A review of shear/slip sensor for improving robotic and human dexterity

Yuting Zhu 1, Tim Giffney2

- Department of Engineering Science, University of Auckland, New Zealand; <u>y.zhu@auckland.ac.nz</u>
- Department of Mechanical Engineering, University of Canterbury, New Zealand; tim.giffney@canterbury.ac.nz

Abstract

The ability to mimic the tactile feedback of the human hand to improve its dexterity, grasp/gripping and manipulation has been widely considered in robotic development. During robotic grasping, three forces are produced: grasp force (pressure), friction force, and tangential force (shear). Most of the tactile sensors are focused on pressure and normal force. However, shear stress is of great importance in manipulation for the prediction of gripping slippage and the implementation of force control. Improved measurement of shear stress can facilitate robots that mimic human-like robot gripping techniques and achieve advanced manipulation tasks. This paper reviews the state-of-the-art of shear/slip sensors for improving robotic and human dexterity. Tactile shear sensors for robotics and biomedical are reviewed, with an analytical comparison of the advantages and disadvantages of different sensing technologies.

Keywords: tactile sensor, shear stress, robotic, gripping.

1 Introduction

Tactile sensors have been developed and widely used in the past few decades in robotics and biomedical fields. For a robot to pick up an object, we need to indicate to the robot what force should apply, and how much force it needs to apply so it can prevent slippage and breaking. In general, three types of forces are produced during gripping: grasp force (pressure), friction force, and tangential force (shear). Shear stress is one of the important factors to prevent slip which can help robots and humans to improve their dexterity, grasp/gripping, and manipulation so that human and robotic devices can function effectively.

Most of the tactile sensors are focused on pressure and normal force. Less attention has been given to direct measurement of shear (tangential) force, which is nevertheless important for applications such as determining if a gripped object will slip or not. Shear force is one of the most common physical forces encountered in everyday life; with shear foce measurements being useful for varied applications ranging from allowing clinicians to monitor foot ulcers to detecting slippage during grasping and manipulation of objects. However, most of current tactile sensors are not capable of shear force measurements.

It is relatively easy for a human to pick up an egg without breaking or dropping it because humans have sensory (haptic) feedback to predict the grip force to grasp an object. However, without the shear sensing information, robots and biomedical surgical devices [1] may only have poor dexterity, which results in many complicating problems, e.g., the incorrect application of contact force resulting in damage to an object or dropping it. Researchers learned that shear measurements have an important role to play in biomedical fields and robotics for gripping objects [2]-[5], thus, many studies have tried to integrate shear sensing into tactile sensors [6]-[10]. However, many tactile sensors only offered normal force measurements and only a few of them have offered shear (tangential) force measurement [11][12].

This review begins with an overview of the need for tactile shear sensing used in robotics and biomedical fields. Next, we describe the importance of shear sensing in tactile sensing development, and also the present state of tactile shear sensors, including different types of tactile shear sensors and their advantages and disadvantages. Finally, we summarise work done in current research in the area of shear sensing and the areas that can be improved.

2 Tactile sensing with shear measurement

Over the past few decades, many researchers have focussed on developing tactile sensors to improve robotics grasping and manipulation capability[13]-[18]. Also, there has been a growing interest in the development of soft robotic devices for interfacing soft tissue or handling delicate objects [19]-[22]. However, the tactile sensors with shear measurement are still immature products[23][24], and have not yet achieved widespread commercial use in robotics.

Tactile feedback information and the exactness of force are important factors to provide the action of perception in biomedical equipment. Using tactile sensors to acquire kinaesthetic (forces) and tactile information as haptic perception is very useful for surgeons. In general, tactile sensors could provide contact force measurements, besides the contact forces (shear force and normal force) measurements are very helpful for clinical diagnoses, such as diabetic foot ulcer[25][26], as well as minimally invasive surgery [27].

In recent years, surgical equipment developers have begun to employ tactile sensing as part of the surgery system. Using tactile sensors during surgical operations, surgeons can find out the operating position and exact force to apply [28]. Several studies have tried to intergrade shear sensing into tactile sensors. Currently, most tactile sensors only offer normal force measurement and only a few of them are compatible with the measurement of shear (tangential) force [11][12][29][30]. Most shear sensors currently measure parallel shear (sliding force) with limited accuracy[31] and limited reliability[32], which means that current shear sensor products available are limited in flexibility[33], reliability[34] and are also costly[35].Innitial examples of commercial sensors include the shear sensor system from Tactilus® [36]and an in-shoe based foot plantar pressure sensor F-Scan® System[37] by Tekscan. However, the precision of tactile sensor measurements that use in biomedical fields is still unsatisfactory[38]. Due to the inaccuracies of shear measurements, tactile sensors are still not used widely in many clinics, such as diabetic clinics[39].

Alvares et al.[40] reports that many tactile shear sensors have been developed and used in the architectural area, but only a few in robotic and biomedical areas. Although many tactile sensors developed and used in robotic and biomedical fields[1][41] in recent years, most of them measure normal force and not many of them recognise measure shear (tangential) force[42].

As these have received comparatively little attention relative to tactile sensors with shear sensing capability that is used in robotics and biomedical fields [31]. Therefore, there would be some gaps for tactile shear sensing to be developed widely to use in robotic and biomedical fields.

2.1 Motivation for Tactile Shear/Slip sensing

During any object manipulation and grasping, a variety of forces are produced, which gives tactile information. When we pick up an object, to prevent slippage, we need to know the normal force and shear force during grasping [43]. For humanoid devices to work well, they need to have sensory (haptic) feedback like us, which should include normal force and shear force [41]. Normal force and shear force are part of the ensemble of tactile (sensing), helping to prevent slippage, as well as improving understanding of how to interact with a real-world object. Alongside this, there is a growing interest in the development of soft robotic devices that interface soft tissue or handle delicate objects. Examples include fruit sorting robotics [44] through to surgical robots such as The Da Vinci robot [45].

Researchers often employ tactile sensors to measure the tactile perception of the sense of touch. Particularly when grasping an object, this tactile sensibility is essential [46][47][48]. This typically involves pressure sensing. Currently, there is a growing awareness of the need to combine pressure sensing with shear sensing [43][49][50]. Pressure and shear force measurements applications as diverse as help to achieve stable grasps [51], also help to predict and prevent diabetic foot ulcers [52][53].

Shear force measurement is an important factor in many fields, such as humanoid robots and biomedical fields. For example, scientists and clinicians believe the shear stress acting on the shoe sole could be the main cause of certain kinds of foot disease, therefore accurate shear measurements in the insole can help clinicians to monitor diabetes patients with foot ulcers [25][54]-[56]. As well, many studies have focused on developing tactile shear sensors for use in rehabilitation and prosthetics [57][58] for affected patients. Accurate shear measurements in an 'active' sole would enable clinicians to monitor these complications [56]. The shear force also should not be neglected to detect slippage during grasping and manipulation, as well as shear measurement could be useful for improving tactile exploration that is used in robotic hands and biomedical equipment. Many studies show that shear measurement is a very important factor, and is very useful for robotics manipulation as well as use for biomedical devices [20][59][60].

Shear sensing technology has progressed in the biomedical field[60]-[62], but the accuracy of shear measurement requires improvement, especially for the measurement of distributed shear over small areas[31]. Most available shear sensors only measure parallel shear with limited accuracy [58][63], and some of the shear sensors are either rigid[64][65] cannot stretch, or are very bulky in size[66][67]. Also, shear data is not readily obtained, and also lacks validation [34][68]. Therefore, it is still necessary to develop a flexible shear sensor that has greater stretchability, three-dimensional measurement capabilities, improved reliability, and accuracy.

For this reason, tactile shear sensing has received much attention due to shear measurement offering important benefits in robotic and biomedical fields in recent years. Many researchers have named tactile shear sensing as well as tactile tangential sensing. To understand tactile shear sensors, we first need to understand what is shear or tangential stress.

2.2 Tactile Shear Sensor Theory

Stresses involve and occur in most of our daily activities. It includes normal and shear stresses, which refer to the local normal or tangential force divided by the surface area of application of the force. Shear stress incules parallel shear stress(tangential force induced sheat stress) and pinch shear stress (normal force gradient induced shear stress), whereas normal stress is the forces perpendicular to a cross-sectional area of the material[69]. The two forces in opposite directions is called parallel shear; if two different amounts of forces acting in the same direction is the pinch shear. Thus, those stresses are commonly been defined as the normal force (pressure) and shear forces (tangential). Moreover, the shear stresses could likely be high if pressures are high. [69].

Therefore, when the shear stress causes the object to change shape (deform), that results from a force parallel (tangential) to the surface of an object. This shear stress τ can express as [70]:

$$\tau = \frac{F}{A} \tag{1}$$

where F is tangential force applied (N); A is area of application of force (m²).

Shear stress exists when there is sliding between two surfaces and this is related to friction [34][69]. For solid surfaces which are often referred to Amontons' law, the coefficient of friction μ can express as [71][72]:

$$\mu = \frac{F}{W} = \frac{A}{W} \cdot \tau \tag{2}$$

where F is the ratio of the tangential force / is the tangential force needed to initiate motion;

W is the normal force/ load force.

It is extremely hard to measure shear accurately [56], so to get an accurate shear measurement, the first step requires an understanding of the definition and the relationship between shear and pressure. Huston et al. [73] conclude that normal stress means the force is directed normal to the area, but if the force is directed tangent (parallel) to the cross section which is called shear force, and the corresponding stress is called shear stress, illustrated in Figure 1.

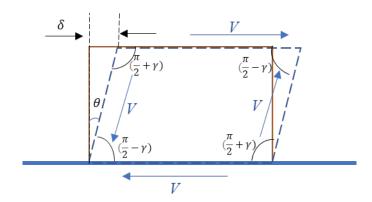


Figure 1: Relationship between normal force and shear stress interpretation: where V is the shearing force, δ is small displacement, γ is the shear strain, and θ is the distortion angle

Shear occurs when two forces are in opposing directions (Figure 1) [69]. Medical interest in shear stress is in the measurement scales for diabetic ulcers, which is one of the factors that may trigger foot ulcers [34]. The current market has a variety of sensors to measure the shear force [34]. However, many existing shear sensors lack a validated and commercially available because shear data is not obtained[68], and for this reason, many clinicians prefer not to use existing shear sensors as a diagnostic tool [74].

Shear or tangential stress also will occur while manipulating and grasping an object. The friction force is the resistive shear or tangential force that acts directly opposite to the direction

of motion [75]. The adhesion mechanism is described as a relationship between the frictional forces (F), the interfacial shear (τ) stress, and the real contact area (A) [76] as:

$$F = \tau A \tag{3}$$

The shear stress can be influenced by contact pressure and sliding velocity, furthermore, it depends on sensor materials and environmental factors such as temperature and humidity [77]. Many studies show that shear measurement is a very important factor, and is very useful for robotics manipulation as well as used for biomedical devices [59][60].

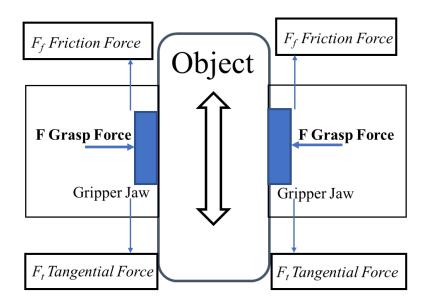


Figure 2: Forces produced during object gripping: which involve Grasp force (Pressure), Friction force, and

Tangential Force (Shear)

Detecting slippage during grasping and manipulation through shear measurement should be able to improve tactile exploration in robotic hands and biomedical equipment. During gripping, the shear stress is where a deforming force is applied parallel to surface as shown in Figure 2.

Balasubramanian et al.[78] point out that shear (tangential) forces also relate to haptic perception, as the perception of shear forces can help to prevent slippage, however, there is a challenge to measuring those shear forces. When a hand picks up an object, there are two acting forces which are normal force (contact) and shear (tangential) force (sliding) [79]. An object's surface difference (i.e. roughness, hardness, softness, etc.) can influence the relationship between grip force and shear force [80] during grasping, that detects pressure and shear through fingers. Napier et al. [81] report that humans can achieve stability for any grasping action by the power grip and the precision grip. Figure 3 illustrates the difference between the power grip and the precision grip. When the object is held and pressure being applied by the thumb lying

more or less in the palm plane is the power grip; while the object is pinched between the flexor aspects of the fingers and the opposing thumb, that is the precision grip. [81]. The relative force direction between hand and object depends on the posture of grasping [82]. Furthermore, Siciliano et al.[83] has summarized tactile sensing in robotics into three functional categories: manipulation, exploration, and reaction/haptics. So that we can take advantage of robotic tactile sensing by understanding human manipulation characteristics. Haptic [78] gives sensations such as stiffness, texture, and weight when touching/ grasping an object. Therefore, understanding human manipulation characteristics can help us to take advantage of the influence of the ability to distinguish objects for robotic tactile sensing.

- 1) Manipulation [78][84] -- grasp force control; contact locations and kinematics; stability assessment
- 2) Exploration [78][83] -- surface texture, friction, and hardness; thermal properties; local features
- 3) Reaction or haptics [78][85] -- detection and reaction to contacts from external agents.



Figure 3: Power grip and precision grip posture; the power grip involves an extensive area of contact between the hand and the object; the precicion grip is opposition pinch that pinched between the flexor aspects of the fingers and the opposing thumb.

Accordingly, for a robot to pick up a fragile object such as an egg without breaking or dropping it, it needs to satisfy two requirements:

- The need to prevent slippage during manipulation (slippage prevention)
- The need to prevent breakage during manipulation (adequate grasp force)

In summary, a tactile shear sensor would be very useful in many areas, including measuring human-produced forces in biomedical devices and developing humanoid robots.

2.2.1 The shear measurement used in robotic and biomedical fields

As the normal force and the static coefficient of friction are related to shear force, to get accurate force measurements one should not only use pressure sensors but also sensors that can measure shear force [86]. Most pressure sensors can only measure normal force, but not shear force. An object's surface difference can influence the relationship between grip force and shear force [80].

In current years, there is a growing awareness of the need to combine pressure sensing with shear sensing [49][87][88]. Robotic systems have been developed for many decades, to be as flexible as humans, but still have a long way to go, such as the sense of touch, for the robotic hardly to have the same sensing feedback as a human, tactile replication still expects to develop. The accuracy of manipulation for robot still need to improve. There still is a challenge for robots to handle objects safely on contact and static force [89].

2.3 Tactile shear sensing techniques

In recent years, many types of flexible tactile shear sensors have been developed. Those tactile sensors have been fabricated in many different ways for many different kinds of functional measurements. Researchers have worked on many technologies to develop tactile sensors, and tactile sensing technologies have been well developed in many areas. There are many synthetic approaches on fabricate the tactile sensor, and the most common tactile shear sensors used in robotic and biomedical fields are including capacitive sensors [90]–[92][93][94][95], piezoresistive sensors [96][97][98], piezoelectric sensors [30][99][100], optical sensors [12][88][101] and multi-component tactile sensors [63], etc. The benefits and drawbacks of these techniques have been stated below. Many tactile shear sensors have been developed in recent years [5][7][102][103], but in addition to improving to the accuracy of the shear force measurement, researchers are still working on improving the sensors' accuracy, robustness as well as low cost, and easy fabrication.

2.3.1 Piezocapacitive/Capacitive tactile shear/slip sensor

There are various ways to fabricate capacitive sensors for measuring shear force. Capacitive sensing is one of the most commonly used methods in tactile sensing development. The reason

for that is capacitive sensors have high sensitivity, low power consumption, low-temperature sensitivity, high spatial resolution, good frequency response, and long-term drift stability and immunity to thermal noise [104][102]. Because of these advantages, capacitive sensors have been widely used nowadays to use for tactile sensing and shear measurements [32][94][105]–[108].

There are many designs of fabricated capacitive shear sensor [4][17][61][87][92][109]-[113]. One example is the sensor of Cheng et al.[114] used 2 x 2 array that the top electrode with each bottom electrode forms a capacitor; when the top electrode moves relative to the bottom electrodes in the overlap area, the four capacitances change. Lee et al.[115] used a similar working principle of four top electrodes and four bottom electrodes.

The electroactive polymer dielectric elastomer (DE) is commonly used to achieve wearable capacitive tactile shear sensors that are flexible and stretchable. Some capacitive tactile shear sensors have been presented in recent years, but the accuracy of the shear measurement is still not satisfactory due to the level of noise continues to be an issue during measurement and crosstalk issues [11][17].

2.3.2 Piezoresistive tactile shear/slip sensor

Piezoresistive is one of the common techniques that have been used in tactile shear sensing [97][98][116]–[118], which changes the resistance during a mechanical stimulus is applied. Piezoresistive tactile sensors have the advantages of low cost, low noise, and good sensitivity, but the limitation of low-frequency response, poor stability, and large hysteresis effect which is not helpful for tactile shear sensors [119].

Kappassov et al.[49] reports that some of the piezoresistive tactile sensors are fragile to shear force. Implementations of piezoresistive and Quantum Tunnel Composite(QTC) sensors suffer sensitivity decreases due to wear and tear through usage as they are not flexible as human skin and cannot cover the space between the links for closing the finger of robot hands [120]. Shi et al. [121] developed a piezoresistive normal and shear force sensor using liquid metal alloy which aims to improve the flexibility and durability of the force sensor but has wiring issues. Jung et al.[97] has developed a piezoresistive type tactile sensor that can measure the shear force, however, the shear force measurement is not accurate, as the normal force interferes with the shear force. Noda et al. [98] believe their piezoresistive sensor sensitivity can be improved by changing the elastic material, which can reduce the error of the shear force measurement.

However, Wen et al. [122] have pointed out that there is no straightforward way to determine the shear force using the conventional piezoresistive sensor.

2.3.3 Piezoelectric tactile shear/slip sensor

The piezoelectric property of Polyvinylidene Fluoride (PVDF) was found by Kawai et al.[123] in 1969. Piezoelectric tactile sensors are effect by the pressure change with stain/ stress polarization [64][100][124]. Xin et al.[67] concludes that the piezoelectric property of polymer polyvinylidene fluoride (PVDF) tactile sensors has the advantages of low permittivity, wide frequency response, good sensitivity, high dynamic range, flexibility, and lightweight. Therefore, it has also been commonly used in tactile sensor development.

Choi et al.[125] claims that their PVDF tactile sensor can detect contact force and slippage, which only measure the normal forces. Moreover, the research Dargahi et al. [126] completed was based on piezoelectric tactile sensors with shear force (detacting slippery) measurements. However, the measurement was unreliable, also piezoelectric sensing could be more difficult in low frequency applications.

2.3.4 Optical tactile shear/slip sensor

Optical sensors are based on optical reflection between media of different refractive indexes. Optical tactile sensors have also been used for shear force measurements, as have been reported in [12][23][60][127]–[130].

Lincoln et al. [60] developed a 3D force optical sensor for shear measurement, but it can only measure the parallel shear with unsatisfied error rates, and also very high error rates in normal force measurement.

The optical sensor gives a far-reaching recurrence reaction and also requires significant processing power, but the size of the sensor and its unbending nature become the major disadvantages of optical sensors [131]-[133].

2.3.5 Other technologies

There are also many other ways to make shear tactile sensors. Such as, Chuang et al.[134] study where they used angle detection for shear measurement, but the work they have done still has alignment challenges. Zhang et al.[112] found a new way to develop a flexible three-axis tactile sensing array sensor by using Quantum Tunnelling Composite (QTC). Johansson et al.[135] has developed multi-modal tactile sensors; Accounting Tjin's article [136], has talk about the fiber Bragg grating (FBG) that was first discussed by Hill in 1978, and which Tjin used the

FBGs to develop a new type of shear force sensor, however, the shear force measurement was unsatisfactory.

2.3.6 Tactile Sensing Array

The most common sensing array techniques used in tactile sensing are Capacitive sensing arrays and resistive sensing arrays.

Wang et al. [103] have developed an 8x8 capacitive tactile sensor array with a spatial resolution of 1.6mm for grasping force measurement, however, this work has given an unsatisfactory and inaccurate measurement of shear force. Also, other work that Wang et.al [24] have done shows that the capacitive sensor array has limited spatial resolution, measurement range, and a slow response time.

Table 1: a list of some example shear sensor technologies developed, with a summary of the advantages and disadvantages; also includes sensor size, resolution, force ranges, sensitivity, and structures of the most common sensor types.

Method	Advantages	Disadvantages	Sensor size /Resolution/Force	Structures
			Range/Sensitivity	
Capacitive [32][94] [103]	high sensitivities, low	Dynamic and	20pF, 14N, 2.8x10 ⁻⁴ kPa ⁻¹ [32];	Polyethylene terephthalate (PET)
[105]-[107][115] [134]	power consumption,	creep responses,	0.05N, 10N [94];	and polydimethylsiloxane
[137]	low temperature		62mm X 62mm, 8 X 8,	(PDMS) with an inkjet-printed
	sensitivity, high		0.49%/mN, 0.50%/mN,	bump [137]; PET substrate with
	spatial resolution,		0.32%/mN[103];	PDMS[134]; PDMS with an air
	good frequency		3 X 3 X 2(mm ³) 2.02pF/N,	gap and a pillar[115]; Cross-
	response, long term		0.472pF/N, 0.496 pF/N [106];	section, multi-element structure
	drift stability,		4X4 array, 1.67%/mN [107];	liquid-based PDMS [106];
	immunity to thermal		8X8 array, 10mN-131kPa,	Parallel-plate capacitor with
	noise		2.5%/mN, 3.0%/mN, 2.9%/mN	Kelvin guarding that consists of
			[115];	two electrode arrays (reference
			9 X 9(mm ²), 0.85pF/N(range),	array and sampling array)[94];
			4.43pF/N [137]	capacitive sensors with a four
				MEMS linear array[138]; four
				sensing capacitors separated by a
				wall structure[139];

Piezoelectric (PVDF)	Low permittivity,	External noise	0.003N with sampling rate	Sandwiched between four square-
[7][51][64][67][100][124]	wide frequency	issue when the	50Hz, 8.2mm/s, 10N/mm,	shaped upper electrodes and one
	response,	applied force is	15.5N [51];	square-shaped lower
	biocompatibility	small	1.5N, 14.93pC/N, 14.92pC/N,	electrode[100];
			6.62pC/N [100];	Sandwiched between two elastic
			3cmX3cm, 49.8kPa,	layers fied to a rigid
			(12.6±0.8)mV/N,	foundation[64]
			(223.9±20.3)mV/N,	
			(55.2±11.9)mV/N[124]	
Piezoresistive	Small cross-talk, low	Fragility and	2 X 2 array, 15mm X 15mm X	Piezoresistors sensor chip
[97][98][104] [116]–[118]	cost, low noise, and	rigidity,	5mm, 12.9kPa, 0.165k.Pa ⁻¹ ,	composed of three pairs of silicon
[140] [141]	good sensitivity,	Temperature	0.0173k.Pa ⁻¹ [97];	beams[117]; Five basic sensing
		sensitivity,	20 X 20 (mm ²), 5.0kPa, 1.30 X	elements (one for normal force
		high-precision	10 ⁻³ kPa ⁻¹ , 0.06 X 10 ⁻³ kPa ⁻¹ [98];	and four for shear force
		limitation,	2.0mm X 2.0mm X 0.3mm,	measurement), each of them with
		limitation of low-	100kPa, 4.5X10 ⁻⁵ (kPa ⁻¹) [116];	two flexible composite films
		frequency	11mm X 11mm X 2mm [117];	interlocking each other[97]; using
		response	300μm X 300μm,	cantilevers embedded with a
			26mV/(V.kPa)[141];	liquid-filled elastomer[142]
			10 X 10(mm ²), 25kPa, 8.3 X 10 ⁻	
			⁷ Pa ⁻¹ , 4.0 X 10 ⁻⁸ Pa ⁻¹ [142]	

Optical	Low profile,	noise ratio, bulky.	3.2mm X 1.7mm X	Used LED-phototransistor
[12][23][60][127][143]	physically robust,		1.1mm(small size), 15.7	couples base with a deformable
	good spatial		mV/kPa, 19.4 mV/kPa,	elastic layer[143]; incorporates a
	resolution, sensitivity		0.96mV/kPa [60];	mesh by using crisscrossing
			2X2 matrix array,	waveguides with tactile sensor
			950X950μm ² , 0.1N (resolution)	array, injection molding with
			[127];	(PDMS) as the optical
			11.4mm X 11.4mm, 40N[143]	medium.[127] Using four gaskets
				of soft fiber optic sensor[110]
Others		Repeatability and	7 mm X 7 mm X 0.52 mm, 29.8	a pyramid-plug with different
[102][112][135][144][145]		limited time	nF N ⁻¹ [102]; 2 X 6 cell array,	types of external mechanical
		performance	20N,0.47 V/N, 0.45 V/N, and	loadings[145]
			0.16 V/N[112]; 0.01 pF/mN,	
			7.37 pF/N and 7.1 pF/N without	
			driving voltage, 0.016 pF/mN,	
			10.1 pF/N and 9.3 pF/N with 60	
			volts driving voltage[144];	
			1.93 kPa ⁻¹ , 29.88 N ⁻¹ , 3.39 (N	
			$(cm)^{-1}$,50kPa[145]	

3 Conclusions

In recent years, tactile shear/slip sensing technology has progressed in biomedical fields [2][9][40][54][61][145], most of the tactile sensors used in robotic and biomedical fields with shear measurement function only measure parallel shear with limited accuracy, and shear data is not readily obtained, also the lack of a validated and commercially available shear strain sensor [34][68]. Moreover, the accuracy of shear measurement is still unsolved as yet.

In clinical trials, shear stress and strain have been mentioned many times, and shear measurement has received much attention in the biomedical field. Shear sensors are attracting widespread interest in fields such as the prevention of diabetic foot ulcers [146], stroke retraining for grip capacity, mainstream soft-robotic applications, etc. However, shear stress is notoriously hard to measure [56], and researchers do not always agree on how to define shear. There are many questions and concerns about the accuracy of shear measurements. Therefore, there should be greater consideration of the different ways in which shear stress operates and how this should be measured in a clinical setting.

There are many tactile sensors have been developed in the past four decades; since the 1980s many researchers have been working on tactile shear (tangential) sensing and it has been developed in many different technologies [102][103], but due to the accuracy of the shear measurement, researchers still working on improving the response time [102], the sensors accuracy, robust, low cost and easy fabrication. Moreover, traditional tactile sensing has not paid much attention to shear measurements and also lacks sensitivity, dynamic range, and metrical strength [147].

Although much work has been done to date, to develop a human-like tactile shear sensory system, more studies need to be focused on [104][148][149]:

- The ability to give humanoid devices the "sense of touch"
- Providing humanoid devices with the ability to manipulate delicate objects
- Enabling the optimisation of grippers for low-power operation by minimizing the grasping force
- Collecting data using the most sensitive and repeatable tactile sensors for robotic applications

As well as to investigate:

- ➤ Novel ways to fabricate shear sensors
- > The accuracy of shear measurement

According to these findings, tactile shear sensing research should work to develop an appropriate shear sensor that could resolve the concerns about the accuracy and how to solve the shear methods of the current shear sensors. This should include the capability of mimicking the human sense of touch, and also the sensor should be flexible, has a greater stretchability, and has three-dimensional measurement capabilities, with improved reliability, and accuracy. For any new development, tactile shear force sensors require high sensitivity under small external forces and have a large measurement range on how to improve the accuracy of shear force measurement, flexibility, and fabrication. It also should consider the complex ways in which shear stress operates and then consider the requirements that a sensor would need to meet to measure this variety of shear stress.

Shear stress and strain have been mentioned many times in Clinical trials. There continue to be many questions and concerns about the accuracy of shear measurements. Existing techniques have produced a wide range of stress sensors with some accuracy of measurement in parallel measurement, but this has not considered other shear stress other than parallel. (E.g. measurements of pinch shear) When drawing down to the definition of shear stress, most engineers have considered parallel shear stress. Up to the present day, the most widely used discussions of shear stress documented appear to consider only parallel shear stress. The identification of other forms of shear stress, such as pinch stress or punch stress is rarely considered or mentioned in the documentation available.

However, shear stress should include more than just parallel shear stress, but should also consider 'pinch shear' and other conditions of stress in the measurements. Therefore, there should be greater consideration of the different ways in which shear stress operates and how this should be measured in a clinical setting.

Future shear sensing research may focus on developing an appropriate shear sensor that could resolve the concerns about the accuracy and how to solve the shear methods of the current shear sensors.

Reference:

- [1] M. H. Lee, "Tactile sensing: new directions, new challenges," *The International Journal of Robotics Research*, vol. 19, no. 7, pp. 636–643, 2000.
- [2] P. Laszczak, M. Mcgrath, J. Tang, J. Gao, L. Jiang, D. Bader, D. Moser, and S. Zahedi, "A pressure and shear sensor system for stress measurement at lower limb residuum/socket interface," *Medical engineering* \& physics, vol. 38, no. 7, pp. 695–700, 2016.
- [3] F. Akhlaghi and M. G. Pepper, "In-shoe biaxial shear force measurement: the Kent shear system.," *Med Biol Eng Comput*, vol. 34, no. 4, pp. 315–7, 1996.
- [4] M. I. Tiwana, A. Shashank, S. J. Redmond, and N. H. Lovell, "Characterization of a capacitive tactile shear sensor for application in robotic and upper limb prostheses," *Sensors and Actuators A: physical*, vol. 165, no. 2, pp. 164–172, 2011.
- [5] G. Wolterink, R. Sanders, and G. Krijnen, "A flexible, three material, 3D-printed, shear force sensor for use on finger tips," in *2019 IEEE SENSORS*, 2019, pp. 1–4.
- [6] Y.-H. Gao, Y.-H. Jen, R. Chen, K. Aw, D. Yamane, and C.-Y. Lo, "Five-fold sensitivity enhancement in a capacitive tactile sensor by reducing material and structural rigidity," *Sensors and Actuators A: Physical*, vol. 293, pp. 167–177, 2019.
- [7] F. Li, Y. Akiyama, X. Wan, S. Okamoto, and Y. Yamada, "Built-in Sensor System for Monitoring Internal Shear Strain and Stress Distribution in Soft Materials," *IEEE Access*, vol. 10, pp. 319–327, 2021.
- [8] N. A. Dvo\vrák and P.-C. Ku, "Low-Profile Shear Force Tactile Sensor Based on Optical Methods," *IEEE Electron Device Letters*, 2022.
- [9] H. Oh, G.-C. Yi, M. Yip, and S. A. Dayeh, "Scalable tactile sensor arrays on flexible substrates with high spatiotemporal resolution enabling slip and grip for closed-loop robotics," *Science advances*, vol. 6, no. 46, p. eabd7795, 2020.
- [10] Y. Wang, X. Wu, D. Mei, L. Zhu, and J. Chen, "Flexible tactile sensor array for distributed tactile sensing and slip detection in robotic hand grasping," *Sensors and Actuators A: Physical*, vol. 297, p. 111512, 2019.
- [11] S. Somlor, A. Schmitz, R. S. Hartanto, and S. Sugano, "First Results of Tilted Capacitive Sensors to Detect Shear Force," *Procedia Computer Science*, vol. 76, pp. 101–106, 2015.
- [12] J. Missinne, E. Bosman, B. Van Hoe, R. Verplancke, G. Van Steenberge, S. Kalathimekkad, P. Van Daele, and J. Vanfleteren, "Ultra thin optical tactile shear sensor," *Procedia Engineering*, vol. 25, pp. 1393–1396, 2011.
- [13] M. Kim, J. Yang, D. Yun, and D. Kim, "Soft tactile sensor to detect the slip of a Robotic hand," *Measurement*, p. 111615, 2022.

- [14] T. M. Huh, H. Choi, S. Willcox, S. Moon, and M. R. Cutkosky, "Dynamically reconfigurable tactile sensor for robotic manipulation," *IEEE Robotics and Automation Letters*, vol. 5, no. 2, pp. 2562–2569, 2020.
- [15] Y. Zhu, A. Tairych, S. Rosset, and I. A. Anderson, "An approach to validate the design and fabrication of dielectric elastomer tactile sensor," in *Electroactive Polymer Actuators and Devices (EAPAD) XXI*, 2019, vol. 10966, p. 109662F.
- [16] E.-S. Hwang, J. Seo, and Y.-J. Kim, "A polymer-based flexible tactile sensor for both normal and shear load detections and its application for robotics," *Journal of microelectromechanical systems*, vol. 16, no. 3, pp. 556–563, 2007.
- [17] A. Shashank, M. I. Tiwana, S. J. Redmond, and N. H. Lovell, "Design, simulation and fabrication of a low cost capacitive tactile shear sensor for a robotic hand.," *Conf Proc IEEE Eng Med Biol Soc*, vol. 2009, pp. 4132–5, 2009.
- [18] H. Devaraj, T. Giffney, A. Petit, M. Assadian, and K. Aw, "The development of highly flexible stretch sensors for a robotic hand," *Robotics*, vol. 7, no. 3, p. 54, 2018.
- [19] E. Battaglia, M. Bianchi, A. Altobelli, G. Grioli, M. G. Catalano, A. Serio, M. Santello, and A. Bicchi, "ThimbleSense: a fingertip-wearable tactile sensor for grasp analysis," *IEEE transactions on haptics*, vol. 9, no. 1, pp. 121–133, 2016.
- [20] G. Zhou, Z. Liao, R. Zhao, H. Yao, and H. Dai, "A Force Decoupling Method for Simultaneously Measuring Vertical and Shear Force," *IEEE Sensors Journal*, 2022.
- [21] P. Gil, C. M. Mateo, A. Delgado, and F. Torres, "Visual/Tactile sensing to monitor grasps with robot-hand for planar elastic objects," in *ISR 2016: 47st International Symposium on Robotics; Proceedings of*, 2016, pp. 1–7.
- [22] F. L. Hammond, Y. Mengüç, and R. J. Wood, "Toward a modular soft sensor-embedded glove for human hand motion and tactile pressure measurement," in *Intelligent Robots and Systems (IROS 2014), 2014 IEEE/RSJ International Conference on,* 2014, pp. 4000–4007.
- [23] A. Massaro, M. Troia, F. Spano, and G. Carbone, "Friction in Totally Optical Robotic Finger Oriented on Shear Force Measurement," *Sensors Journal, IEEE*, vol. 13, no. 2, pp. 548–555, 2013.
- [24] G. Liang, Y. Wang, D. Mei, K. Xi, and Z. Chen, "Flexible Capacitive Tactile Sensor Array With Truncated Pyramids as Dielectric Layer for Three-Axis Force Measurement," *Microelectromechanical Systems, Journal of*, vol. 24, no. 5, pp. 1510–1519, 2015.
- [25] M. Yavuz, "Plantar shear: Casting light on 'dark matter," Low. Extrem. Rev., 2010.
- [26] M. Lord and R. Hosein, "A study of in-shoe plantar shear in patients with diabetic neuropathy.," *Clin Biomech (Bristol, Avon)*, vol. 15, no. 4, pp. 278–83, 2000.

- [27] P. Puangmali, K. Althoefer, L. D. Seneviratne, D. Murphy, and P. Dasgupta, "State-of-the-art in force and tactile sensing for minimally invasive surgery," *IEEE Sensors Journal*, vol. 8, no. 4, pp. 371–381, 2008.
- [28] M. Eltaib and J. Hewit, "Tactile sensing technology for minimal access surgery--a review," *Mechatronics*, vol. 13, no. 10, pp. 1163–1177, 2003.
- [29] M. Cianchetti, C. Laschi, A. Menciassi, and P. Dario, "Biomedical applications of soft robotics," *Nature Reviews Materials*, vol. 3, no. 6, pp. 143–153, 2018.
- [30] F. Li, Y. Akiyama, X. Wan, S. Okamoto, and Y. Yamada, "Measurement of shear strain field in a soft material using a sensor system consisting of distributed piezoelectric polymer film," *Sensors*, vol. 20, no. 12, p. 3484, 2020.
- [31] L. Wang and D. J. Beebe, "Characterization of a silicon-based shear-force sensor on human subjects," *Biomedical Engineering, IEEE Transactions on*, vol. 49, no. 11, pp. 1340–1347, 2002.
- [32] J. A. Dobrzynska and M. Gijs, "Polymer-based flexible capacitive sensor for three-axial force measurements," *Journal of Micromechanics and Microengineering*, vol. 23, no. 1, p. 015009, 2012.
- [33] J. Missinne, E. Bosman, B. Van Hoe, R. Verplancke, G. Van Steenberge, S. Kalathimekkad, P. Van Daele, and J. Vanfleteren, "Two axis optoelectronic tactile shear stress sensor," *Sensors and Actuators A: Physical*, vol. 186, pp. 63–68, 2012.
- [34] S. Rajala and J. Lekkala, "Plantar shear stress measurements A review.," *Clin Biomech (Bristol, Avon)*, vol. 29, no. 5, pp. 475–83, 2014.
- [35] L. Beccai, S. Roccella, A. Arena, F. Valvo, P. Valdastri, A. Menciassi, M. C. Carrozza, and P. Dario, "Design and fabrication of a hybrid silicon three-axial force sensor for biomechanical applications," *Sensors and Actuators A: Physical*, vol. 120, no. 2, pp. 370–382, 2005.
- [36] V. Rajtukova, R. Hudak, J. Zivcak, P. Halfarova, and R. Kudrikova, "Pressure distribution in transtibial prostheses socket and the stump interface," *Procedia Engineering*, vol. 96, pp. 374–381, 2014.
- [37] P. Catalfamo, D. Moser, S. Ghoussayni, and D. Ewins, "Detection of gait events using an F-Scan in-shoe pressure measurement system," *Gait* \& posture, vol. 28, no. 3, pp. 420–426, 2008.
- [38] J. Dargahi and S. Najarian, "Human tactile perception as a standard for artificial tactile sensing—a review," *The International Journal of Medical Robotics and Computer Assisted Surgery*, vol. 1, no. 1, pp. 23–35, 2004.
- [39] A. Amemiya, H. Noguchi, M. Oe, H. Sanada, and T. Mori, "Establishment of a measurement method for in-shoe pressure and shear stress in specific regions for diabetic ulcer prevention," in *Engineering in Medicine and Biology Society (EMBC)*,

- 2016 IEEE 38th Annual International Conference of the, 2016, pp. 2291–2294.
- [40] D. Alvares, L. Wieczorek, B. Raguse, F. Ladouceur, and N. H. Lovell, "Development of nanoparticle film-based multi-axial tactile sensors for biomedical applications," *Sensors and Actuators A: Physical*, vol. 196, pp. 38–47, 2013.
- [41] R. S. Dahiya, G. Metta, M. Valle, and G. Sandini, "Tactile sensing—from humans to humanoids," *Robotics, IEEE Transactions on*, vol. 26, no. 1, pp. 1–20, 2010.
- [42] L. Wang and D. J. Beebe, "A silicon-based shear force sensor: development and characterization," *Sensors and Actuators A: Physical*, vol. 84, no. 1, pp. 33–44, 2000.
- [43] W. Yuan, R. Li, M. A. Srinivasan, and E. H. Adelson, "Measurement of shear and slip with a GelSight tactile sensor," in 2015 IEEE International Conference on Robotics and Automation (ICRA), 2015, pp. 304–311.
- [44] E. Dean-Leon, K. Ramirez-Amaro, F. Bergner, I. Dianov, P. Lanillos, and G. Cheng, "Robotic technologies for fast deployment of industrial robot systems," in *Industrial Electronics Society, IECON 2016-42nd Annual Conference of the IEEE*, 2016, pp. 6900–6907.
- [45] A. Sergeeva, M. Huysman, and S. Faraj, "Transforming work practices of operating room teams: the case of the Da Vinci robot," 2015.
- [46] R. Johansson and G. Westling, "Roles of glabrous skin receptors and sensorimotor memory in automatic control of precision grip when lifting rougher or more slippery objects," *Experimental brain research*, vol. 56, no. 3, pp. 550–564, 1984.
- [47] P. Jenmalm, S. Dahlstedt, and R. S. Johansson, "Visual and tactile information about object-curvature control fingertip forces and grasp kinematics in human dexterous manipulation.," *J. Neurophysiol.*, vol. 84, no. 6, pp. 2984–97, 2000.
- [48] D. A. Nowak, S. Glasauer, and J. Hermsdörfer, "How predictive is grip force control in the complete absence of somatosensory feedback?," *Brain*, vol. 127, no. 1, pp. 182–192, 2004.
- [49] Z. Kappassov, J.-A. Corrales, and V. Perdereau, "Tactile sensing in dexterous robot hands—Review," *Robotics and Autonomous Systems*, vol. 74, pp. 195–220, 2015.
- [50] M. Geerligs, "Skin layer mechanics," Eindhoven: TU Eindhoven, 2010.
- [51] X. Song, H. Liu, K. Althoefer, T. Nanayakkara, and L. D. Seneviratne, "Efficient break-away friction ratio and slip prediction based on haptic surface exploration," *IEEE Transactions on Robotics*, vol. 30, no. 1, pp. 203–219, 2014.
- [52] M. Yavuz, A. Ersen, J. Hartos, B. Schwarz, A. G. Garrett, L. A. Lavery, D. K. Wukich, and L. S. Adams, "Plantar Shear Stress in Individuals With a History of Diabetic Foot Ulcer: An Emerging Predictive Marker for Foot Ulceration," *Diabetes care*, vol. 40, no. 2, pp. e14–e15, 2017.

- [53] S. Park and Y.-H. Kim, "Local shear stress measurements in the normal and diabetic foot patients during walking," in *World Congress on Medical Physics and Biomedical Engineering 2006*, 2007, pp. 2957–2960.
- [54] L. Wang, D. Jones, G. J. Chapman, H. J. Siddle, D. A. Russell, A. Alazmani, and P. Culmer, "A review of wearable sensor systems to monitor plantar loading in the assessment of diabetic foot ulcers," *IEEE Transactions on Biomedical Engineering*, vol. 67, no. 7, pp. 1989–2004, 2019.
- [55] M. Yavuz, "Plantar shear stress distributions in diabetic patients with and without neuropathy," *Clinical biomechanics (Bristol, Avon)*, vol. 29, no. 2, p. 223, 2014.
- [56] C. Groner, "shear madness beyond plantar pressure," Low. Extrem. Rev., 2009.
- [57] M. Hopkins, R. Vaidyanathan, and A. H. Mcgregor, "Examination of the performance characteristics of velostat as an in-socket pressure sensor," *IEEE Sensors Journal*, vol. 20, no. 13, pp. 6992–7000, 2020.
- [58] C.-T. Chang, C. S. Liu, W. Soetanto, and W.-C. Wang, "A platform-based foot pressure/shear sensor," in *SPIE Smart Structures and Materials+ Nondestructive Evaluation and Health Monitoring*, 2012, p. 83481U–83481U.
- [59] T. Nelson, S. Jin, S. Hackwood, G. Beni, and others, "Shear-sensitive magnetoresistive robotic tactile sensor," *IEEE Transactions on Magnetics*, vol. 22, no. 5, pp. 394–396, 1986.
- [60] L. S. Lincoln, M. Quigley, B. Rohrer, C. Salisbury, and J. Wheeler, "An optical 3D force sensor for biomedical devices," in 2012 4th IEEE RAS & EMBS International Conference on Biomedical Robotics and Biomechatronics (BioRob), 2012, pp. 1500–1505.
- [61] M. I. Tiwana, S. J. Redmond, and N. H. Lovell, "A review of tactile sensing technologies with applications in biomedical engineering," *Sensors and Actuators A: physical*, vol. 179, pp. 17–31, 2012.
- [62] J. Sorab, R. Allen, and B. Gonik, "Tactile sensory monitoring of clinician-applied forces during delivery of newborns," *IEEE Transactions on Biomedical Engineering*, vol. 35, no. 12, pp. 1090–1093, 1988.
- [63] P. Peng and R. Rajamani, "Flexible microtactile sensor for normal and shear elasticity measurements," *IEEE Transactions on Industrial Electronics*, vol. 59, no. 12, pp. 4907–4913, 2012.
- [64] C. Domenici, D. De Rossi, A. Bacci, and S. Bennati, "Shear stress detection in an elastic layer by a piezoelectric polymer tactile sensor," *IEEE Transactions on Electrical Insulation*, vol. 24, no. 6, pp. 1077–1081, 1989.
- [65] N. Wettels, D. Popovic, V. J. Santos, R. S. Johansson, and G. E. Loeb, "Biomimetic tactile sensor for control of grip," in *Rehabilitation Robotics*, 2007. ICORR 2007.

- *IEEE 10th International Conference on*, 2007, pp. 923–932.
- [66] M. Cheng, X. Huang, C. Ma, and Y. Yang, "A flexible capacitive tactile sensing array with floating electrodes," *Journal of Micromechanics and Microengineering*, vol. 19, no. 11, p. 115001, 2009.
- [67] Y. Xin, H. Tian, C. Guo, X. Li, H. Sun, P. Wang, J. Lin, S. Wang, and C. Wang, "PVDF tactile sensors for detecting contact force and slip: A review," *Ferroelectrics*, vol. 504, no. 1, pp. 31–45, 2016.
- [68] W.-C. Wang, W. R. Ledoux, B. J. Sangeorzan, and P. G. Reinhall, "A shear and plantar pressure sensor based on fiber-optic bend loss," *Journal of rehabilitation research and development*, vol. 42, no. 3, p. 315, 2005.
- [69] G. Taylor, "Pressure and shear-definitions, relationships and measurements," *Vista Medical. Available online at: http://www. pressuremapping. com/File/ShearTerms. pdf (accessed 7 October 2008)*, 2014.
- [70] H. Orsted, T. Ohura, and K. Harding, "Pressure, shear, friction and microclimate in context," *A consensus document. Wounds International, London, UK*, 2010.
- [71] G. Cadoret and A. M. Smith, "Friction, not texture, dictates grip forces used during object manipulation," *Journal of Neurophysiology*, vol. 75, no. 5, pp. 1963–1969, 1996.
- [72] A. M. Smith, "Some shear facts and pure friction related to roughness discrimination and the cutaneous control of grasping," *Canadian journal of physiology and pharmacology*, vol. 72, no. 5, pp. 583–590, 1994.
- [73] R. Huston and H. Josephs, "Practical Stress Analysis in Engineering designCH2," 2009.
- [74] S. Bus, "Innovations in plantar pressure and foot temperature measurements in diabetes," *Diabetes/metabolism research and reviews*, vol. 32, no. S1, pp. 221–226, 2016.
- [75] B. Bhushan, *Introduction to tribology*. John Wiley & Sons, 2013.
- [76] B. Briscoe, A. Arvanitaki, M. Adams, and S. Johnson, "The friction and adhesion of elastomers," *Tribology Series*, vol. 39, pp. 661–672, 2001.
- [77] B. Briscoe and D. Tabor, "Shear properties of thin polymeric films," *The Journal of Adhesion*, vol. 9, no. 2, pp. 145–155, 1978.
- [78] R. Balasubramanian and V. J. Santos, *The human hand as an inspiration for robot hand development*, vol. 95. Springer, 2014.
- [79] D. A. Nowak, *Sensorimotor control of grasping: physiology and pathophysiology*. Cambridge University Press, 2009.

- [80] A. W. Goodwin, P. Jenmalm, and R. S. Johansson, "Control of grip force when tilting objects: effect of curvature of grasped surfaces and applied tangential torque.," *J. Neurosci.*, vol. 18, no. 24, pp. 10724–34, 1998.
- [81] J. R. NAPIER, "The prehensile movements of the human hand.," *J Bone Joint Surg Br*, vol. 38-B, no. 4, pp. 902–13, 1956.
- [82] T. Feix, J. Romero, H.-B. Schmiedmayer, A. M. Dollar, and D. Kragic, "The grasp taxonomy of human grasp types," *IEEE Transactions on Human-Machine Systems*, vol. 46, no. 1, pp. 66–77, 2016.
- [83] B. Siciliano and O. Khatib, Springer handbook of robotics. Springer, 2016.
- [84] B. León, A. Morales, and J. Sancho-Bru, *From robot to human grasping simulation*. Springer, 2014.
- [85] S. T. Venkataraman and T. Iberall, *Dextrous robot hands*. Springer Science & Business Media, 2012.
- [86] N. J. Seo and T. J. Armstrong, "Investigation of grip force, normal force, contact area, hand size, and handle size for cylindrical handles," *Human Factors: The Journal of the Human Factors and Ergonomics Society*, vol. 50, no. 5, pp. 734–744, 2008.
- [87] M. S. us Sarwar, "Soft capacitive sensors for proximity, touch, pressure and shear measurements," *T, University of British Columbia*, 2019.
- [88] D. Baimukashev, Z. Kappassov, and H. A. Varol, "Shear, torsion and pressure tactile sensor via plastic optofiber guided imaging," *IEEE Robotics and Automation Letters*, vol. 5, no. 2, pp. 2618–2625, 2020.
- [89] N. Elkmann, M. Fritzsche, and E. Schulenburg, "Tactile sensing for safe physical human-robot interaction," in *International conference on advances in computer-human interactions*, 2011, pp. 212–217.
- [90] J. G. Rocha and S. Lanceros-Mendez, *Three Dimensional Capacitive Force Sensor for Tactile Applications*. INTECH Open Access Publisher, 2008.
- [91] Y.-H. Jen, C.-T. Mo, K. Aw, D. Yamane, and C.-Y. Lo, "Extensive Sensitivity Enhancement in Stacked Capacitive Tactile Sensors," in *2019 IEEE SENSORS*, 2019, pp. 1–4.
- [92] M. Schouten, C. Spaan, D. Kosmas, R. Sanders, and G. Krijnen, "3D printed capacitive shear and normal force sensor using a highly flexible dielectric," in *2021 IEEE Sensors Applications Symposium (SAS)*, 2021, pp. 1–6.
- [93] J. Novak, "Initial design and analysis of a capacitive sensor for shear and normal force measurement," in *Robotics and Automation*, 1989. Proceedings., 1989 IEEE International Conference on, 1989, pp. 137–144.

- [94] F. Zhu and J. Spronck, "A capacitive tactile sensor for shear and normal force measurements," *Sensors and Actuators A: Physical*, vol. 31, no. 1–3, pp. 115–120, 1992.
- [95] Y. Huang, D. Fang, C. Wu, W. Wang, X. Guo, and P. Liu, "A flexible touch-pressure sensor array with wireless transmission system for robotic skin," *Review of Scientific Instruments*, vol. 87, no. 6, p. 065007, 2016.
- [96] S. Stassi, V. Cauda, G. Canavese, and C. F. Pirri, "Flexible tactile sensing based on piezoresistive composites: A review," *Sensors*, vol. 14, no. 3, pp. 5296–5332, 2014.
- [97] Y. Jung, D.-G. Lee, J. Park, H. Ko, and H. Lim, "Piezoresistive tactile sensor discriminating multidirectional forces," *Sensors*, vol. 15, no. 10, pp. 25463–25473, 2015.
- [98] K. Noda, K. Hoshino, K. Matsumoto, and I. Shimoyama, "A shear stress sensor for tactile sensing with the piezoresistive cantilever standing in elastic material," *Sensors and Actuators A: physical*, vol. 127, no. 2, pp. 295–301, 2006.
- [99] R. S. Dahiya and M. Valle, *Robotic tactile sensing: technologies and system*. Springer Science & Business Media, 2012.
- [100] P. Yu, W. Liu, C. Gu, X. Cheng, and X. Fu, "Flexible piezoelectric tactile sensor array for dynamic three-axis force measurement," *Sensors*, vol. 16, no. 6, p. 819, 2016.
- [101] M. A. McGeehan, S. S. Karipott, M. E. Hahn, D. C. Morgenroth, and K. G. Ong, "An Optoelectronics-Based Sensor for Measuring Multi-Axial Shear Stresses," *IEEE Sensors Journal*, vol. 21, no. 22, pp. 25641–25648, 2021.
- [102] B. Nie, R. Li, J. D. Brandt, and T. Pan, "Microfluidic tactile sensors for three-dimensional contact force measurements," *Lab on a Chip*, vol. 14, no. 22, pp. 4344–4353, 2014.
- [103] Y. Wang, G. Liang, D. Mei, L. Zhu, and Z. Chen, "A flexible capacitive tactile sensor array with high scanning speed for distributed contact force measurements," in 2016 IEEE 29th International Conference on Micro Electro Mechanical Systems (MEMS), 2016, pp. 854–857.
- [104] Y. Jung, D.-G. Lee, J. Park, H. Ko, and H. Lim, "Piezoresistive tactile sensor discriminating multidirectional forces," *Sensors*, vol. 15, no. 10, pp. 25463–25473, 2015.
- [105] B. Kim, S. Shin, J. Chung, Y. Lee, J.-D. Nam, H. Moon, H. R. Choi, and J. C. Koo, "A dual axis shear force film sensor for robotic tactile applications," in *SPIE Smart Structures and Materials+ Nondestructive Evaluation and Health Monitoring*, 2011, pp. 797628–797628.
- [106] K. Liao, M. T. Hou, and J. A. Yeh, "A dielectiric liquid-based capcitive tactile sensor for normal and shear force sensing," in *Solid-State Sensors, Actuators and Microsystems (TRANSDUCERS \& EUROSENSORS XXVII), 2013 Transducers \&*

- *Eurosensors XXVII: The 17th International Conference on*, 2013, pp. 1000–1003.
- [107] M.-Y. Cheng, C.-L. Lin, and Y.-J. Yang, "Tactile and shear stress sensing array using capacitive mechanisms with floating electrodes," in *Micro Electro Mechanical Systems (MEMS)*, 2010 IEEE 23rd International Conference on, 2010, pp. 228–231.
- [108] P. Roberts, D. D. Damian, W. Shan, T. Lu, and C. Majidi, "Soft-matter capacitive sensor for measuring shear and pressure deformation," in 2013 IEEE International Conference on Robotics and Automation, 2013, pp. 3529–3534.
- [109] Y. Zhang, A. S. Sezen, and R. Rajamani, "A Low-Profile Supercapacitor-Based Normal and Shear Force Sensor," *IEEE Sensors Journal*, vol. 21, no. 1, pp. 239–249, 2020.
- [110] Z. F. Zhang, X. M. Tao, H. P. Zhang, and B. Zhu, "Soft Fiber Optic Sensors for Precision Measurement of Shear Stress and Pressure," *Sensors Journal, IEEE*, vol. 13, no. 5, pp. 1478–1482, 2013.
- [111] J. A. Dobrzynska and M. A. Gijs, "Flexible polyimide-based force sensor," *Sensors and Actuators A: Physical*, vol. 173, no. 1, pp. 127–135, 2012.
- [112] T. Zhang, H. Liu, L. Jiang, S. Fan, and J. Yang, "Development of a flexible 3-D tactile sensor system for anthropomorphic artificial hand," *Sensors Journal, IEEE*, vol. 13, no. 2, pp. 510–518, 2013.
- [113] P. S. Girão, P. M. P. Ramos, O. Postolache, and J. Miguel Dias Pereira, "Tactile sensors for robotic applications," *Measurement*, vol. 46, no. 3, pp. 1257–1271, 2013.
- [114] M.-Y. Cheng, C.-L. Lin, Y.-T. Lai, and Y.-J. Yang, "A polymer-based capacitive sensing array for normal and shear force measurement," *Sensors*, vol. 10, no. 11, pp. 10211–10225, 2010.
- [115] H.-K. Lee, J. Chung, S.-I. Chang, and E. Yoon, "Normal and shear force measurement using a flexible polymer tactile sensor with embedded multiple capacitors," *Journal of Microelectromechanical Systems*, vol. 17, no. 4, pp. 934–942, 2008.
- [116] H. Takahashi, A. Nakai, N. Thanh-Vinh, K. Matsumoto, and I. Shimoyama, "A triaxial tactile sensor without crosstalk using pairs of piezoresistive beams with sidewall doping," *Sensors and Actuators A: Physical*, 2013.
- [117] T. Okatani, H. Takahashi, K. Noda, T. Takahata, K. Matsumoto, and I. Shimoyama, "A Tactile Sensor Using Piezoresistive Beams for Detection of the Coefficient of Static Friction," *Sensors*, vol. 16, no. 5, p. 718, 2016.
- [118] L. Wang and D. J. Beebe, "Shear sensitive silicon piezoresistive tactile sensor prototype," in *Micromachining and Microfabrication*, 1998, pp. 359–367.
- [119] T. Yang, D. Xie, Z. Li, and H. Zhu, "Recent advances in wearable tactile sensors: Materials, sensing mechanisms, and device performance," *Materials Science and*

- *Engineering: R: Reports*, vol. 115, pp. 1–37, 2017.
- [120] Y. Amarasinghe, A. Kulasekera, and T. Priyadarshana, "Quantum tunneling composite (QTC) based tactile sensor array for dynamic pressure distribution measurement," in *Sensing Technology (ICST)*, 2013 Seventh International Conference on, 2013, pp. 1–4.
- [121] X. Shi, C.-H. Cheng, C. Chao, L. Wang, and Y. Zheng, "A piezoresistive normal and shear force sensor using liquid metal alloy as gauge material," in *Nano/Micro Engineered and Molecular Systems (NEMS)*, 2012 7th IEEE International Conference on, 2012, pp. 483–486.
- [122] C.-C. Wen and W. Fang, "Tuning the sensing range and sensitivity of three axes tactile sensors using the polymer composite membrane," *Sensors and Actuators A: Physical*, vol. 145, pp. 14–22, 2008.
- [123] H. Kawai, "The piezoelectricity of poly (vinylidene fluoride)," *Japanese Journal of Applied Physics*, vol. 8, no. 7, p. 975, 1969.
- [124] S. Kärki, J. Lekkala, H. Kuokkanen, and J. Halttunen, "Development of a piezoelectric polymer film sensor for plantar normal and shear stress measurements," *Sensors and Actuators A: Physical*, vol. 154, no. 1, pp. 57–64, 2009.
- [125] B. Choi, H. R. Choi, and S. Kang, "Development of tactile sensor for detecting contact force and slip," in *Intelligent Robots and Systems*, 2005.(IROS 2005). 2005 IEEE/RSJ International Conference on, 2005, pp. 2638–2643.
- [126] J. Dargahi, R. Sedaghati, H. Singh, and S. Najarian, "Modeling and testing of an endoscopic piezoelectric-based tactile sensor," *Mechatronics*, vol. 17, no. 8, pp. 462–467, 2007.
- [127] W.-C. Wang, R. R. Panergo, C. M. Galvanin, W. Ledoux, B. Sangeorzan, and P. G. Reinhall, "A flexible micromachined optical sensor for simultaneous measurement of pressure and shear force distribution on foot," in *NDE for Health Monitoring and Diagnostics*, 2003, pp. 275–285.
- [128] M. Ohka, H. Kobayashi, J. Takata, and Y. Mitsuya, "Sensing precision of an optical three-axis tactile sensor for a robotic finger," in *ROMAN 2006-The 15th IEEE International Symposium on Robot and Human Interactive Communication*, 2006, pp. 214–219.
- [129] V. N. Dubey and R. M. Crowder, "A dynamic tactile sensor on photoelastic effect," *Sensors and Actuators A: Physical*, vol. 128, no. 2, pp. 217–224, 2006.
- [130] H. Yussof, S. C. Abdullah, and M. Ohka, "Development of optical three-axis tactile sensor and its application to robotic hand for dexterous manipulation tasks," in *Mathematical/Analytical Modelling and Computer Simulation (AMS), 2010 Fourth Asia International Conference on*, 2010, pp. 624–629.
- [131] M. Ohka, N. Morisawa, H. Suzuki, J. Takata, H. Koboyashi, and H. B. Yussof, "A robotic finger equipped with an optical three-axis tactile sensor," in *Robotics and*

- Automation, 2008. ICRA 2008. IEEE International Conference on, 2008, pp. 3425–3430.
- [132] S. C. Mukhopadhyay and G. S. Gupta, *Autonomous Robots and Agents*. Springer Publishing Company, Incorporated, 2007.
- [133] D. Tan, Q. Wang, R. Song, X. Yao, and Y. Gu, "Optical fiber based slide tactile sensor for underwater robots," *Journal of Marine Science and Application*, vol. 7, no. 2, pp. 122–126, 2008.
- [134] S.-T. Chuang, M. Chandra, R. Chen, and C.-Y. Lo, "Capacitive tactile sensor with asymmetric electrodes for angle-detection-error alleviation," *Sensors and Actuators A: Physical*, vol. 250, pp. 159–169, 2016.
- [135] R. S. Johansson and J. R. Flanagan, "Coding and use of tactile signals from the fingertips in object manipulation tasks," *Nature Reviews Neuroscience*, vol. 10, no. 5, pp. 345–359, 2009.
- [136] S. Tjin, R. Suresh, and N. Ngo, "Fiber Bragg grating based shear-force sensor: Modeling and testing," *Journal of lightwave technology*, vol. 22, no. 7, pp. 1728–1733, 2004.
- [137] Y.-C. Chung, S.-T. Chuang, T.-Y. Chen, C.-Y. Lo, and R. Chen, "Capacitive Tactile Sensor for Angle Detection and Its Accuracy Study," *IEEE Sensors Journal*, vol. 16, no. 18, pp. 6857–6865, 2016.
- [138] H. Muhammad, C. Recchiuto, C. Oddo, L. Beccai, C. Anthony, M. Adams, M. Carrozza, and M. Ward, "A capacitive tactile sensor array for surface texture discrimination," *Microelectronic Engineering*, vol. 88, no. 8, pp. 1811–1813, 2011.
- [139] H.-K. Lee, J. Chung, S.-I. Chang, and E. Yoon, "Real-time measurement of the three-axis contact force distribution using a flexible capacitive polymer tactile sensor," *Journal of Micromechanics and Microengineering*, vol. 21, no. 3, p. 035010, 2011.
- [140] S. Cramp, C. Maccoll, and R. B. Wallace, "Preliminary results for novel shear force sensor using force sensitive resistors," in 2020 IEEE international instrumentation and measurement technology conference (I2MTC), 2020, pp. 1–6.
- [141] B. Kane and G. Kovacs, "A CMOS compatible traction stress sensing element for use in high resolution tactile imaging," in *Solid-State Sensors and Actuators, 1995 and Eurosensors IX.*. Transducers' 95. The 8th International Conference on, 1995, vol. 1, pp. 648–651.
- [142] K. Sato, N. Binh-Khiem, M. Hosono, K. Matsumoto, and I. Shimoyama, "Shear force sensor using a cantilever with liquid-embedded hinges," in *Micro Electro Mechanical Systems (MEMS)*, 2012 IEEE 25th International Conference on, 2012, pp. 603–606.
- [143] G. De Maria, C. Natale, and S. Pirozzi, "Force/tactile sensor for robotic applications," *Sensors and Actuators A: Physical*, vol. 175, pp. 60–72, 2012.

- [144] K.-W. Liao, M. T. Hou, and J. A. Yeh, "Multi-axis dielectric liquid-based tactile sensor with tunable sensing range and sensitivity," in *Design, Test, Integration and Packaging of MEMS/MOEMS (DTIP), 2016 Symposium on,* 2016, pp. 1–4.
- [145] D. Choi, S. Jang, J. S. Kim, H.-J. Kim, D. H. Kim, and J.-Y. Kwon, "A Highly Sensitive Tactile Sensor Using a Pyramid-Plug Structure for Detecting Pressure, Shear Force, and Torsion," *Advanced Materials Technologies*, vol. 4, no. 3, p. 1800284, 2019.
- [146] M. Lord, R. Hosein, and R. Williams, "Method for in-shoe shear stress measurement," *Journal of biomedical engineering*, vol. 14, no. 3, pp. 181–186, 1992.
- [147] S.-I. Ao, B. B. Rieger, and S.-S. Chen, *Advances in Computational Algorithms and Data Analysis*, vol. 14. Springer Science & Business Media, 2008.
- [148] B. D. Argall and A. G. Billard, "A survey of tactile human-robot interactions," *Robotics and autonomous systems*, vol. 58, no. 10, pp. 1159–1176, 2010.
- [149] L. M. Castano and A. B. Flatau, "Smart fabric sensors and e-textile technologies: a review," *Smart Materials and Structures*, vol. 23, no. 5, p. 053001, 2014.