206.

1579 225. Foote P. Structural health monitoring: tales from Europe. Structural Health Monitoring.
1580 2000:24-35.

1581 226. Van der Auweraer H, Peeters B. International research projects on structural health
1582 monitoring: an overview. Structural Health Monitoring. 2003;2(4):341-58.

1583 227. Nguyen T, Chan TH, Thambiratnam DP, King L. Development of a cost-effective and
1584 flexible vibration DAQ system for long-term continuous structural health monitoring. Mechanical
1585 Systems and Signal Processing. 2015;64:313-24.

1586 228. Nguyen A, Kodikara KTL, Chan TH, Thambiratnam DP. Deterioration assessment of
1587 buildings using an improved hybrid model updating approach and long-term health monitoring
1588 data. Structural Health Monitoring. 2019;18(1):5-19.

1589 229. Nguyen A, Chan TH, Zhu X. real-world application of SHM in Australia. Sage
1590 Publications Sage UK: London, England; 2019.

1591 230. Kodikara KTL, Chan TH, Nguyen A, Thambiratnam DP. Model updating incorporating
1592 measured response uncertainties and confidence levels of tuning parameters. International Journal
1593 of Lifecycle Performance Engineering. 2016;2(1-2):61-78.

1594 231. Nguyen A, Kodikara K, Chan T, Thambiratnam D. Toward effective structural
1595 identification of medium-rise building structures. Journal of Civil Structural Health Monitoring.
1596 2018;8(1):63-75.

1597 232. Ventura C, Priori H, Black C, Rezai K M, Latendresse V, editors. Modal properties of a
1598 steel frame used for seismic evaluation studies. Proceedings of SPIE, the International Society for
1599 Optical Engineering; 1997: Society of Photo-Optical Instrumentation Engineers.

1600 233. Los Alamos National Laboratory Available from: www.lanl.gov

1601 234. Figueiredo E, Park G, Figueiras J, Farrar C, Worden KJLANL, Los Alamos, NM, Report
1602 No. LA-14393. Structural health monitoring algorithm comparisons using standard data sets. 2009.

1603 235. Kubota J, Suzuki Y, Suita K, Sawamoto Y, Kiyokawa T, Koshika N, et al. Experimental
1604 study on the collapse process of an 18-story high-rise steel building based on the large-scale
1605 shaking table test.

1606 236. Farrar CR, Baker W, Bell T, Cone K, Darling T, Duffey T, et al. Dynamic characterization
1607 and damage detection in the I-40 bridge over the Rio Grande. Los Alamos National Lab., NM
1608 (United States); 1994.

1609 237. Maeck J, De Roeck G. Description of Z24 benchmark. Mechanical Systems and Signal
1610 Processing. 2003;17(1):127-31.

1611 238. Krämer C, De Smet C, De Roeck G, editors. Z24 bridge damage detection tests. IMAC 17,
1612 the International Modal Analysis Conference; 1999: Society of Photo-optical Instrumentation
1613 Engineers.

1614 239. Dervilis N, Worden K, Cross E. On robust regression analysis as a means of exploring
1615 environmental and operational conditions for SHM data. *Journal of Sound and Vibration*.
1616 2015;347:279-96.

1617 240. Cross E, Koo K, Brownjohn J, Worden K. Long-term monitoring and data analysis of the
1618 Tamar Bridge. *Mechanical Systems and Signal Processing*. 2013;35(1-2):16-34.

1619